

Title	Effect of Neutron Irradiation on Strength of Electron Beam Welded Joint of JFMS Steel for Fusion Reactor (Materials, Metallurgy & Weldability)
Author(s)	Kaga, Seiichi; Fujii, Katsuhito; Tamura, Toshihiro et al.
Citation	Transactions of JWRI. 1989, 18(2), p. 253-257
Version Type	VoR
URL	https://doi.org/10.18910/10328
rights	
Note	

Osaka University Knowledge Archive : OUKA

<https://ir.library.osaka-u.ac.jp/>

Osaka University

Effect of Neutron Irradiation on Strength of Electron Beam Welded Joint of JFMS Steel for Fusion Reactor†

Seiichi KAGA*, Katsuhito FUJII**, Toshihiro TAMURA***, Toshiaki BABA***, Yoshiaki YAMAMOTO****, Kouichi OGAWA*****, Nobuyuki ABE***** and Michio TOMIE*****

Abstract

JFMS steel is a candidate material for nuclear fusion reactor in Japan. It is a material for high temperature use. Structural materials of fusion reactor will be exposed in neutron irradiation. In order to research the basic property of the material under irradiation, low temperature strength of JFMS steel and its electron beam welded joint is investigated under various irradiated conditions in this experiment.

It was shown, as testing results, that decreasing of strength and elongation at low temperature of base metal and electron beam welded joint of JFMS steel increases with increasing of neutron fluence.

KEY WORDS: (Nuclear Fusion Reactor) (Neutron Irradiation) (Ferritic Special Steel) (Tensile Test) (Notch Brittleness) (Welded Joint)

1. Introduction

Ferritic special steel (JFMS) is selected as testing materials in this study from the candidate materials for nuclear fusion reactor in Japan¹⁾. JFMS (Japanese Ferritic and Martensitic Steel) is selected as candidate material for nuclear fusion reactor in 9Cr - 2Mo ferritic steel²⁾. 9Cr - 2Mo steel is a heat proof material but it is superior than austenitic stainless steel in resistance to swelling by neutron irradiation and resistance to helium embrittlement^{3),4)}.

So, in this investigation, the material are welded by electron beam welding and the strength of base metal and welded joint is examined at cryogenic temperature. JFMS is a material for high temperature use but test is conducted at only low temperature, in this investigation.

2. Testing Method

2.1 Testing materials

Chemical composition is shown in Table 1.

2.2 Processing of the materials

After the materials are welded by electron beam welding method in the condition shown in Table 2, the

smooth specimen and notched specimen are sampled in the direction of rolling shown in Fig. 1. Horizontal position welding method is used to prevent the melting down of weld metal. Schematic diagram of horizontal position welding method is shown in Fig. 2. C/D value is 10% in this experiment. In full penetration welding, the important factor is the value of C/D, the beam pass rate of the beam current. ($C/D = I_c / I_b$; I_b indicates the incident beam current, I_c indicates the collected beam current shown in Fig. 3.) Size of the specimens is shown in Fig. 3. Small size of specimens are used under the consideration of evaporation of helium and capacity of testing machine. It has volume ratio of 1 / 360 compared with that of JIS No. 4 specimen. After processing the specimens, they are

Table 1 Chemical compositions of JFMS

Material	Chemical compositions (wt%)										
	Fe	Si	Mn	Cr	Ni	C	P	S	Mo	V	Nb
JFMS	BAL.	0.67	0.58	9.58	0.94	0.05	0.009	0.006	2.31	0.12	0.06

Table 2 Welding conditions of materials used (6.7×10^{-2} Pa)

Material	Welding position	Beam voltage (kV)	Beam current (mA)	Welding speed (m/min)
JFMS*	Horizontal	100	60	0.6

* Beam oscillation : $f_x = 30$ (Hz), $d_x = 3$ (mm)

† Received on October 31, 1989

* Professor, Osaka Institute of Technology.

** Research Associate, Osaka Institute of Technology.

*** Graduate Student, Osaka Institute of Technology.

**** Associate Professor, Setsunan University.

***** Assistant Professor, University of Osaka Pref.

***** Associate Professor

Transaction of JWRI is published by Welding Research Institute of Osaka University, Ibaraki, Osaka 567, Japan

Table 3 Neutron irradiation conditions of JFMS ($E < 0.1\text{MeV}$)

Irradiation apparatus	Irradiation time (hr)	Fast neutron flux density ($\text{n/m}^2\cdot\text{s}$)	Neutron fluence (n/m^2)	Irradiation temperature (K)
KUR	78.30	7.3×10^{16}	2.0×10^{22}	363
Reactor core	313.66		8.2×10^{22}	

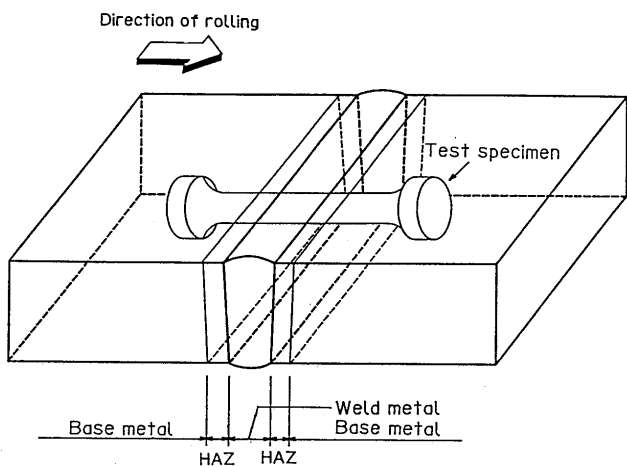


Fig. 1 Sampling of test specimen from welded joint

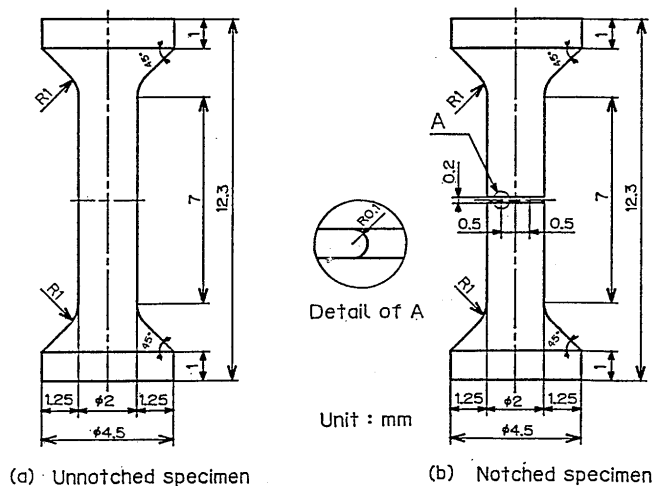


Fig. 3 Test specimen of JFMS

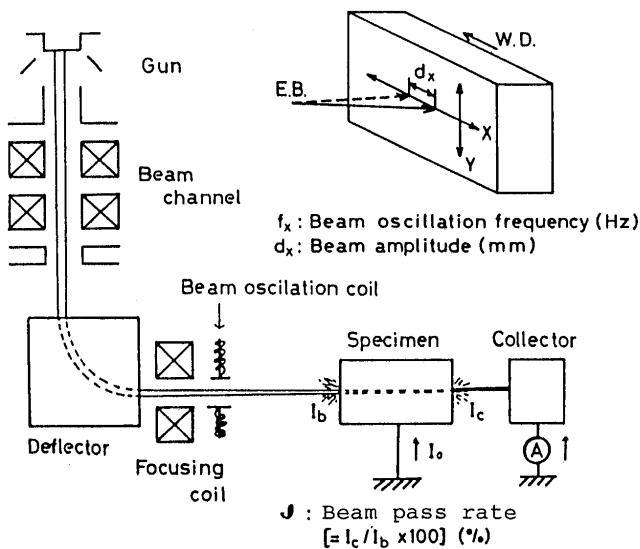


Fig. 2 Schematic diagram of horizontal position welding method

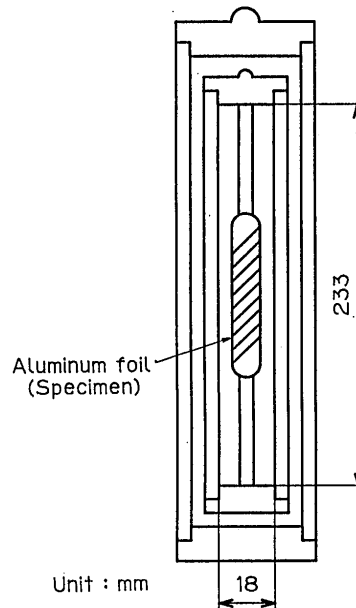


Fig. 4 Capsule for neutron irradiation

exposed to neutron irradiation in KUR reactor core by using the capsule for neutron irradiation shown in Fig. 4. Neutron irradiation conditions of the material are shown in Table 3.

2.3 Tensile test

Testing apparatus used in this experiment is shown in Fig. 5. Cryostat is used in experiment at liquid helium temperature. Autograph (AG-500A, capacity 4900N) is used as tensile apparatus. Testing temperatures are room temperature (293K), liquid nitrogen temperature (77K)

and liquid helium temperature (4.2K), and initial strain rate is $2.38 \times 10^{-4} \text{ s}^{-1}$.

3. Results of experiment and consideration

3.1 Nominal stress-nominal strain curve

Load-displacement curves obtained in this test of base metal and welded joint are shown in Fig. 6 and Fig. 7,

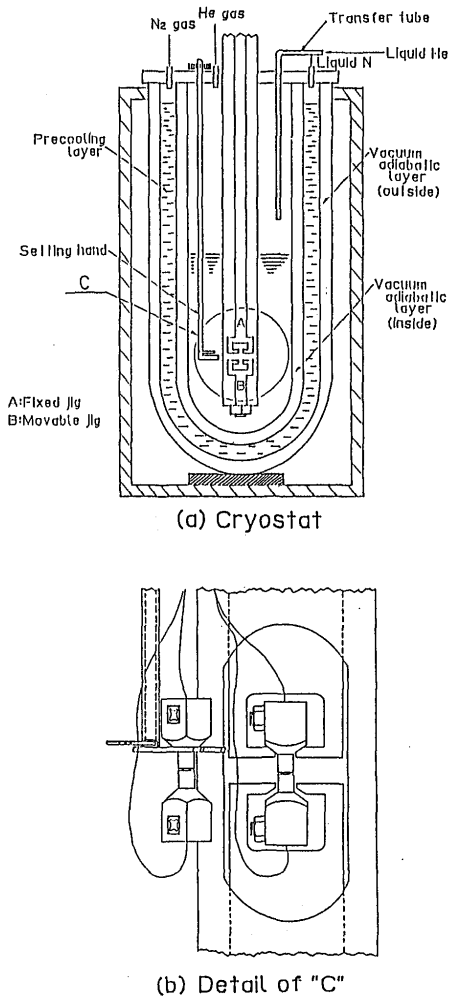


Fig. 5 Apparatus for cryogenic test

respectively.

3.2 Neutron fluence dependences of strength of the material

Neutron fluence dependences of ultimate tensile strength and 0.2% proof stress of base metal and welded joint of JFMS are shown in Fig. 8 and Fig. 9, respectively.

Proof stress and ultimate tensile strength at 293K and 77K of base metal of JFMS increase with increasing of neutron fluence.

Proof stress and ultimate tensile strength at 293K of welded joint of JFMS also increase with increasing of neutron fluence. However, proof stress and ultimate tensile strength at 4.2K of base metal and welded joint of JFMS much decrease at high neutron fluence of $8.2 \times 10^{22} \text{ n / m}^2$.

3.3 Neutron fluence dependences of elongation of the material

Neutron fluence dependences of elongation of JFMS against various test temperatures are shown in Fig. 10. Elongation of base metal and welded joint of JFMS at various test temperature decrease with increasing of neutron fluence.

3.4 Tensile property of notched specimen

3.4.1 Notch tensile strength

Neutron fluence dependence of notch tensile strength of JFMS against various temperatures are shown in Fig. 11. Notch tensile strength of welded joint of JFMS at

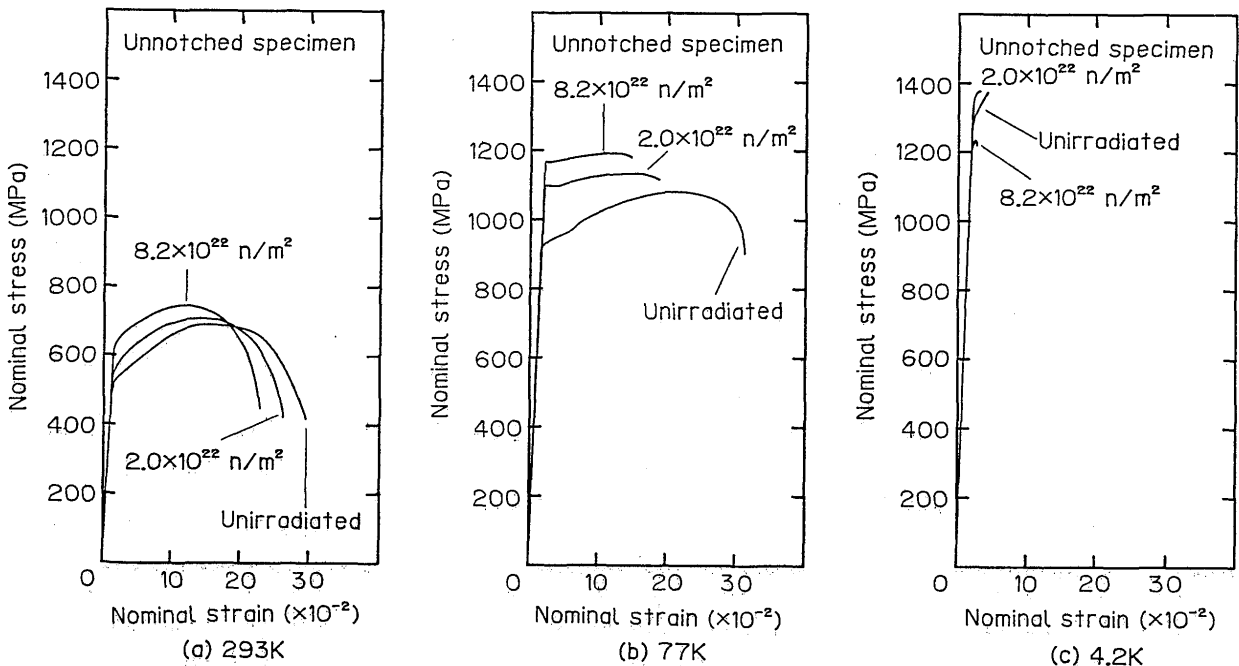


Fig. 6 Nominal stress-strain curves at various test temperatures of JFMS base metals irradiated at different neutron fluence

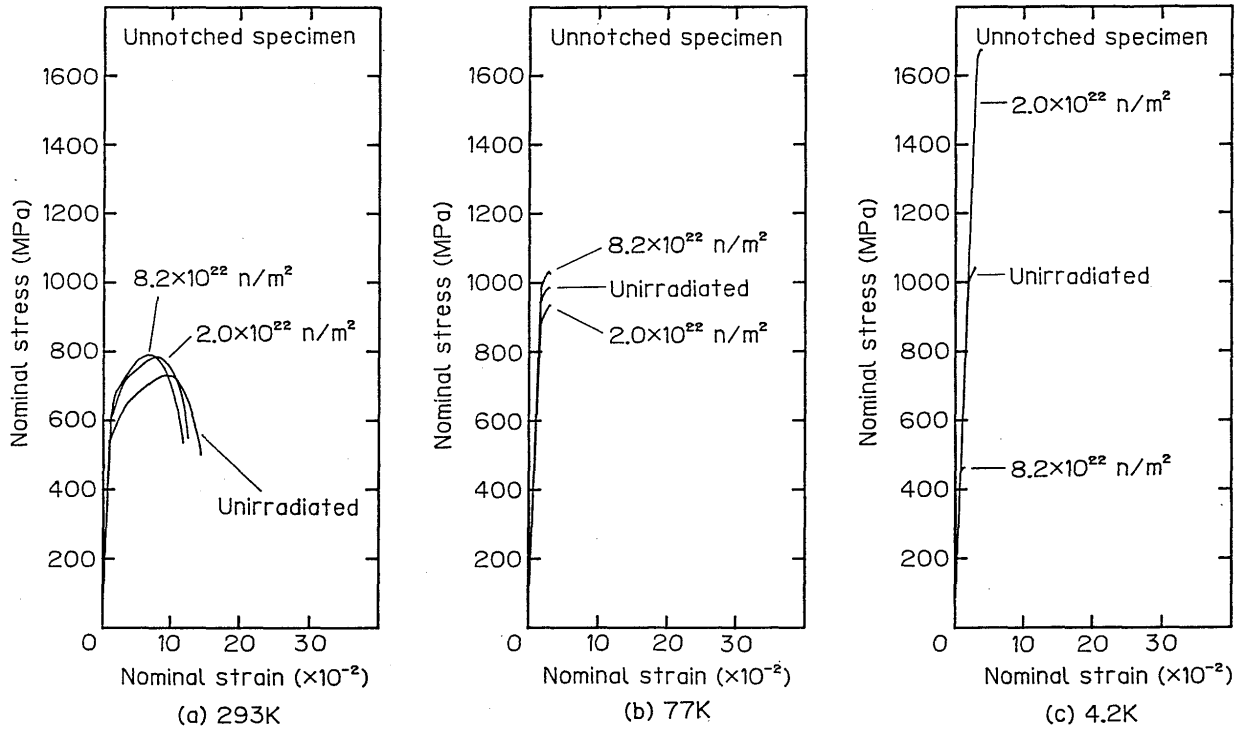


Fig. 7 Nominal stress-strain curves at various test temperatures of JFMS welded joints irradiated at different neutron fluence

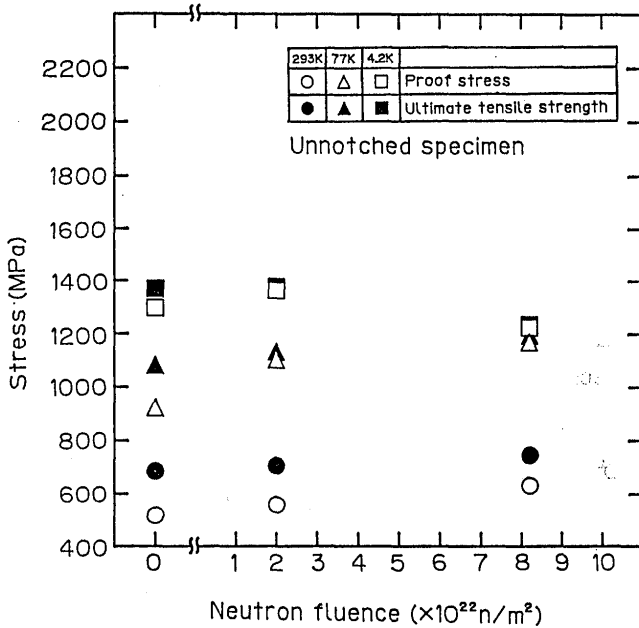


Fig. 8 Neutron fluence dependences of ultimate tensile strength and 0.2% proof stress of JFMS base metals against various test temperatures

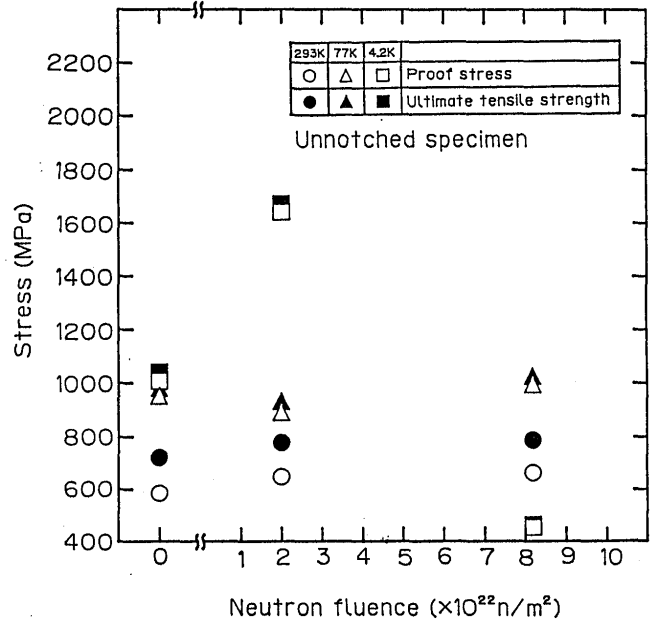


Fig. 9 Neutron fluence dependences of ultimate tensile strength and 0.2% proof stress of JFMS welded joints against various test temperatures

293K increases with increasing neutron fluence and notch tensile strength of welded joint of JFMS at 4.2K decrease with increasing of neutron fluence. Effect of neutron irradiation on the notch tensile strength of welded joint is more evident than effect of neutron irradiation on the notch tensile strength of base metal.

3.4.2 Notch proof stress ratio

Neutron fluence dependences of notch proof stress ratio (notch tensile strength / unnotched proof stress) between notched and unnotched specimen of JFMS against various temperatures are shown in Fig. 12. Notch proof ratio has good correlation to fracture toughness and is used as evaluating method of toughness. Notch proof stress ratio decreases at low neutron fluence and increases again at high neutron fluence as shown in Fig. 12.

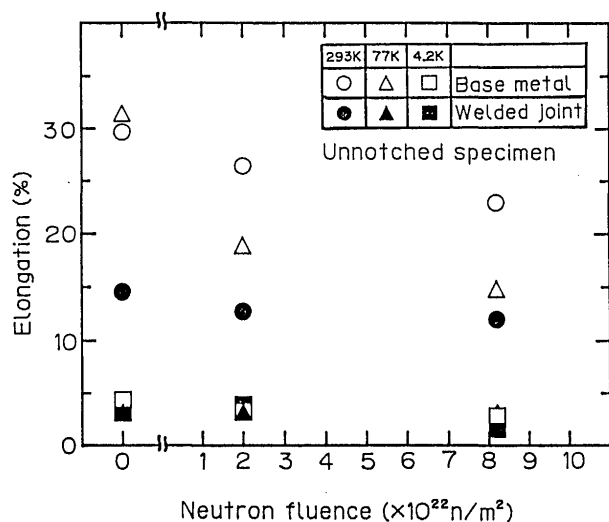


Fig. 10 Neutron fluence dependences of notch tensile strength of JFMS against various test temperatures

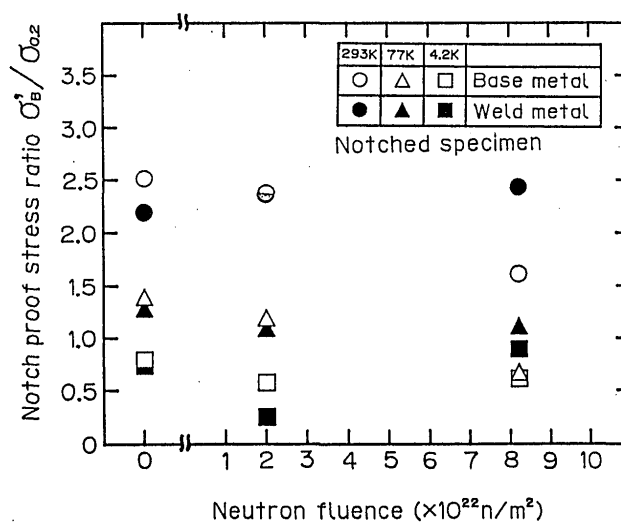


Fig. 12 Neutron fluence dependences of notch proof stress ratio between notched and unnotched specimen of JFMS against various test temperatures

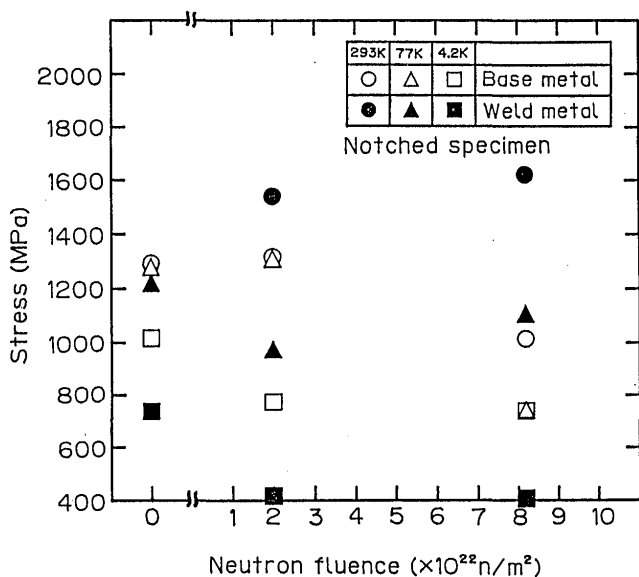


Fig. 11 Neutron fluence dependences of notch tensile strength JFMS against various test temperatures

4. Conclusion

- (1) Strength of base metal and welded joint at 293K and 77K increases with increasing of neutron fluence. Strength at 4.2K decreases with increasing of neutron fluence. Decreasing of the strength at 4.2K in high neutron fluence is larger in welded joint than in base metal.
- (2) Elongation of base metal and welded joint of JFMS decreases with increasing of neutron fluence.
- (3) Notch tensile strength of welded joint of JFMS at 293K increases with increasing of neutron fluence and notch tensile strength of welded joint of JFMS at 4.2K decreases with increasing of neutron fluence.

- (4) Notch proof stress ratio between notched and unnotched specimen of JFMS at various test temperatures decreases with low neutron fluence and increases again with high neutron fluence.

Acknowledgement

Material was presented and neutron irradiation was conducted by Dr. Hiroyuki Yoshida, associate professor, Hot Laboratory, Research Reactor Institute of Kyoto University. Tensile test are conducted by using the testing apparatus of the Hot Laboratory with the assistance of Mr. Kiyomi Miyata, research assistant, Research Reactor Institute of Kyoto University.

References

- 1) Society of Atomic Energy Engineering; Present State and Problem of Design and Research Development of Nuclear Fusion Reactor, (1983) (in Japanese)
- 2) Society of Atomic Energy Engineering; Progress of Research of Neutron Fusion Reactor and Review of Development of Power Reactor, (1976) (in Japanese)
- 3) Energy Special Research (Nuclear Fusion) Group of Heavy Irradiation; "Progress of Heavy Irradiation Research", Total Report, (1986), 183-203 (in Japanese)
- 4) T. Takeyama; Problem and Irradiated Structure of Irradiation proof Ferritic Stainless Steel, Metal, Vol. 56, No 1 (1986), 24-28 (in Japanese)
- 5) Y. Arata, M. Tomie; 100kW Class Electron Beam Welding Technology (Report IV), Trans. of JWRI, Vol.9, No.2 (1980), 15-24