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Controlling of Ceramic-Metal Interfacial Structure Using Molten Metals†

Masaaki NAKA*

Abstract

This article reviews the dominating factors of wettablility of ceramics by molten metals and interface strength of ceramic/metal joint. The role of titanium in copper–titanium alloys during brazing is discussed. The formation of TiN nitride or TiC, Ti₅SiC₂ carbide at the interface and the wetting of Cu–Si alloy against compounds formed during brazing are attributable to the better wettablility of Cu–Ti alloy against Si₃N₄ or SiC. The Al–base alloys are also used for joining ceramics to metal. The Al rich alloys with small amount of alloying element shows the superior strength of Si₃N₄/Si₆N₄ joints. The superior wettabilities and mechanical properties of the alloys are attributable to the improvement of strength for ceramic/metal joint. The physical effect of ultrasound is also applied to joining ceramics to metals.

KEY WORDS: (Wetting) (Work of Adhesion) (Contact Angle) (Interface Structure) (Interface Strength) (Ceramic/Metal Joining) (Ultrasound)

1. Introduction

The understanding of interface phenomena is necessary for ceramic–metal joint and ceramic–fiber containing metal based composite and for brazing or bonding of the ceramic–metal joint in practical engineering application.

The wetting of alumina oxide ceramics by molten metals as interfacial phenomena between ceramics and metals have been investigated.

McDonald and Eberhart have reported that the works of adhesion of molten metals are related with the formation free energies of the metallic oxides1). Since the work of adhesion is defined as the formation energy to make new surface by separating molten metals from ceramics, the value of metals is used as a measure of joining ability. Apart from the formation of oxide at the interface between molten metal and Al₂O₃, the metals with easier oxidizing abilities possess better wettabilities. For instance, the work of adhesion is large for Ti which is easily oxidized. In other words, the active elements such as Ti are used as the elements in brazing fillers for oxide ceramics. The joining strength of Ni alloys with Ti and Y against Al₂O₃ is high2). Si₃N₄ nitride and SiC carbide composed of ionic and covalent bonding have attracted recent interests because of their superior mechanical properties at elevated temperatures.

This paper describes the dominating factors in wetting of Si₃N₄ nitride and SiC carbide by molten metals, also the intermediate phases at ceramic/metal interface and the interface strength of ceramic/metal joint.

2. The role of titanium as active element

Molten copper doesn't wet oxide and non-oxide ceramics though it, which is often used as molten filler metal, well wets metallic materials such as steels. If the wetting of ceramics is improved by alloying elements to copper, the molten copper will be used as the filler metal for joining ceramics to metals.

Figure 1 shows the titanium content dependence of equilibrium contact angle on Si₃N₄ and SiC at 1373 K in vacuum. The molten copper with contact angles below 90 degree is called to be in the wetting state, and begins to spread on the ceramics at the titanium content of 5 at % or more.

The molten metals with 20 at % titanium or more which possess the contact angle below 10 degree also well spread on the ceramics. The titanium content dependence of interface strength Si₃N₄/Si₆N₄ and SiC/SiC joints brazed with amorphous Cu–Ti fillers is shown in Fig. 2, where the strength is evaluated by fracture shearing. The interface strength of joints decreases with increasing titanium content in Cu–Ti fillers. The interface structures of Si₃N₄ and SiC joints brazed with Cu–50 at % Ti at a condition of

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1373K and 1.8ks are shown in Figs. 30 and 4(a), (b), respectively. The Ti rich intermediate phase at Si$_3$N$_4$ side is identified as TiN by X-ray diffraction method. Ti$_6$Si$_3$ silicide is formed in the filler which is composed of $(\gamma + \epsilon)$ Cu-Si with 18 at% Si. The content of Si increases with increasing the brazing temperature. Ti in Cu-Ti alloy reacts with Si$_3$N$_4$ by the following equations (kJ/mol)$^{10}$,

\[
\begin{align*}
S_i N_i(s) + 4Ti(l) & = 4TiN(s) + 3Ti(s) \\
\Delta G &= -639 + 0.652T \\
S_i N_i(s) + 9Ti(l) & = 4TiN(s) + T_b S_i_3(s) \\
\Delta G &= -130.9 + 0.152T
\end{align*}
\]

Ti reacts with Si$_3$N$_4$ and forms TiN nitride and Ti$_6$Si$_3$ silicide. The formed free Si also reacts with Cu. The formation of TiN at the cermets/metal interface, and the superior wetting of molten Cu-Si alloy against Si$_3$N$_4$ and TiN are attributable to the improvement of wetting of molten copper against Si$_3$N$_4$ by the addition of titanium.

The interface structure and X-ray image analysis of element in SiC/Cu-50 at% Ti interface indicate that TiC and Ti$_6$Si$_3$C$_2$ (Ti) carbide, Ti$_5$Si$_3$ and Ti$_3$Si$_2$ silicide are formed at the interface$^{10}$. The excess reaction of Cu-Ti alloy with SiC accounts for the lower strength of SiC joints, compared with Si$_3$N$_4$ joints.

Al$_2$O$_3$ oxide, Si$_3$N$_4$ nitride and SiC carbide are wetted with Ti. The dominating factor in the wetting of Al$_2$O$_3$ is the easiness of bonding of metal and oxygen. On the other hand, the factors against the wetting of Si$_3$N$_4$ and SiC are the easiness of bonding between metal and nitrogen, metal and carbon, and metal and silicon. The metal which possesses the high reactivity shows the superior wetting. In order to suppress the excess reaction of titanium with Si$_3$N$_4$,
the titanium content in Ag–Cu eutectic filler with 60 at % Ag is decreased down to 4.5 at %
by adding 64 selected metal. The wetting of molten copper is improved at the titanium content of 20 at % or more. The joining mechanism of Ag–Cu–Ti alloy with Si₃N₄ is similar to that of Cu–Ti alloy, and TiN and Ti₃Si₂ are formed at the ceramic/metal interface.

Fig. 4 Interface microstructure of SiC/SiC joint brazed with Cu–50 at% Ti alloy at 1373 K for 1.8 ks.

The filler metals containing Sn and In are also reported in order to decrease the brazing temperature and titanium content. The precoating of Ti on SiC causes the Ti content down to 3.8 at % in the brazing of SiC. In order to improve the heat–resistance of ceramic joint brazed, nickel instead of copper is used as a matrix element. Fig. 5 shows the titanium content dependence of interface strength of SiC/SiC joint brazed with Ni–Ti alloys at 1523 K for 1.8 ks. SiC joint with Ni–Ti alloy shows the different dependence of Ti content, compared with SiC joint with Cu–Ti alloy. The microstructure of SiC joint with Ni–50 at % Ti in Fig. 6 indicates that the higher brazing temperature in SiC joint with Ni–Ti alloy causes the uniform distribution of TiC carbide in Ni matrix, compared with that in

Fig. 5 Titanium content dependence of SiC/SiC joint brazed with Cu–50 at% Ti alloy at 1373 K for 1.8 ks.

Fig. 6 Interface microstructure of SiC/SiC joint brazed with Cu–50 at% Ti alloy at 1373 K for 1.8 ks.

SiC joint with Cu–Ti alloy. The species and the distribution of compounds formed are important in the interface strength of ceramic/metal joint. The SiC joint with Ni–Ti filler at elevated temperature represents the superior strength as shown in Fig. 7.

3. The role of Al

The molten Al is used for brazing ceramics. According to McDonald and Eberhart, molten aluminum possesses the high work of adhesion. The interface strength of Al/
Fig. 7 Strength of SiC/SiC joint with Ni-50 mass % Ti at elevated temperatures.

Fig. 8 Temperature dependence of Al on Al₂O₃, ZrO₂, Si₃N₄, and SiC.

Fig. 9 Alloying content dependence of equilibrium Al base alloys on Si₃N₄. Al₂O₃ was measured. As shown in Fig. 8, the molten aluminum improves the wettability against CaO-stabilized ZrO₂, SiC and Si₃N₄ with increasing temperature. The molten aluminum based alloys which also wet Si₃N₄ (Fig. 9) are used as filler metals for joining ceramics. Al rich based alloys with small amounts of alloying elements increases the strength of Si₃N₄/Si₃N₄ joints as shown in Fig. 10.

In Fig. 11 the work of adhesion of Al–Cu alloys against Si₃N₄, Al₂O₃, and ZrO₂ departs to plus values from ideal mixing one. This means that the interface strength of Si₃N₄/Al will be increased by adding Cu to Al, because the work of adhesion gives a measure of interface strength. The mechanical properties of Al–Cu alloys are improved by mixing copper as shown in the microstructure and the copper dependence of hardness of Al–Cu alloys (Fig. 12). The two factors of the interface strength and mechanical properties of the alloys operate in improving mechanical properties of ceramic/metal joint. The dispersive energy rather than the fracture energy of interface works in the ceramic/metal joint from view points of the
Fig. 10 Alloying contact dependence of strength of Si₃N₄/Si₃N₄ joint brazed with Al based Alloys at 1373 K for 3.6 ks.

Fig. 11 Copper content dependence of work of adhesion for Al-1Cu alloys on Al₂O₃, ZrO₂ and 1373 K.

Fig. 12 Hardness and microstructure of Al-Cu alloys.

4. Effect of ultrasound application

The ultrasound has been applied to soldering industry fields[19,20]. The effect of ultrasound application is discussed from the new view points[21]. While the chemical effect of Ti and Al promotes the wetting of ceramics by molten metals, the energy of ultrasound also accelerates to wet ceramics. It was considered that the remove of bubbles from the surface by applying the ultrasound against ceramics. On the other hand, the another active role of ultrasound attracts new attention. The gas confined in defects near surface of ceramics were expanded and removed as bubbles by the irradiation of ultrasound. The bubbles, further, continue to be expanded and compressed by the successive irradiation of ultrasound. The effect of ultrasound called as the cavitation also activates the wetting of molten metals against ceramics.

The practical process of ultrasonic brazing is shown in Fig. 13[19,20]. First, the alumina is metallized in molten Zn-Al alloys, and then it is joined to copper pre-metallized with the same Sn-Al alloys without loading. Fig. 14 represents the time dependence of ultrasound application on the
5. Summary

Joining of ceramics to metals necessitates the knowledge of wetting of molten metals against ceramics, and also the elucidation of dominating factors in interface strength of ceramic/metal joints. The molten metals wets the ceramics with or without the formation of intermediate phases. In wetting of molten metals against ceramics the intermediate phases are often formed at the ceramic/metal interfaces. The molten phases formed also wet the intermediate phases during the wetting process.

The strength or ceramic/metal joints formed is dominated by the interface strength which is evaluated from the work of adhesion of metals, and the size and distribution state of intermediate phases formed during joining.

The those wettability of molten metals against ceramics, necessitates the the improvement of ability of metals for joining ceramic/metals. The improving methods are described as; (1) Alloying metal such as Ti to the filler, which metal possesses the easiness of bonding with nitrogen, carbon or silicon. Further, applying Al base filler metals with the superior wettability against ceramics. In order words the chemical effects of Ti and Al are used in these process. (2) The physical effects of ultrasound are used in the ultrasonic brazing process. The ultrasound accelerates to wet molten metals against ceramics.

References