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STUDIES ON ELECTRON SCATTERING BY MERCURY ATOMS

AND

ELECTRON SPIN POLARIZATION DETECTOR

1977

Yasunori YAMAZAKI

Fundamental laws of Nature do not govern the world as it appears in our mental picture in any very direct way, but instead they control a substratum of which we cannot form a mental picture without introducing irrelevancies.

P.A.M. Dirac

(The Principles of Quantum Mechanics)

Dedicated to my mother

Preface and Acknowledgements

Since N.F.Mott's prediction that unpolarized electrons may undergo considerable spin polarization during scattering with a heavy atom, many experimental and theoretical investigations have been performed in the area of atomic physics. Currently, experiments concerning spin polarization have attracted much attention from various fields of physics, particularly surface physics.

One of the most important considerations in spin polarization experiment is the spin polarization detector, which is markedly inefficient and structurally complex.

In the present study, a polarization detector which utilizes electronatom scattering was systematically investigated and the optimum operation conditions has clearly been determined. For this purpose, electron-mercury scattering was studied in both an experimental and a theoretical view point. The elastic scattering cross section calculated herein has turned out to provide useful information for understanding the generation of Auger electons in solids. Furthermore, the study of the inelastic process leads to intimate insight to plasma physics.

The present paper is comprised of two sections; Part I, which includes Chapter 1-5, concerns the study of the electron-mercury scattering process. Part II, which includes Chapter 6-8, concerns the study of the electron-spin polarization detector which utilizes electron-mercury scattering.

Introducing Part I, Chapter 1 describes general concepts and the history of electron-mercury scattering.

Chapter 2 deals with the theoretical treatment of elastic scattering, based on the partial wave expansion method. The calculations of both the differential cross section and the Sherman function are also included in this chapter for incident electron energies between 300 and 2000 eV.

Chapter 3 discusses the theoretical treatment of inelastic scattering, based on distorted wave Born approximation. The calculation for both the differential cross section and the spin polarization for 6¹P excitation are performed for incident electron energies between 50 and 500 eV.

Chapter 4 is treating the apparatus constructed for observation of the loss-spectra of electron-mercury scattering, together with measured results of incident energies between 300 and 1000 eV and scattering angles between 50° and 110°.

Chapter 5 compares experimental (including the data in Chapter 4) and theoretical (Chapter 3) results for 6 P excitation.

As an introduction to Part II, Chapter 6 generally describes the electron spin polarization detector.

Chapter 7 describes how the optimum conditions for the spin polarization detector were determined using the results of Chapters 2 and 4, and compares it to Mott detector.

Chapter 8 treats the construction of the apparatus for double scattering experiments which allows to perform experiment under the optimum conditions suggested in Chapter 7. Also described in this chapter, is the Pierce type electron gun with a single crystal LaB_6 cathode which was used in the experiment with considerable success and is of most practical use for high power electron beam source.

Research for the present thesis was carried out under the direction of Professor H.Hashimoto of the Department of Applied Physics, Osaka University.

The author wishes to thank Professor H.Hashimoto for the encouragement and stimulus during the course of the research. Several critical suggestions from Professors A. Mitsuishi and I. Shoji of Department of Applied Physics have been most helpful. Suggestions by Professor T.E.Everhart of Univ. of California at Berkeley provided more impetus for an investigation of Pierce type electron gum with single crystal LaB_6 cathode.

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To Associate Professor R.Shimizu, I am very thankful for critical suggestions and systematic discussion of both experiments and theory throughout the present work. The author would also like to express thanks to Dr. K. Ueda for his help with some aspects of the construction of the experimental apparatus and to Mr. Endoh for his advice on computer calculation procedures. I am thankful to my colleagues Mr.M.Shikata for his assistance in the development and successful operation of the Pierce electron gun, Messrs. S. Ichimura and T. Okutani for many stimulating discussions, Miss K.Nishiyama for her typing skill, and all other members of the Hashimoto Laboratory who supported the present work in various aspects.

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PART I ELECTRON-MERCURY SCATTERING

CHAPTER 1 INTRODUCTION

1-1 General Concept of Electron-Mercury Scattering

In low and intermediate energy electron scattering by heavy atoms, electrons are strongly diffracted by an atomic potential because the electron wave length is the same order of magnitude with an atomic radius (see Appendix 1 for detailed discussion). The scattering intensity exhibits apparatent oscillatory features (diffraction pattern) as a function of both the scattering angle and incident electron energy (see Sec.2-5). From a theoretical viewpoint, this means that only a few partial waves contribute to the scattering process, as Arnot (1931) first pointed out. In contrast to atomic potential, spin-orbit interaction is usually very weak, even in electron-heavy atom scattering. However, spin-orbit interaction becomes dominant at a deep minimum of the oscillatory features, at which the effective atomic potential becomes extremely weak. Since spinorbit interaction is non-uniform over azimuthal angles where the z-axis follows the direction of the incident electrons, it would be expected that some effects concerning electron spin polarization take place at the deep minimum of diffraction patterns.

An ensemble of electrons is referred to as polarized if the electrons are unequally populated with respect to the two spin states. The polarization P of the electron ensemble is defined by $P=(N_{\uparrow}-N_{\downarrow})/(N_{\uparrow}+N_{\downarrow})=2\cdot\{(\frac{1}{2})\cdot N_{\uparrow}+(-\frac{1}{2})N_{\downarrow}\}/(N_{\uparrow}+N_{\downarrow})$, twice the expectation value of spin, where N_{\uparrow} and N_{\downarrow} equal the number of electrons with parallel or anti-parallel spin directions respectively in regards to a fixed direction.

1-2 Historical Review of Electron-Mercury Scattering

Since the historic experiment of Franck and Hertz (1914), mercury atoms were often used as a scatterer in early stages of scattering experiments because of their moderate vapour pressure and high atomic number (Z=80), which produces high scattering intensity. Quite a few experiments were performed in systems of various types (see Table 1-1). In the next decade, however, few investigations were carried out because the complicated atomic electron configuration makes theoretical application quite difficult. Success of measurement of electron spin polarization (ESP) by

electron-mercury double scattering (Deichsel 1961) revived experiments concerning electron heavy atom scattering (Kessler 1970 and 1976, and Eckstein 1970, another review papers are summarized at the top of the reference section).

It is widely known that the macroscopic magnetic field cannot orderly align the spin direction of free electrons (see Appendix 2). The detectability and producibility of polarized electrons for free states of electrons was first predicted by Mott (1929, 1932) in application of the relativistic electron theory (Dirac 1928) to double scattering, using Coulomb potential. This treatment predicted the finite ESP for high energy electrons ≥100 keV scattered at a large angle by a gold atom. This condition corresponds to the condition that the spin-orbit interaction is larger or comparable to the electro-static potential.

In regards to the ESP experiment, since Langstroth's early experiment (1932), the first measurement using electron-gold foil double scattering was performed by Shull et al. (1943), where the measured spin polarization amounts to 12% (polarization) at an electron energy of 340 keV. This is in close agreement to Mott's theoretical prediction (10%).

Later, Bartrett and Welton (1941) and Massey and Mohr (1941) proposed that the screening effect on Coulomb potential by atomic electrons played an important role at electron impact energy of lower than 10 keV, and that a large spin polarization could be expected for gold, even at this energy region. Large polarization occurs because of diffraction effect which is referred to in Sec.1-1 and Appendix 1. Deichsel (1961) first detected spin polarization at these low impact energies for mercury double scattering at incident electron energy from 1 to 2 keV, and the maximum polarization was found to be approx. 40% for 1500 eV at a scattering angle of 90°.

Thereafter, numerous experiments were performed and theoretical calculations made for ESP with various scatterers under various scattering conditions (see Tables 1-1, 1-2 and 6-1 for detailed references). In general, close agreement has been obtained for theory and experiment, particularly in elastic scattering of electron-atom system.

Currently, ESP experiments have extended to surface physics in order to investigate the surface states of solids in detail.

On the other hand, a detailed study of the electron impact spectra for mercury has been made by Skerbele et al.(1969), and Skerbele and Lassettre (1972) for a small scattering angle at hundreds eV electron energies, in order to investigate the usefulness of Born approximation (i.e. the utility of the concept as "generalized oscillator strength").

1-3 Bibliographies of the Research of Electron-Mercury Scattering

The bibliographies concerning electron-mercury scattering is summarized in Table 1-1 and Table 1-2 for experiment and theory respectively. ESP experiments concerning electron-atom scattering for atoms other than mercury are also included.

As can be seen in Table 1-1, there is sufficient experimental data for elastic scattering of both the cross section and ESP at various energies and scattering angles. However, few experiments have been performed concerning inelastic scattering, particularly loss spectra at large scattering angles in an intermediate energy region. Experiments for ESP measurements of inelastically scattered electrons are equally scarce.

In regard to theoretical aspects, the case is similar. That is, for elastic scattering, many calculations on both the cross section and ESP have been made, with results comparable to experimental data. In inelastic scattering, however, only calculations for $6^{1}P$ and $6^{3}P$ excitation at low impact energies have been made.

Table 1-1. Bibliographies on experiments of electron-mercury scattering and related experiments.

Hg				Franck and Hertz(1914)
Hg	Forward	10-17 eV	Loss spectra retarding mesh	Davis and Goucher(1917)
Hg	Forward	4.8-10.4 eV	Loss spectra, retarding mesh	Eldridge(1922)
Нg	Forward	threshold-40 eV	σ , inel, loss spectra	Whitney(1929)
Hg	Forward	4-41 eV	σ , inel, loss spectra	Foard(1930)
Hg	5-60°		σ , el, inel.	Armot(1930)
Hg	15-125°	8.6-800 eV	σ, e1.	Arnot(1931)
Ar				Bullard and Massey (1931)
				Pearson and Arnquist(1931)
	90°	1,2,10 keV	P	Langstroth(1932)
He,Ar,Hg	20-160°	23-196 eV	σ , e1, ine1.	Mohr and Nicol1(1932)
Hg	50-120°	80-700 eV	σ , el, inel.	Tate and Palmer(1932)
Hg	Total	8-200 eV	σ , el, inel.	Arnot(1935)
Au	90°	340keV	P, el.	Shull et al.(1943)
Au		194 keV	Mott Detector	Greenberg et al.(1960)
Hg	60-110°	1-2 keV	σ, P, e1.	Deichsel(1961)
Au	30-155°	150-1900 eV	P, el.	Reichert(1963)
Hg	30-150°	900 eV	P, el.	Deichsel(1964)
Hg	30-150°	900-1500 eV	P, e1.	Deichsel and Reichert (1965)
Hg	30-150°	300-700 eV	P, e1.	Steidl et al.(1965)
Hg	25-150°	200-4000 eV	σ, el.	Kessler (1965)
He,Ne,Ar, Kr,Xe,Hg	Forward	20 eV	σ , resonance scattering	Kuyatt et al.(1965)
Hg(solid)	30-150°	300 eV	σ, P, e1.	Loth(1966)

⁻ to be continued -

Нg	30-150°	3.5, 7, 23, 45 eV	σ, P	Deichsel et al.(1966)
Hg	30-150°	180-1700 eV	P, e1.	Jost and Kessler (1966)
Hg	30-150°	100-2000 eV	σ, P,e1.	Eitel(1967)
He,Ne,Ar, Kr,Xe	20-155°	5-1000 eV	P, e1.	Mehr(1967)
Hg	45-135°	46-204 keV	σ , el.	Kessler (1968)
He,Ne,Ar, Kr,Xe	30-150°	40-150 eV	P,el.	Schakert(1968)
Нg		180-900 eV	P,el. influence of plural scattering	Eitel et al.(1968)
Hg	Forward	50-300 eV	σ, loss spectra	Skerbele et al.(1969)
Hg	2.5, 20°	300-500 eV	σ, el., absolute	Bromberg(1969)
Hg	80-140°	6.75 eV	P, e1.	Wilmers et al.(1969)
Hg	95°	6.75 eV	P,ESP-detector	Gehenn et al.(1969)
Hg	20-130°	25,180 eV	σ, P, 6 ¹ P	Eitel and Kessler(1970)
Hg	20-155°	20-300 eV	σ , e1., 6^{1} P	Gronemeier(1970)
Нg	Forward	300-500 eV	6 ¹ P generalized oscillator strength	Skerbele and Lassettre(1970)
Sb ₄	20-150°	50-1000 eV	p	Kessler et al.(1971)
Hg	20-130°	25,30,50,180 eV	P, 6 ¹ P	Eitel(1971)
Нg	Forward	500 eV	inel., absolute generalized oscillator strength	Skerbele and Lassettre(1972)
Hg	20-150°	30-300 eV	σ, P, 6 ¹ P, 6p ^{†3} P	Hanne et al.(1972)
Нg		90-600 eV	6 ¹ P, 6p ³ P generalized oscillator strength	
Hg	30-150°	4-5 eV	σ , resonance scattering	Duweke et al.(1973)
Hg			inel.	Bass (1974)

⁻ to be continued -

Hg			life time 6 ³ P	King and Adams(1974)
Hg	forward	4-10 eV	exchange excitation of 6³P	Hanne and Kessler(1976)
Hg	30-150°	4.4-6.1 eV	σ , P, resonance scattering	Duweke et al.(1976)
Hg			σ , electron impact excitation of $6^{3}P_{0.2}$	Krause et al.(1977)
Хе	20-155°	150-1200 eV	P, el.	Kessler et al.(1977)
Нg	50-110°	300-1000 eV	σ, loss spectra	Yamazaki et al.(1977)

Table 1-2. Bibliographies on the theory of electron-mercury scattering and the related theoretical calculations.

			application of Dirac theory to scattering	Darwin(1928)
Hg	Total	6.7-40 eV	σ, inel	Penny(1932)
Au	90°	0.1-150 keV	P,el. screened Coulomb	Massey and Mohr(1941)
Hg		100,230 keV	$\sigma_{f ,}$ el. Hartree	Bartlett and Welton (1941)
Hg	30-180°	1.95-121 keV	σ, P	Mohr(1954)
Au	30-150°	150MeV		Yennie et al.(1954)
Au,Cd,Hg	15-165°	20-650 keV	σ ,P,el. Coulomb pot.	Sherman(1956)
Au,Al	0-180°	75,121 keV	σ ,P,el. screened Coulomb	Sherman and Nelson(1959)
Hg	0-180°	1-2 keV	σ ,P,el. rel. Hartree pot.	Bunyan(1963)
		,	σ ,P,el. Coulomb pot.	Gluckstern and Lin(1964a)
			σ,P,el. Coulomb pot.	Gluckstern and Lin(1964b)
Hg,Au,Cu	10-170°	50-400 keV	σ ,P,el. screened Coulomb	Lin(1964)
Au,Hg		0.2-290 keV	σ ,P,e1.	Holzwarth and Meister(1964a,b)
			quadratic correction of the potential	Bühring(1965)
			power series expansion	Bühring(1965)
Hg	30-150°	100-2000 eV	rel.Hartree ø,P,el.	Bunyan (1965)
Hg,Au,Bi		10-500 eV	σ ,P,el. calculation of Hartree pot.	Schonfelder(1966)
			rel.effect	Spruch(1966)
			rel.effect	Rotenberg(1966)
			rel.effect	Browne and Bauer(1966)
Hg,Au,Bi	30-150°	10-500 eV	σ,P,e1.	Schonfelder(1967)

-to be continued-

			rela. effect	Dawson(1967)
Z=1-54		10-100 keV	o, e1.	Cox(1967)
Hg	0-180°	7-180 eV	rel.effect σ ,P	Meister(1968)
Hg	Total	6.7-200 eV	σ , oscillator strength	McConnel and Moiseiwitsch (1968)
Hg	30-150°	20eV-150 keV	σ , rel.effect	Yates and Strand(1968)
Hg	45-180°	46-204 keV	σ, e1.	Bühring(1968)
Hg		100-2000 eV	P, el.complex scattering amplitude	Bühring(1968)
Hg			tests of atomic pot.	Yates and Fink(1969)
Hg		3.5-500 eV	σ , P,el. influence of rel. and exchange	Walker(1969)
Hg,Ar	0-180°	3.5-8 eV	σ ,P,el. influence of atomic polarization	Weiss(1969)
Нg			σ ,el. influence of inelastic channel	Mohr(1969)
H,He.C,Ne, Ar,Kr,Rb, Xe,Cs,Au, Hg,Pb,Bi		25-800 eV	rel.Hartree-Fock-Slater	Fink and Yates(1970-a)
		100-1500 eV		Fink and Yates(1970-b)
Hg		3.5-100 eV	σ ,P,e1. influence of distortion	Walker(1970)
Hg	0-180°	25-180 eV	σ ,P, 6^{1} P DWB approx.	Madison and Shelton(1973)
Li,Na,Mg, P,K,Ca,Ga, Br,Sr,Mo, Rh,Cd,Ba, W,Os		25-1500 eV 100-1500 eV	rel. Hartree-Fock- Slater pot.	Gregory(1974) (1970)

Hg	30-150°	300-2000 eV	σ ,P.el. optimum condition of ESP detector	Yamazaki et al.(1976)
Hg	Forward		$\sigma_{\rm ex}$, P, 6^3 P	Hanne(1976)
Hg	Forward	4-12eV	σ ,6 ¹ P, Born-Okhur	Moiseiwitsch(1976)
Нg	0-180°	300-2000 eV	σ,P non-rel.Hartree	Yamazaki et al.(1977)
Hg	0-180°	50-500 eV	σ ,P,6 ¹ P DWB	Yamazaki et al.(1977)

CHAPTER 2 THEORY OF ELECTRON-MERCURY ELASTIC SCATTERING ---- MODIFICATION AND EXTENTION OF CURRENT THEORY

2-1 Introduction

This chapter views elastic scattering theoretically employing partial wave expansion, for which detailed calculation procedures applicable to computer use have been developed by many authors (see Table 1-1). Calculation has been made for energy regions not studied previously using an accurate and fast calculation procedure developed for high speed digital computer (Yamazaki et al. 1976 and 1977). The theories are generally formulated for use in Chapter 3.

2-1-1 Necessity of Relativistic Treatment

In theoretical treatment of electron heavy atom scattering, particular points should be noted. First, the system should be treated relativistically even in the non-relativistic energy regions of incident electrons. This may be interpreted qualitatively as follows; The atomic potential attracts electrons and because of a high Z number, is very strong. The electrons passing through near a nucleus may be accelerated to near light velocity, which in turn necessitates relativistic correction of the electron mass as a distance function between the electron and nucleus.

Table 2-1. Comparison of phase shift calculated relativistically and non-relativistically for Hg and Ar (Meister and Weiss 1968).

	Hg 45 eV				Ar 40 eV			
relativistic		tic	nonrelativistic		relativistic		nonrelativistic	
1	δ_l	δ_{-l-1}	δ_l	δ_{-l-1}	δ_l	δ_{-l-1}	δ_l	δ_{-l-1}
0	-1.304		-0.361		0.386		0.402	
1	-1.364	-0.981	-0.568	-0.192	1.214	1.230	1.206	1.231
2	-0.746	-1.010	-0.719	-0.641	1.247	1.247	1.240	1.240
3	0.730	-1.104	0.798	0.810	0.172	0.163	0.171	0.163
4	0.255	0.080	0.296	0.296	0.041	0.042	0.041	0.041

The differences between relativistic and non-relativistic treatments have been calculated for mercury by Meister and Weiss (1968). The phase shifts and ESP of these results are shown in Table 2-1 and in Fig.2-1. In Table

2-1, we see that the 0-th order relativistic phase shift differs considerably from that of the non-relativistic. This difference lessens for large l because of a small mass correction. Apparent differencies of ESP are recognized in very low energies as well.

The above consideration may also lead to a theoretical explanation of the seemingly contradictory phenomena that the behaviour of apparently relativistic electron (electron energy of up to 100 keV) can be explained by Schrödinger's non-relativistic equation by modifying the electron rest mass by incident electron energy. This treatment is commonly used in high voltage electron microscopy and has explained various phenomena with considerable success(M.von Laue 1948, Fujiwara 1961 and Hashimoto et al. 1964). This is because the electron mass is not greatly affected by the atomic field in high energy regions. That is, the Hamiltonian H_{rel} and H_{rol} for relativistic and non-relativistic cases respectively, are written

$$H_{rel} = \sqrt{1 + p^2 + V(r)}$$
 (2-1)

$$H_{non} = p^2/2 + 1 + V(r) , \qquad (2-2)$$

where the system of units is natural unit (see Sec.2-2). From the uncertainity principle,

$$\Delta p \cdot \Delta r \sim 1$$
 (2-3)

In simplification $V(r) = -Z e^2/r$, the minimum energy H_{rel}^{min} and H_{non}^{min} is estimated as

$$H_{rel}^{min} = \sqrt{1 - Z^2 e^4}$$
 (2-4)

$$H_{non}^{min} = 1 - Z^2 e^4/2 . (2-5)$$

These values amount to e.g. H_{rel}^{min} =2.304 keV and H_{non}^{min} =2.299 keV for aluminum, and H_{rel}^{min} =30.99 keV and H_{non}^{min} =30.05 keV for silver. The H_{non}^{min} may be regarded as the maximum modified kinetic energy ΔE of an electron, due to the atomic field. If one takes into account that the electron microscope uses only forward scattering, i.e., uses mainly electrons scattered distant from the nucleus, it is seen that the above value for ΔE is overestimated. Thus, it may be concluded that the electron mass modified by the incident electron energy is nearly constant during scattering.

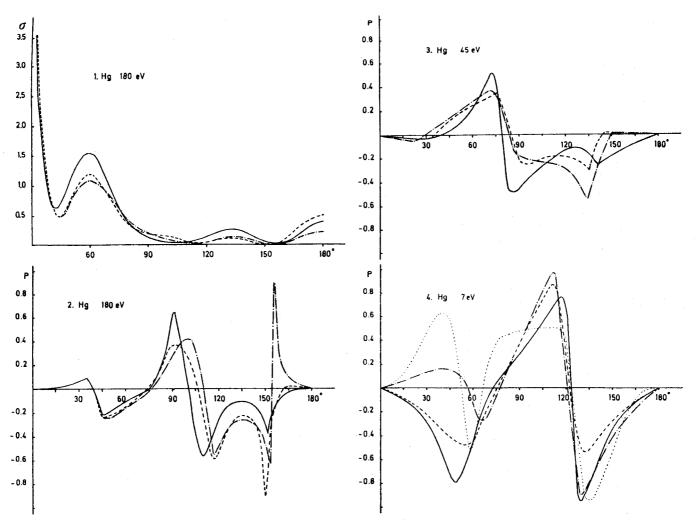


Fig. 2-1. The comparison of the relativistic and non-relativistic calculation of the differential cross section σ and spin polarization P (——relativistic and ----- non-relativistic calculation with Mayer's potential, relativistic and ——non-relativistic calculation with Froese potential) (Meister and Weiss 1968).

It should be noted, however, that because of large mass corrections and effect of spin, large angle scattering for heavy atoms need to be treated with the proper relativistic method in even hundreds keV energy regions(e. g. for mercury $H_{rel}^{min} = 96.11$ keV and $H_{non}^{min} = 87.07$ keV).

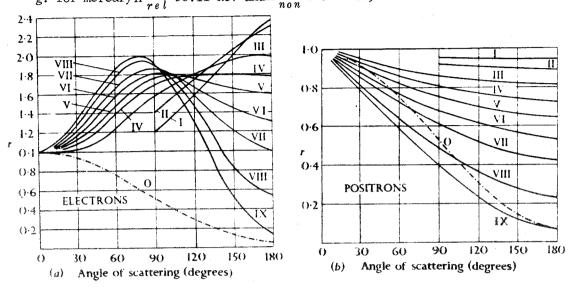


Fig. 2-2. Angular distributions (a) of electrons and (b) of positrons of various energies scattered by mercury nuclei. The scattered intensity is given as the ratio r to that given by the formula

$$\frac{Z^2 e^4}{4 v^4} \cdot \frac{1}{\sin^4(\theta/2)} \cdot (1 - v^2/c^2)$$

Curves I-IX respectively correspond to particles of energies 23, 44, 74, 119, 160, 237, 340, 654, 1712 keV. Curve 0 is that given by the approximation formula (2-27) for an energy of 1712 keV (Mott and Massey 1965).

Fig. 2-2 shows the cross section for electrons and positrons normalized by the ordinary Rutherford scattering cross section. It shows that at high incident energy and large scattering angle the effect of spin becomes important (The effect of spin is discussed in Appendix 3 using Born approximation). For positron, Born-like behaviour appears clearly than for electron, this may be due to the repulsive force between the positron and nucleus (see also Appendix 1).

The occurrence of ESP(electron spin polarization) is a direct consequence of the interaction of the magnetic moment of electrons and the magnetic field induced by the atomic field. Charged particles travelling in a static-electric field "feel" the magnetic field which is written

$$\mathbf{H} = -\mathbf{v} \times \mathbf{E},\tag{2-6}$$

where \mathbf{v} the velocity of the charged particles and \mathbf{E} the electric field of the atom. The interaction energy $\mathbf{\varepsilon}$ is expressed as

$$\begin{split} \boldsymbol{\varepsilon} &= - \, \boldsymbol{\mu} \, \cdot \, \boldsymbol{\mathsf{H}} \\ &= - \, \boldsymbol{e} \, \cdot \, \boldsymbol{\mathsf{S}} \cdot \, \left(\, \boldsymbol{\mathsf{v}} \, \times \, \boldsymbol{\mathsf{H}} \right) \, \cdot \, \frac{1}{\boldsymbol{e} \, r} \cdot \frac{\mathrm{d} \, \boldsymbol{V}}{\mathrm{d} \, r} \\ &= \frac{1}{r} \frac{\mathrm{d} \, \boldsymbol{V}}{\mathrm{d} \, r} \, \, \boldsymbol{\mathsf{L}} \cdot \boldsymbol{\mathsf{S}} \, , \end{split} \tag{2-7}$$

where μ is the magnetic moment of electron, e the charge of electron, L the orbital angular momentum and S the spin angular momentum. This term is called spin-orbit interaction which changes its sign in accordance with the direction of the spin or orbital angular momentum, causing ESP of initially unpolarized scattered electrons or initially polarized electrons to be scattered asymmetrically. On the other hand, we can obtain

$$E\psi = \left(\frac{\mathbf{p}^2}{2} + V(r) - \frac{\pi}{2} \nabla^2 V(r) + \frac{1}{2r} \frac{dV}{dr} \mathbf{L} \cdot \mathbf{S}\right) \psi , \qquad (2-8)$$

as the non-relativistic approximation of Dirac equation (Foldy et al.1950). The 1st and 2nd terms are that of the ordinary Schrödinger Hamiltonian, and the 3rd term the so-called Darwin term, which originates from the Zitterbewegung. The 4th term is the spin-orbit term in question, which agrees with that of equation (2-7) with the exception of factor 2, which is called Thomas factor (Thomas 1927). Since the electron spin effects Hamiltonian through primarily the spin-orbit term (see equation (2-8)), the above model may provide valuable insight regarding the origin of ESP. In order for a large spin polarization to occur, the atomic potential V(r) needs to be relatively small in comparison to the spin-orbit interaction. Such a condition might be to occur 1) at the minimum points of diffraction pattern of the cross section (This condition requires that incident electron energy should be low enough (e.g. lower than several keV for mercury) in order for diffraction phenomena to occur during scattering. see

Sec.1-1 and Appendix 1 , 2 at large scattering angle in order to make the factor dV/dr in equation (2-8) large because impact parameter becomes small at large scattering angle and 3) for atoms of large Z-number because $1/r \cdot dV/dr$ becomes comparable to or larger than V at the minimum distance between electron and nucleus (see equation (2-9)).

In these energy regions, only the partial waves of lower order contribute to scattering. Therefore, the partial wave expansion method may incur reasonable success for calculation of cross section and spin polarization.

2-1-3 Choice of the Atomic Potential

In theoretical treatment of electron-atom scattering, important consideration is the choice of the atomic potential. Due to the complexity of electron configuration, particularly for heavy atoms, several models based on various grades of approximation have been developed (as summarized in Table 2-2).

Table 2-2. Various calculation method of atomic potential.

	without exchange	with exchange
statistical model	analytical expression of T-F (Tietz 1962, Byatt 1957)	analytical expression of T-F-D (R.A.Bonham et al.,1963) Atomic energy level by T-F and T-F-D (R.Latter, 1955) Consideration on exchange effect (P.A.M.Dirac 1930)
self-consistent model	R-H (J.L.Schonfelder 1966) analytical expression of N-R-H (T.Tietz 1962, Byatt 1957) R-H (S.Cohen 1960, D.F.Mayers 1960)	R-H-F-S (D.Liberman et al. 1965) approximate treatment of exchange effect (V.W.Maslen 1956, J.C.Slater 1951)

Since the schematic Hamiltonian is represented by equations (2-1) and (2-2), the distance between the (1s) atomic electrons and the nucleus is estimated as:

$$r_{rel}^{min} \sim \sqrt{1/Z^2 e^4 - 1}$$
 (2-9)

$$r_{non}^{min} \sim 1/Z e^2 \qquad , \tag{2-10}$$

respectively, based on the uncertainity principle. This means that an incorporation of relativity in the calculation of atomic potentials results in greater screening and reduces both the phase shift and scattering cross section.

The ratio of the binding energy calculated relativistically to that non-relativistically is shown in Table 2-3-a (Boyd et al. 1963). The ratio for inner electrons such as (1s) or (6s) is greater than 1, which means that the attractive force becomes stronger in the relativistic case. On the other hand, the ratio for outer electrons such as (4f) and (5d) is smaller than 1, which means greater screening of the nuclear field in the relativistic case.

Table 2-3-a. Ratio of relativistic to non-relativistic eigenvalues for several electron shells. (Boyd et al. 1963)

	1s	4f	5 <i>d</i>	6s
₂₆ Fe	1.008	• • •		
74W	1.09	0.81	0.84^{a}	1.16
78Pt	1.10	0.86	0.88	1.27
80Hg	1.11	0.87	0.84	1.20
92U	1.15	0.91	0.95	1.34

On the other hand, the relativistic treatment of incident electrons increases the phase shift of the lower order according to a similar consideration, i.e. the attractive force in a relativistic treatment is greater than that in non-relativistic treatment.

The incorporation of exchange interaction between atomic electrons lowers the energy of the electron level, increases the screening, and reduces the phase shift (see Sec.2-3). However, the exchange interaction between incident and atomic electrons acts as an attractive force, thus increases the phase shift.

Table 2-3-b. Comparison of phase shift for mercury (Walker 1969) (H, no exchange, Hartree potential; H-F, no exchange, Hartree-Fock potential; Exchange, Hartree-Fock potential with exchange. All phases are modulo π .).

Energy	l	Sn	in up		Spin	down	
(ev)	•	Н	H-F	Exchange	Н	H-F	Exchange
3.5	. 0	0.86	0.15	1.35			
	1	0.30	0.01	1.00	0.50	0.12	1.32
	2	0.53	0.06	0.03	-0.75	0.06	0.04
	2 3	0.01	0.00	0.01	0.01	0.00	0.01
45	0	-1.09	-1.44	-1.01			
	1	-0.58	-0.94	-0.48	-0.28	-0.65	-0.20
	2	-0.67	-1.18	-0.51	-0.59	-1.09	-0.44
	2 3	0.92	0.51	1.07	0.93	0.52	1.07
	4	0.30	0.18	0.26	0.30	0.18	0.26
	4 5	0.12	0.07	0.09	0.12	0.07	0.09
	6	0.05	0.03	0.04	0.05	0.03	0.04
	7	0.02	0.01	0.01	0.02	0.01	0.01
300	0	-0.24	-0.46	-0-26			
	1	0.60	0.37	0-58	0.90	0.67	0.88
	2 3	1.26	1.00	1.23	1.34	1.07	1.30
	3	1.56	1.23	1.49	-1.56	1.26	1.51
	4 5	-1.21	-1.52	-1.36	-1.21	-1.52	-1.35
	5	0.99	0.79	0.84	1.00	0.79	0.83
	6	0.60	0.45	0.48	0.60	0.45	0.47
	7	0.39	0.28	0.30	0.39	0.28	0.29
	8	0.26	0.19	0.19	0.26	0.19	0.19
	9	0.18	0.12	0.12	0.18	0.12	0.12

Moreover, the electric field of the incident electron may distort the atomic potential, which in turn causes a long range attractive force for the incident electron. The calculated phase shifts for the various approximations are shown in Table 2-3-b which confirm the qualitative interpretation given above. That is, for lower order phase shifts (l < 3), the Hartree potential without exchange and Hartree-Fock potential with exchange comply well because of opposite effects in the two exchange interactions. For a higher order of phase shift(l > 7), Hartree-Fock potential without exchange and Hartree-Fock potential with exchange agree satisfactory. This occurs because the largest principal quantum number of

mercury is 6, and partial wave from \$l > 6\$ have little exchange interaction with atomic electrons. The difference between the Hartree potential without exchange and the Hartree-Fock potential with exchange for a higher order of partial waves is not negligible but is small and affects only at forward scattering. Therefore, the former model with relativistic treatment, despite its simplicity, is considered to give accurate results. Atomic distortion is not thought to notably affect the electron-mercury scattering at intermediate energies (Walker 1970),* thus is not considered in the present study.

Among various available expressions of atomic potentials, an analytical expression is most convenient for the present calculations. We have therefore used the non-relativistic Hartree potential, analytically expressed by Byatt(1956). The present calculation agree well with those obtained using Mayer's relativistic potential(1957, see Sec.2-4)**

^{*} A recent report on e-Xe elastic scattering (Kessler 1970) implies that exchange scattering has relevance until 700 eV, and atomic distortion should be taken into account using the polarized orbital methods at 150 eV.

^{**} The effects of and the relation between relativistic and non-relativistic equation, and relativistic and non-relativistic atomic potential are discussed by several authors (Spruch 1966, Rotenberg 1966, Browne 1966 and Meister and Weiss 1968). It was concluded as a vital point that one should perform relativistic and non-relativistic calculation using relativistic and non-relativistic potentials, respectively (Walker 1971). However, as is shown in Sec.2-5, the combination of relativistic treatment and non-relativistic potential gives good results in the energy region under consideration here.

2-2 Born Approximation

2-2-1 Integral Expression of Dirac Equation

The Dirac equation in common expression is written as

$$W\psi = - (\mathbf{a}\,\mathbf{p} + \beta + V)\,\psi \qquad (2-11)$$

where

$$\mathbf{a} = \begin{pmatrix} 0 & \sigma \\ \sigma & 0 \end{pmatrix} \tag{2-12}$$

$$\beta = \begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} , \qquad (2-13)$$

 σ the Pauli matrix, * W the total energy, \mathbf{p} the momentum, V the atomic potential energy and ψ the four component spinor. The system of units is so-called natural unit, in which c=m=K=1, where c is the light velocity, m the electron rest mass and K the Planck's constant devided by 2π . The unit of various quantity is tabulated in Table 2-4.

Table 2-4. Unit of various quantities in natural unit.

	unit	value
energy	mc ²	8.1 x 10 ¹⁴ joul.
length	th/mc	4.0×10 ¹³ m
charge	hc/m	1.8 × 10 ¹⁸ coul.
time	th /mc²	1.2 ×10 ²¹ sec.

*
$$\sigma_x = \begin{pmatrix} 0 & 1 \\ 1 & 0 \end{pmatrix}$$
 $\sigma_y = \begin{pmatrix} 0 & i \\ i & 0 \end{pmatrix}$ $\sigma_z = \begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix}$

The formal solution of the wave equation $H \psi_j = W_j \psi_j$ is written either explicitly as

$$\phi_{j}^{(\pm)} = \boldsymbol{\varphi}_{j} + \frac{1}{W_{j} - H \pm i \varepsilon} V \boldsymbol{\varphi}_{j} , \qquad (2-14)$$

or implicitly as

$$\boldsymbol{\psi}_{j}^{(\pm)} = \boldsymbol{\Phi}_{j} + \frac{1}{W_{j} - K \pm i \, \epsilon} \, V \boldsymbol{\psi}_{j}^{(\pm)} \tag{2-15}$$

$$K = H - V \tag{2-16}$$

K is not necessarily kinetic energy and ϕ_j satisfies $K\phi_j = W_j \phi_j$. The sign + or - represents the asymptotic conditions which correspond to outgoing or incoming scattered states, respectively. Equation (2-15) is called the Lippmann-Schwinger equation (Lippmann and Schwinger 1950 and Gell-Mann and Goldberger 1953).

The equation (2-15) can be rewritten as follows; The operator $1/(W-K\pm i\,\epsilon)$ is defined as

$$(W-K\pm i\,\varepsilon\,)\cdot 1/(W-K\pm i\,\varepsilon)=1, \qquad (2-17-a)$$

$$1/(W-K\pm i\,\epsilon)\cdot(W-K\pm i\,\epsilon)=1$$
, (2-17-b)

and

$$W-K\pm i\,\varepsilon = W + (\mathbf{a}\mathbf{p} + \boldsymbol{\beta}) + i\,\varepsilon$$

$$= \begin{pmatrix} W+1\pm i\,\varepsilon & \sigma \cdot \mathbf{p} \\ \sigma \cdot \mathbf{p} & W-1\pm i\,\varepsilon \end{pmatrix},$$
(2-18)

so

$$1/(W-K\pm i\,\varepsilon) = 1/((W\pm i\,\varepsilon)^{2}-\mathbf{p}^{2}-1)\begin{pmatrix} W-1\pm i\,\varepsilon & -\sigma\cdot\mathbf{p} \\ -\sigma\cdot\mathbf{p} & W+1\pm i\varepsilon \end{pmatrix}$$
$$= (W-\mathbf{a}\,\mathbf{p}-\beta)/(W\pm i\,\varepsilon)^{2}-\mathbf{p}^{2}-1), \qquad (2-19)$$

which can be easily proven by direct substitution. Equation (2-15) results in

$$\boldsymbol{\psi}_{j}^{(\pm)} = \boldsymbol{\varrho}_{j} + \frac{W - \mathbf{a} \, \mathbf{p} - \beta}{(W \pm i \, \varepsilon)^{2} - \mathbf{p}^{2} - 1} \quad V \boldsymbol{\psi}_{j}^{(\pm)} . \tag{2-20}$$

Using the relation,

$$\iint e^{-i\mathbf{k}\cdot(\mathbf{r}-\mathbf{r}')} d\mathbf{k} d\mathbf{r}' = (2\pi)^3 \int \delta(\mathbf{r}-\mathbf{r}') d\mathbf{r}' = (2\pi)^3, \qquad (2-21)$$

the second term of the right hand side of equation (2-20) can be transformed as

$$(W - \mathbf{a} \mathbf{p} - \beta) / ((W \pm i\varepsilon)^{2} - \mathbf{p}^{2} - 1) V (\mathbf{r}) \psi_{j}^{(\pm)}(\mathbf{r})$$

$$= (W - \mathbf{a} \mathbf{p} - \beta) / ((W \pm i\varepsilon)^{2} - \mathbf{p}^{2} - 1) \int \delta (\mathbf{r} - \mathbf{r}') d\mathbf{r}' V (\mathbf{r}) \psi_{j}^{(\pm)}(\mathbf{r})$$

$$= \frac{1}{(2\pi)^{3}} \iint \frac{W - \mathbf{a} \mathbf{p} - \beta}{(W \pm i\varepsilon)^{2} - \mathbf{p}^{2} - 1} e^{i\mathbf{k} \cdot (\mathbf{r} - \mathbf{r}')} V (\mathbf{r}') \psi_{j}^{(\pm)} (\mathbf{r}') d\mathbf{k} d\mathbf{r}'$$

$$= \frac{1}{(2\pi)^{3}} \iint \frac{W - \mathbf{a} \mathbf{p} - \beta}{(W + i\varepsilon)^{2} - K^{2} - 1} e^{i\mathbf{k} \cdot (\mathbf{r} - \mathbf{r}')} V (\mathbf{r}') \psi_{j}^{(\pm)} (\mathbf{r}') d\mathbf{k} d\mathbf{r}',$$
 (2-22)

where $K = |\mathbf{k}|$

Using the residue theorem, the integrations of the variable ${\bf k}$ can be performed and gives

$$\frac{1}{(2\pi)^3} \int \frac{e^{i \mathbf{k} \cdot (\mathbf{r} - \mathbf{r}')}}{(W \pm i \, \epsilon)^2 - K^2 - 1} \, d \, \mathbf{k} = -\frac{1}{4\pi} \frac{e^{\pm i \sqrt{W^2 - 1} \, | \, \mathbf{r} - \mathbf{r}' \, |}}{|\, \mathbf{r} - \mathbf{r}' \, |} . \tag{2-23}$$

Equation (2-20) results in

where $K = \sqrt{W^2 - 1}$, $\mathbf{k}_f = K^{\bullet p} r$ and $r = |\mathbf{r}| \cdot$ The final expression of equation (2-24) is obtained assuming the usual scattering condition $|\mathbf{r}| \gg |\mathbf{r}|$ (see Fig.2-3).

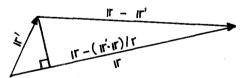


Fig. 2-3. Relation of r and r'.

Equation (2-24) is the integral form of the relativistic Dirac equation (2-11). From equation (2-24), the scattering amplitude for the usual outgoing wave boundary condition is written

$$f(\theta) = -\frac{1}{4\pi} (W - \mathbf{a} \mathbf{k}_f - \beta) \int e^{-i \mathbf{k}_f \cdot \mathbf{r}'} V(\mathbf{r}') \psi_j^{(+)}(\mathbf{r}') d\mathbf{r}'. \tag{2-25}$$

Note that equation (2-25) represents the exact scattering amplitude for Dirac electrons.

2-2-2 Born Approximation

In order to obtain an approximation of the scattering amplitude, the $\psi_j^{(+)}$ appearing in the right hand side of equation (2-25) is replaced by $\pmb{\varPhi}_j$. This approximation is called the first Born approximation

$$f_{Born}(\theta) = -\frac{1}{4\pi} (W - \mathbf{a} \mathbf{k}_f - \beta) \int e^{-i \mathbf{k}_f \cdot \mathbf{r'}} V(\mathbf{r'}) \Phi_j(\mathbf{r'}) d\mathbf{r'}, \qquad (2-26)$$

For Coulomb potential $-Z\,e^2/r$, equation (2-26) produces the ordinary Rutherford formula with correction factors (see Appendix 3).

$$(d\sigma/dQ)_{Born} = \frac{Z^2 e^4}{4 v^4 \sin^4(\theta/2)} \cdot (1 - v^2 \cdot \sin^2(\theta/2)) \cdot (1 - v^2) \qquad (2-27)$$

The first factor of equation (2-27) is that of the classical Rutherford formula, the second is that originating from the spin of electrons (see Appendix 3) and the third is the mass correction term.

It is of note that the scattering amplitude of first Born approximation gives zero spin polarization as is also shown in Appendix 3. Thus, a calculation on spin polarization of high energy electrons is often performed using second Born approximation (Walker 1971).

2-3. Partial Wave Expansion

For a central field of force we may separate equation (2-11) by polar coordinates. Substitution of $\psi = \begin{pmatrix} -ifX_{-\kappa}\mu \\ g & X_{\kappa}\mu \end{pmatrix}$ gives (Rose 1957)

$$\begin{cases}
-iX_{-\kappa,\mu} & [(W-V+1) f - dg/dr - (\kappa+1) \cdot g/r] \\
X_{\kappa,\mu} & [(W-V-1) g + df/dr - (\kappa-1) f/r]
\end{cases} = 0,$$
(2-28)

where f and g are radial wave function and

$$X_{\kappa,\mu} = \sum_{m} C(l, \frac{1}{2}, j; m, \mu - m) Y_{lm} \psi_{\frac{1}{2}, \mu - m}.$$
 (2-29)

with

$$\mu - m = \pm \frac{1}{2}$$
 (2-30-a)

$$j = |\kappa| - \frac{1}{2} \tag{2-30-b}$$

$$l = \begin{cases} \kappa & \kappa > 0 \\ -\kappa - 1 & \kappa < 0 \end{cases}, \qquad (2-30-c)$$

 $C(l, \frac{1}{2}, j; m, \mu-m)$ is the Clebsch-Gordan coefficient, the detailed form of which is shown in Table 2-5, where Y_{lm} is the spherical harmonics and $\psi_{\frac{1}{2}, \mu-m}$ the spin function. As the asymptotic forms of these four components are related with one another, it suffices to treat only the lower part of equation (2-28) (Mott and Massey 1965). Hereafter this two component spinor is referred to as ψ unless otherwise noted.

Table 2-5. Clebsch-Gordan coefficients $C(j_1,1/2,j;m-m_2,m_2)$.

j=	$m_2 = 1/2$	$m_2 = -1/2$	
j ₁ +1/2	$[(j_1+m+1/2)/(2j_1+1)]^{1/2}$	$[(j_1-m+1/2)/(2j_1+1)]^{1/2}$	
j ₁ -1/2	$-[(j_1-m+1/2)/(2j_1+1)]^{1/2}$	$[(j_1+m+1/2)/(2j_1+1)]^{1/2}$	

Thus, the general solution of equation (2-28) in the polar coordinate system is expressed as

$$\psi = \sum_{\kappa\mu} a_{\kappa\mu} g_{\kappa} X_{\kappa\mu}$$

$$= \begin{cases}
\sum_{l=1}^{\infty} \sum_{\mu} a_{l\mu} g_{l} C(l, \frac{1}{2}, l-\frac{1}{2}; \mu-\frac{1}{2}, \frac{1}{2}) Y_{l,\mu-\frac{1}{2}} + \\
\sum_{l=1}^{\infty} \sum_{\mu} a_{l\mu} g_{l} C(l, \frac{1}{2}, l-\frac{1}{2}; \mu+\frac{1}{2}, -\frac{1}{2}) Y_{l,\mu+\frac{1}{2}} + \\
\sum_{l=0}^{\infty} \sum_{\mu} a_{-l-1} , \mu g_{-l-1} C(l, \frac{1}{2}, l+\frac{1}{2}; \mu-\frac{1}{2}, \frac{1}{2}) Y_{l,\mu+\frac{1}{2}} + \\
\sum_{l=0}^{\infty} \sum_{\mu} a_{-l-1} , \mu g_{-l-1} C(l, \frac{1}{2}, l+\frac{1}{2}; \mu-\frac{1}{2}, \frac{1}{2}) Y_{l,\mu+\frac{1}{2}} \\
\sum_{l=0}^{\infty} \sum_{\mu} a_{-l-1} , \mu g_{-l-1} C(l, \frac{1}{2}, l+\frac{1}{2}; \mu+\frac{1}{2}, -\frac{1}{2}) Y_{l,\mu+\frac{1}{2}}
\end{cases}$$
(2-31)

From equation (2-28), the radial equation with respect to g can be easily derived as

$$\frac{\mathrm{d}^2 g_{\kappa}}{\mathrm{d} r^2} + \left(\frac{2}{r} - \frac{a'}{a}\right) \frac{\mathrm{d} g_{\kappa}}{\mathrm{d} r} + \left\{ab - \frac{\kappa (\kappa + 1)}{r^2} + \frac{\kappa}{r} \frac{a'}{a}\right\} g_{\kappa} = 0, \quad (2-32)$$

where a = W - V + 1, b = W - V - 1 and a' = da/dr. For $r \rightarrow \infty$, equation (2-32) reduces to

$$\frac{\mathrm{d}^{2}g_{\kappa}}{\mathrm{d}r^{2}} + \frac{2}{r} \frac{\mathrm{d}g_{\kappa}}{\mathrm{d}r} + \left(K^{2} - \frac{l(l+1)}{r^{2}}\right)g_{\kappa} = 0 \qquad (2-33)$$

where $K^2 = W^2 - 1$. Since this differential equation is that of spherical Bessel function, the solution may be represented as follows;

$$g_{\kappa \to \infty} \sim l^{(Kr) \cdot \cos(\delta_{\kappa}) - n} l^{(Kr) \cdot \sin(\delta_{\kappa})}$$

$$\sim (Kr)^{-1} \sin(Kr - \pi/2 \cdot l + \delta_{\kappa}). \qquad (2-34)$$

where \mathbf{j}_l and \mathbf{n}_l are spherical Bessel and spherical Neumann function respectively and $\boldsymbol{\delta}_{\kappa}$ is called the phase shift.

Corresponding to the two initial spin states with respect to z-axis, the scattering states are written

$$\psi \sim \left(e^{i\mathbf{k}\cdot\mathbf{r}} + f_{\uparrow}(\theta', \phi') e^{iKr}/r\right)$$

$$g_{\uparrow}(\theta', \phi') e^{iKr}/r$$

$$q_{\downarrow}(\theta', \phi') e^{iKr}/r$$

$$\left(e^{i\mathbf{k}\cdot\mathbf{r}} + f_{\downarrow}(\theta', \phi') e^{iKr}/r\right)$$

$$(2-35)$$

and

where f and g are called direct and spin-flip scattering amplitude, respectively. From the comparison between equation (2-31) and equation (2-35), $a_{\kappa,\mu}$ is fully determined as

$$a_{l,\mu}^{=-4\pi(l-\mu+1/2)^{\frac{1}{2}}} (2l+1)^{-\frac{1}{2}} e^{i(\delta_{l}+\pi/2\cdot l)} Y_{l,\mu-\frac{1}{2}}^{*} (\theta,\phi) (2-37-a)$$

$$a_{-l-1,\mu} = 4\pi \left(l + \mu + \frac{1}{2}\right)^{2} \left(2 l + 1\right)^{-\frac{1}{2}} e^{i \left(\delta_{-l-1} + \pi/2 l\right)} Y_{l,\mu-\frac{1}{2}}^{*} \left(\theta,\phi\right),$$
(2-37-b)

for spin-up initial state, and from equations (2-31) and (2-36)

$$a l, \mu = 4\pi (l + \mu + \frac{1}{2})^{\frac{1}{2}} (2 l + 1)^{-\frac{1}{2}} e^{i (\delta_l + \pi/2 \cdot l)} Y_{l, \mu + \frac{1}{2}}^{*} (\theta, \phi)$$
 (2-38-a)

$$a_{-l-1}$$
, $\mu^{=4\pi}$ $(l-\mu+\frac{1}{2})^{\frac{1}{2}}$ $(2l+1)^{-\frac{1}{2}}$ e $i(\delta_{-l-1}+\pi/2\cdot l)Y_{l,\mu+\frac{1}{2}}^*$ (θ,ϕ) , (2-38-b)

for spin-down initial state, taking into account the Rayleigh's formula,

$$e^{i \mathbf{k} \mathbf{r}} = \sum_{l=0}^{\infty} (2l+1) i^{l} \mathbf{j}_{l} (Kr) P_{l} (\cos r)$$

$$= 4\pi \sum_{l=0}^{\infty} (\sum_{m} i^{l} \mathbf{j}_{l} (Kr) Y *_{lm} (\theta', \phi') Y_{lm} (\theta, \phi)$$

$$(2-39)$$

where $\mathbf{r} = (r, \theta', \phi) K = (K, \theta, \phi)$ and $\mathbf{kr} = Kr\cos\gamma$. Using equations (2-31) and (2-37) and setting $\theta = \phi = 0$ (incident along the z-axis), we can express the scattering amplitude as

$$\begin{split} f(\theta) = & f_{\uparrow} = f_{\downarrow} = \frac{(4\pi)^{\frac{1}{2}} \sum_{l=0}^{\infty} (2l+1)^{-\frac{1}{2}} (l+1) (\mathrm{e}^{2i\delta_{-l-1}} - 1) + l (\mathrm{e}^{2i\delta_{-l-1}}) \Big\} Y_{l0}(\theta', \phi') \\ g(\theta) = & g_{\uparrow} \mathrm{e}^{-i\phi'} = -g_{\downarrow} \mathrm{e}^{i\phi'} = \frac{(4\pi)^{\frac{1}{2}}}{2iK} \sum_{l=1}^{\infty} (2l+1)^{\frac{1}{2}} (l+1)^{\frac{1}{2}} \cdot l^{\frac{1}{2}} (\mathrm{e}^{2i\delta_{-l-1}} - \mathrm{e}^{2i\delta_{l}}) Y_{l1}(\theta', \phi') \,. \end{split}$$

For further derivation let us start at the initial conditions (2-40-b)

$$\psi = \begin{pmatrix} A & e^{iKZ} \\ B & e^{iKZ} \end{pmatrix} , \qquad (2-41)$$

which have the initial polarization,

$$\mathbf{P} = \langle \sigma \rangle = \langle (A^*B + B^*A, i (B^*A - A^*B), |A|^2 - |B|^2) \rangle, \qquad (2-42)$$

under the normalization condition $|A|^2 + |B|^2 = 1$. Here, the polarization of an electron beam is defined by statistical averaging as equation (2-42). Then, using the Sherman function S defined by

$$S = i \left(f g^* - f^* g \right) / \left(|f|^2 + |g|^2 \right) , \qquad (2-43)$$

and the scattering cross-section for unpolarized electrons

$$\sigma_{0}(\theta) = |f|^{2} + |g|^{2} \tag{2-44}$$

we obtain the scattering cross section with initial polarization P as,

$$\sigma (\theta, \phi) = \langle |Af \uparrow + Bg \downarrow |^2 + |Ag \uparrow + Bf \downarrow |^2 \rangle$$

$$= \sigma_0 (\theta) \quad (1 + S \mathbf{n} \mathbf{P}) \qquad (2-45)$$

where

$$\mathbf{n} = (-\sin\phi, \cos\phi, 0) , \qquad (2-46)$$

 ${\bf n}$ S is a polarization vector of scattered electrons with an initially unpolarized electron beam. As the polarization ${\bf P}_S$ of scattered electrons

is derived from equation (2-42), substituting $Af_{\phi}+Bg_{\phi}$ for A and $Ag_{\phi}+Bf_{\phi}$ for B one obtains

$$P_{S}^{x} = \left\{ P_{z} \cdot U \cdot \cos \phi - S \cdot \sin \phi + P_{x} - (1 - T/\sigma) \cos \phi \left(P_{x} \cos \phi + P_{y} \sin \phi \right) \right\}$$

$$/ (1 + S \cdot \mathbf{n} \cdot \mathbf{p})$$

$$(2 - 47 - a)$$

$$P_{S}^{y} = \left\{ P_{z} \cdot U \cdot \mathbf{s} \, \mathbf{i} \, \mathbf{n} \, \boldsymbol{\phi} + S \cdot \mathbf{c} \, \mathbf{o} \, \mathbf{s} \, \boldsymbol{\phi} + T \cdot P_{y} - (1 - T / \sigma) \, \mathbf{c} \, \mathbf{o} \, \mathbf{s} \, \boldsymbol{\phi} \cdot \right.$$

$$\left. \left. \left(P_{x} \cdot \mathbf{s} \, \mathbf{i} \, \mathbf{n} \, \boldsymbol{\phi} - P_{y} \cdot \mathbf{c} \, \mathbf{o} \, \mathbf{s} \, \boldsymbol{\phi} \right) \right\} / \left. \left(1 + S \cdot \mathbf{n} \cdot \mathbf{P} \right) \right.$$

$$\left. \left(2 - 47 - \mathbf{b} \right) \right.$$

$$\left. \left(2 - 47 - \mathbf{b} \right) \right.$$

$$P_{S}^{z} = \left\{ P_{z} \cdot T - U \left(P_{x} \cdot \mathbf{c} \circ \mathbf{s} \phi - P_{y} \cdot \mathbf{s} \circ \mathbf{n} \phi \right) \right\} / (1 + S \cdot \mathbf{n} \cdot \mathbf{P}) , \qquad (2-47-c)$$

where $U=2Re(fg^*)/\sigma$ and $T=(|f|^2-|g|^2)/\sigma$. Equation (2-47) can be rewritten in simple form as,

$$\mathbf{P}_{S} = \frac{\left[\mathbf{P} \cdot \mathbf{n} + S\right] \cdot \mathbf{n} + T \cdot \mathbf{n} \times \left[\mathbf{P} \times \mathbf{n}\right] + U \cdot \left[\mathbf{n} \times \mathbf{P}\right]}{1 + S \cdot \mathbf{n} \cdot \mathbf{P}}$$
(2-48)

From equation (2-48) we see that the polarization of incident electrons are affected as follows; the vector S \mathbf{n} is added to the components $[\mathbf{P} \cdot \mathbf{n}] \cdot \mathbf{n}$ perpendicular to the scattering plane, i.e., perpendicular to the wave number vectors of both the incident and scattered states. The component parallel to the scattering plane is reduced by the factor T (|T| < 1). The polarization vector is rotated out of its original plane defined by \mathbf{n} and \mathbf{P} because of an additional component determined by U (Kessler 1976). Thus this leads to the polarization of the scattered electrons for the initially unpolarized electrons as

$$\mathbf{P}_{S} = S \quad (-\sin\phi, \cos\phi, 0) \quad . \tag{2-49}$$

Equations (2-45) and (2-49) suggest that Sherman function S has two roles, i.e. giving scattering asymmetry for initially polarized electrons and polarization of scattered electrons for initially unpolarized ones (for the qualitative explanation see Appendix 4). Equation (2-49) also shows that the direction of the ESP of the scattered electrons is perpendicular to the scattering plane.

2-4. Adopted Numerical Calculation Procedure

Hence the scattering amplitudes are expressed as a function of the phase shifts δ_l and δ_{-l-1} (see equation (2-40)), it is necessary to determine phase shift by clarifying the relationship with the radial wave function. Various calculation procedures have been developed for the estimation of phase shifts. Present calculation adopts one of the most advantageous procedure which were developed for accurate and fast computer calculation combining various calculation procedures (Yamazaki et al. 1976,1977). Some of them except for that shown below are summarized and compared with each other in Appendix 5.

Introducing the change of variables (Bunyan and Schonfelder, 1965),

$$F_{\kappa} = A_{\kappa}(r) \sin \phi_{\kappa}(r) / r \tag{2-50-a}$$

$$G_{\kappa} = A_{\kappa} (r) \operatorname{cos} \phi_{\kappa} (r) / r$$
 (2-50-b)

we get,

$$\mathrm{d}\phi_{\kappa}/\mathrm{d}r = \kappa/r\sin 2\phi_{\kappa} + W-V - \cos 2\phi_{\kappa} \tag{2-51-a}$$

$$d(\ln A) / dr = -\kappa / r \cos 2\phi_{\kappa} - \sin 2\phi_{\kappa}$$
 (2-51-b)

From equations (2-34) and (2-51-a) and their derivatives we obtain the expression for the phase shift

$$\tan \delta_{\kappa} = \frac{K \cdot j_{l+1} (Kr) - j_{l} (Kr) \{ (W+1) \tan \phi_{\kappa} + (1+l+\kappa) / r \}}{K n_{l+1} (Kr) - n_{l} (Kr) \{ (W+1) \tan \phi_{\kappa} + (1+l+\kappa) / r \}}.$$
 (2-52)

The expression on the right is evaluated at r=a where a satisfies $V(a) \sim_0$ Equation (2-52) allows us to evaluate δ_{κ} using only the first order nonlinear differential equation (2-51-a), which simplifies the computer calculation procedure considerably.

As the numerical integration of differential equation (2-51-a) cannot be made from r=0 because of the divergence of the potential energy V(r), we expand V(r) and $\phi_{\kappa}(r)$ in a power series in order to derive initial conditions at small r (Bunyan and Schonfelder 1965) as,

$$V(r) = -1/r \left(Z_0 + Z_1 r + Z_2 r^2 + Z_3 r^3\right)$$
 (2-53)

$$\phi_{\kappa}(r) = \phi_0 + \phi_1 r + \phi_2 r^2 + \cdots$$
 (2-54-a)

$$\ln (A_{\kappa}(r)) = B_0 + B_1 \ln (r) + B_1 r + B_2 r^2 + \cdots$$
 (2-54-b)

Substituting equations (2-53) and (2-54-a) into equation (2-51-a) we obtain the following equations;

$$\sin \left(2\phi_0\right) = -Z_0/\kappa \tag{2-55-a}$$

$$\phi_1 = (W + Z_1 \cos (2\phi_0)) / (1 - 2\kappa \cos (2\phi_0))$$
 (2-55-b)

$$\phi_2 = (2\phi_1 \sin(2\phi_0)) (1-\kappa\phi_1) + Z_2) / (2-2\kappa\cos(2\phi_0))$$
 (2-55-c)

$$\phi_{3} = (2\phi_{2} \sin (2\phi_{0}) \cdot (1 - 2\kappa\phi_{1}) + 2\phi_{1}^{2} \cos (2\phi_{0}) \cdot (1 - 2/3\kappa\phi_{1} + Z_{3})) / (3 - 2\kappa\cos(2\phi_{0}))$$
(2-55-d)

$$\begin{split} \phi_4 &= \left[((2\phi_3 - (2\phi_1)^3/3!) - \kappa (4\phi_1\phi_3 + 2\phi_2^2 - (2\phi_1)^4/4!)) \times \right. \\ & \text{sin} \ (2\phi_0) + (1 - \kappa\phi_1) 4\phi_1\phi_2 \cos (2\phi_0) \right] / 2 (2 - \kappa\cos(2\phi_0)) \\ & B_l = -\kappa\cos(2\phi_0) \end{split} \tag{2-56}$$

In order to keep the wave function finite at r=0 i.e., to maintain the positive B_l in equation (2-56), we choose

$$0 \le 2 \phi_0 \le \pi/2 \qquad \kappa < 0 \tag{2-57-a}$$

$$\pi \le 2 \phi_0 \le 3/2 \cdot \pi \qquad \kappa \ge 0 \tag{2-57-b}$$

Integrations were carried out from r=0.1 by the fourth order Lunge-Kutta process which has sufficient accuracy for the present calculations. In the region $0.1 \le r \le 15$, to avoid the use of excessively small intervals in r when performing the integration, a change of variables $r=0.1e^{t}$ is introduced. The equation (2-51-a) is then rewritten as

$$d\phi_{\kappa}/dt = \kappa \sin(2\phi_{\kappa}) + 0.1e^{t}(W-V-\cos(2\phi_{\kappa})). \qquad (2-58)$$

Thereafter the ordinary equation (2-51-a) was employed for integration up

to r=300. We stopped the integration at r=518 (=2Å) to reduce computing time. To make this process more appropriate, the charge distribution was reconstructed in the region $300 \le r \le 518$ as a quadratic form, the coefficients of which are determined so as to make the total charge equal to Ze, where Z is the atomic number of mercury, and the charge density and its derivative continuous at r=300 to avoid anormalous δ -function type charge distribution (Bühring 1965).

A charge reconstruction of this type may have some influence on forward scattering but may have little influence on backward scattering, since in the latter, electron is scattered by the not reconstructed potential because of small impact parameter.

According to the consideration given in Sec.2-1-3, a non-relativistic Hartree potential analytically expressed by Byatt (1957) is adopted, which is written as

$$V(r) = -Z e^{2} / r \cdot \sum_{i=1}^{3} a_{i} e^{-b} i^{r}, \qquad (2-59)$$

where a_i = 0.19, 0.56, 0.25, b_i = 9.133×10⁻³, 2.768×10⁻², 1.123×10⁻¹, respectively. All phase shift was evaluated from l =0 to $|\delta_{g}| < 10^{-5}$.

To evaluate scattering cross section and Sherman function, it may be advantageous to use the functions $E(\theta)$ and $H(\theta)$ instead of the scattering amplitudes $f(\theta)$ and $g(\theta)$ which are defined in equation (2-40) (Bühring 1968).

$$4 i H (\theta) = \sum_{l=1}^{\infty} (e^{2i\delta - l} - e^{2i\delta} l) L_l$$
 (2-60-a)

4
$$i E(\theta) = \sum_{l=1}^{\infty} (e^{2i\delta} l + e^{2i\delta - l} - 2) L_{l}^{+},$$
 (2-60-b)

where

$$L_{n}^{(\pm)}(\cos\theta) = n \left[P_{n}(\cos\theta) \pm P_{n-1}(\cos\theta) \right]. \tag{2-61}$$

The cross section and Sherman function are then expressed as

$$I(\theta) = K^{-2} (\sec^2 \theta / 2 \cdot |E|^2 + \csc^2 \theta / 2 \cdot |H|^2)$$
 (2-62)

$$S(\theta) = i(EH^* - HE^*) / (|H|^2 \cot \theta / 2 + |E|^2 \tan \theta / 2)$$
 (2-63)

These transformations have some advantages. At 180° the Legendre function is expressed as P_n (-1)=(-1) , thus the numerical summation of a large number of phase shifts, which is usually the case in high energy scattering, would incur error at angles near the backward scattering. However, L_n^+ which appears in $E(\theta)$ behaves like $\cos^2(\theta/2)$ so would be more accurate The same arguments hold for the forward scattering.

Each angular distribution of cross section and Sherman function was calculated at 1° intervals from 0° to 180° for various angular resolutions All input data such as matching radius and intervals of integrations were made sufficiently large and small, respectively, in order to make the results insensitive to those parameters.

The order of phase shifts estimated ranges from 18 to 53 for the incident energy of 300 to 2000 eV.

All the necessary additional functions such as Bessel, Neumann and Legendre functions were calculated using recurrence relations as,

$$j_{m+1}(x) = -j_{m-1}(x) + (2m+1) \quad j_m(x) / x$$
 (2-64-a)

$$n_{m+1}(x) = -n_{m-1}(x) + (2m+1) n_m(x) / x$$
 (2-64-b)

with initial conditions

$$j_0(x) = \sin(x)/x$$
, $j_1(x) = \sin(x)/x^2 - \cos(x)/x$ (2-65-a)

$$n_0(x) = -\cos(x)/x$$
, $n_1(x) = -\cos(x)/x^2 - \sin(x)/x$ (2-65-b)

and

$$L_{n+1}^{\pm}(x) = \left[(2n+1) \cdot x \cdot L_{n}^{\pm}(x) - (n+1) L_{n-1}^{\pm}(x) - (1 \pm x) P_{n-1}(x) \right] / n$$
(2-66-a)

$$P_{n+1}(x) = \left[(2n+1) x P_n(x) - n P_{n-1}(x) \right] / (n+1)$$
 (2-66-b)

with initial conditions,

$$L_0^{\pm}(x) = 0$$
 $L_1^{\pm}(x) = x \pm 1$ (2-67-a)

$$P_0(x) = 1$$
 $P_1(x) = x$ (2-67-b)

respectively, throughout the present calculations. The flow chart and the list of program for the present calculation is shown in Appendix 6.

2-5 Results and Discussion

In Fig.2-4, calculated results of the cross section are compared to the data of Bromberg's absolute measurements for primary energies of 300,

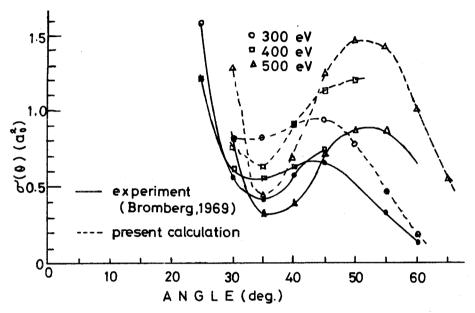


Fig. 2-4. Comparison of the cross section between the present calculation and the absolute measurements of Bromberg (1969).

400 and 500 eV(1969). Here, the theoretical calculations describe experimental curves quite well qualitatively, but in quantitative arguments the theoretical values are about 1.5 times larger for each incident electron energy. Fig.2-5 shows the calculated angular distribution of the cross section and Sherman function for various incident energies. Fig.2-5 shows comparisons to calculated results by Holzwarth and Meister (1964b), where Mayer's relativistic Hartree potential(1956) was used. Although several approximation procedures have been introduced in the present calculation, such as the scattering of relativistic electrons using a non-relativistic atomic potential, it should be noted that these calculations give satisfactory agreement with the more accurate but complicated calculation. In Fig.2-6, results are also given as a function of incident electron energy for the purpose of convenience. Results are summarized in Fig.2-7

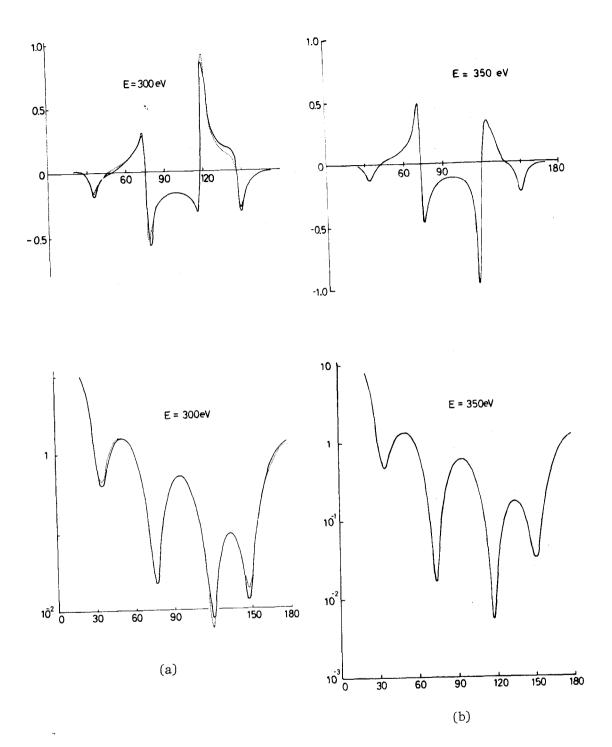
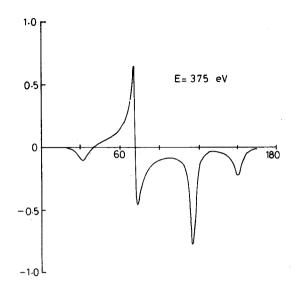
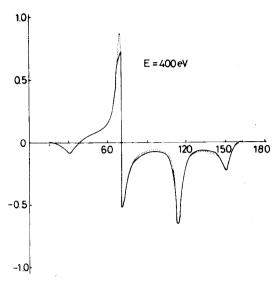
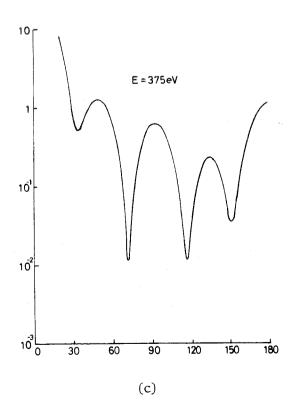
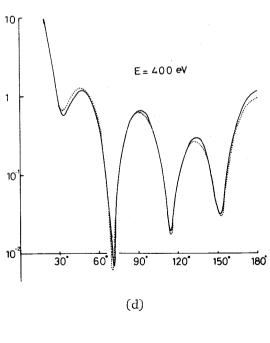


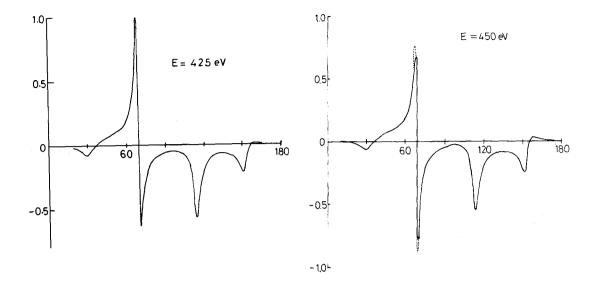
Fig. 2-5. Calculated results of spin polarization and differential cross section in unit of a_0^2 with respect to scattering angle. (——present calculation and --- calculated results using Mayer's relativistic Hartree potential (Holzwarth and Meister 1964b)).

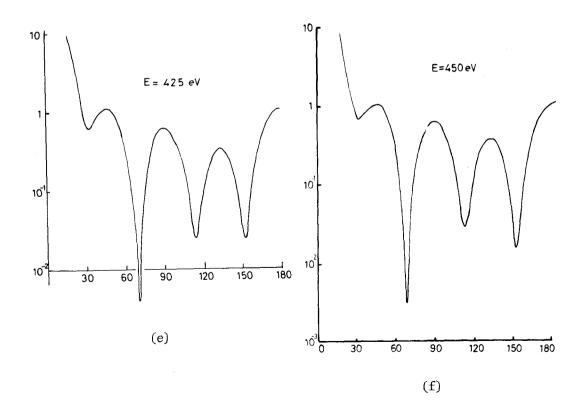


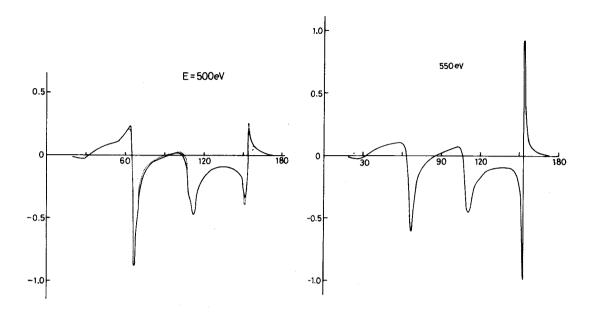


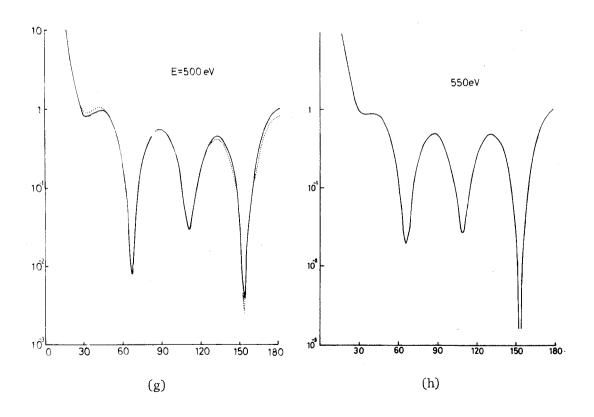


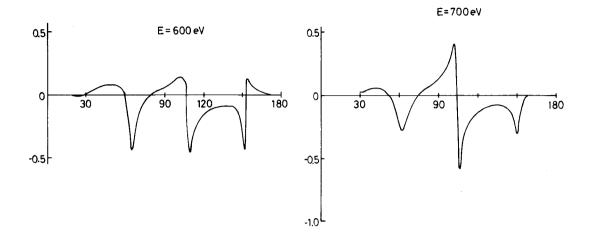


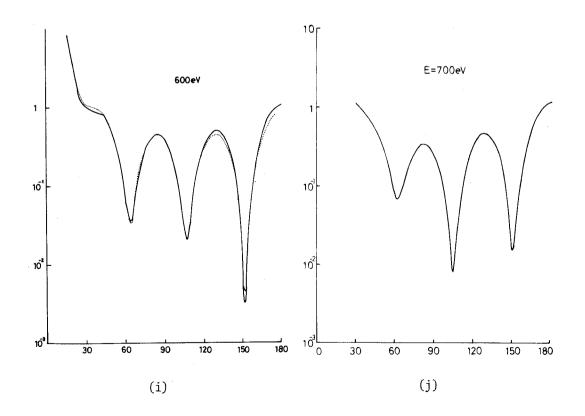


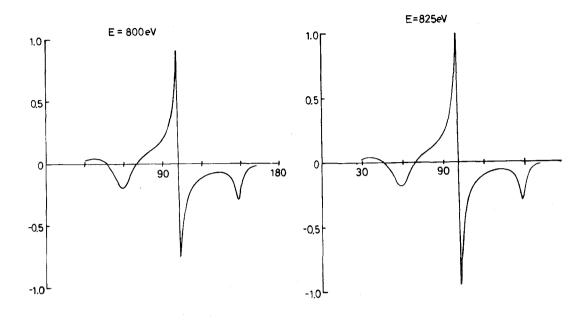


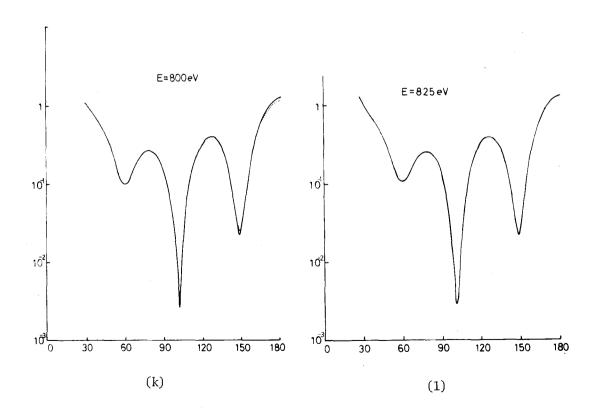


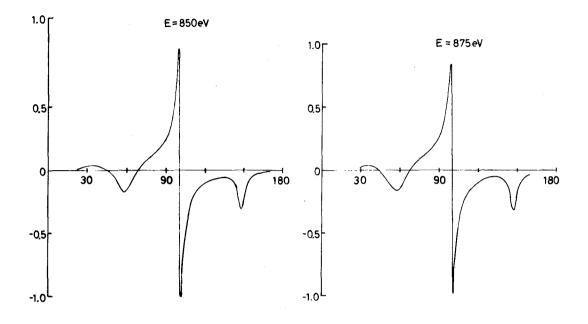


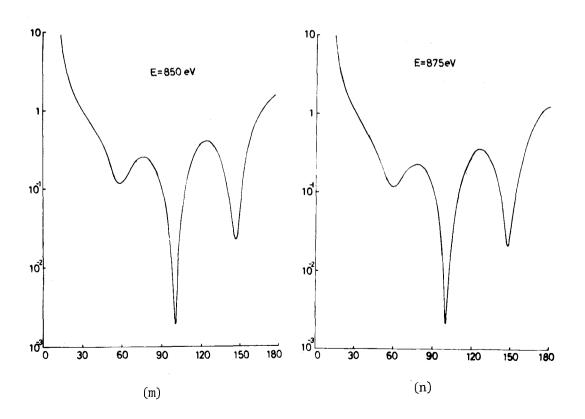


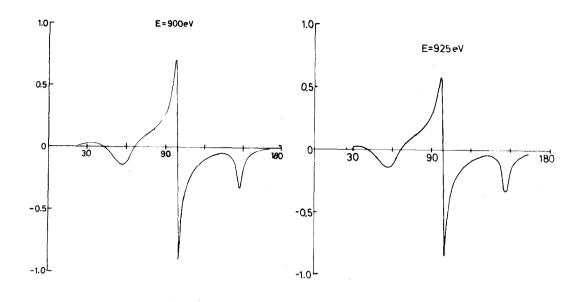


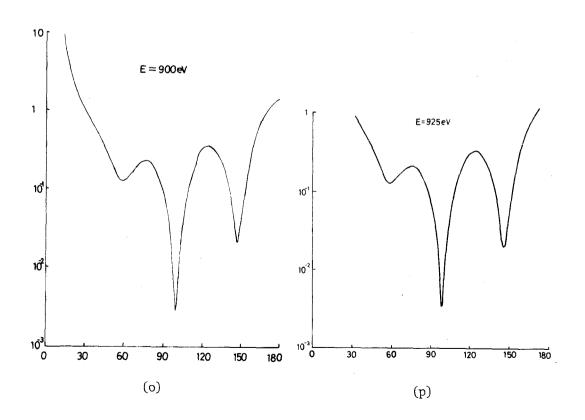


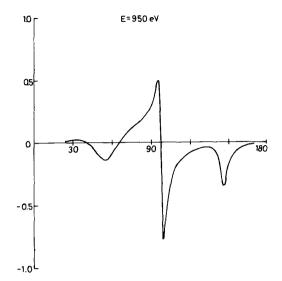


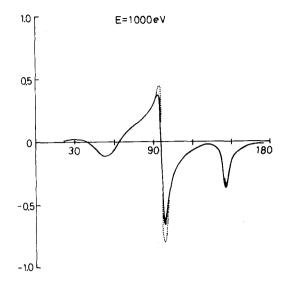


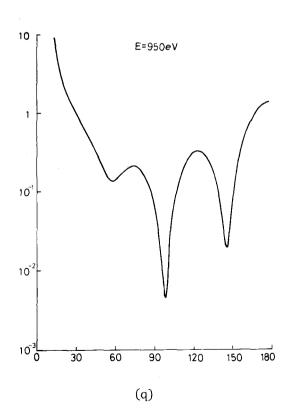


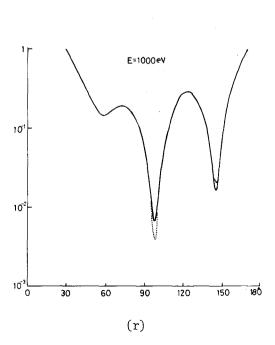


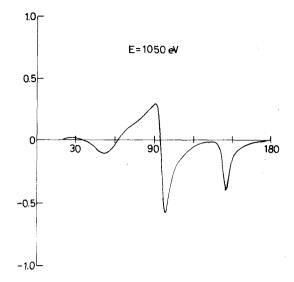


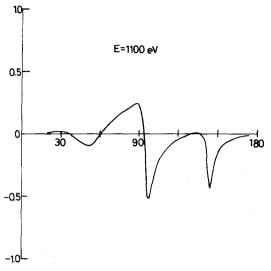


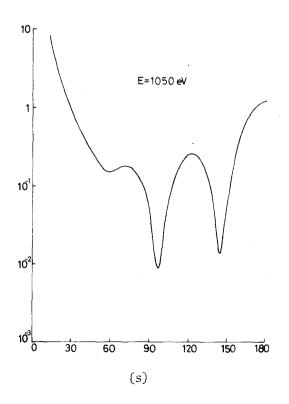


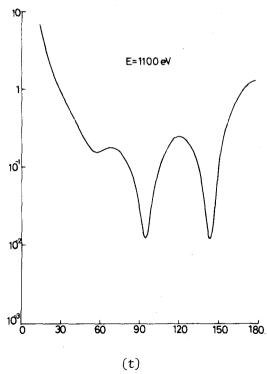


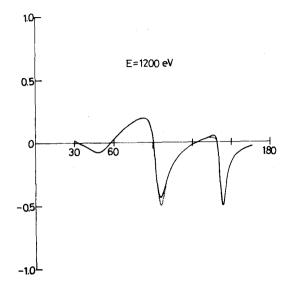


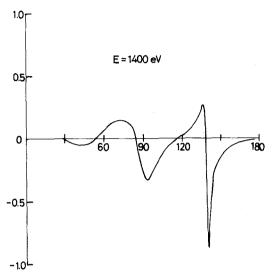


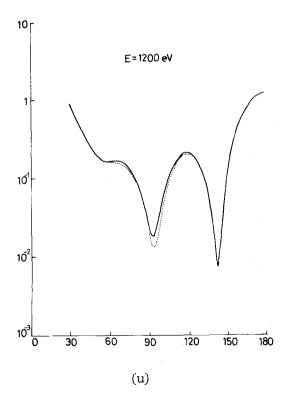


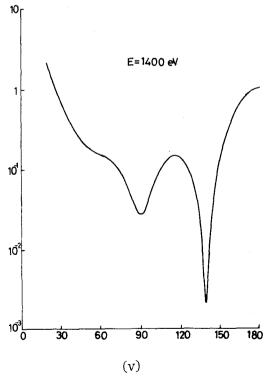


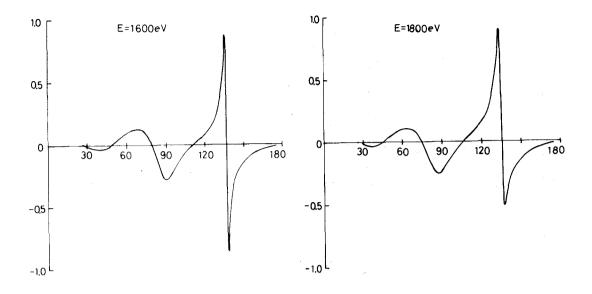


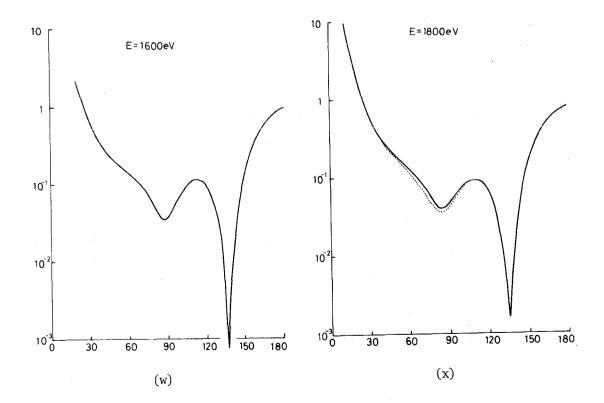


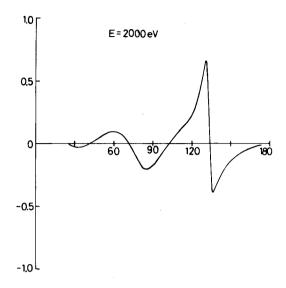


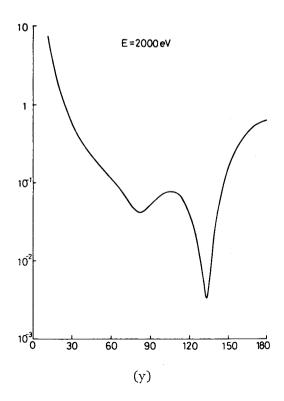












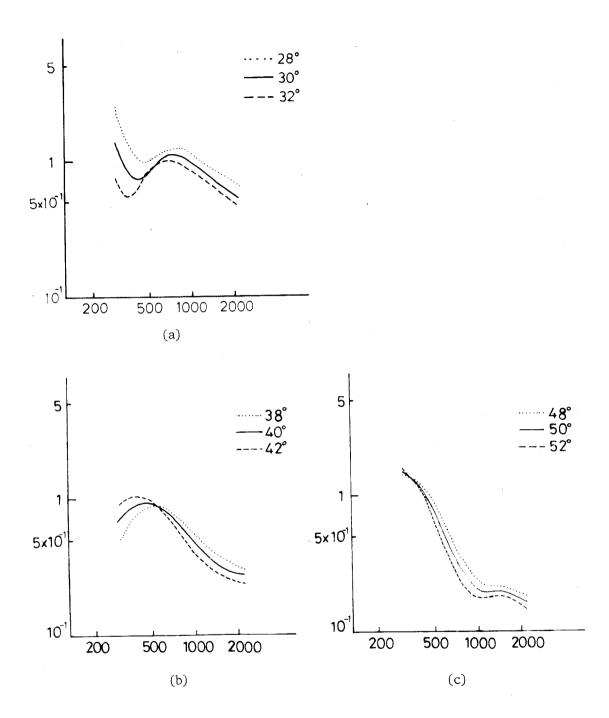
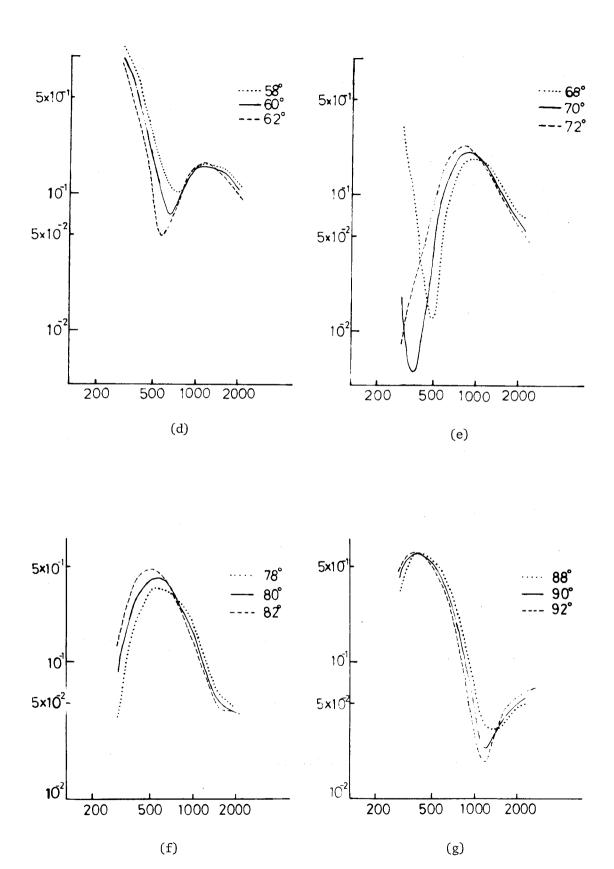
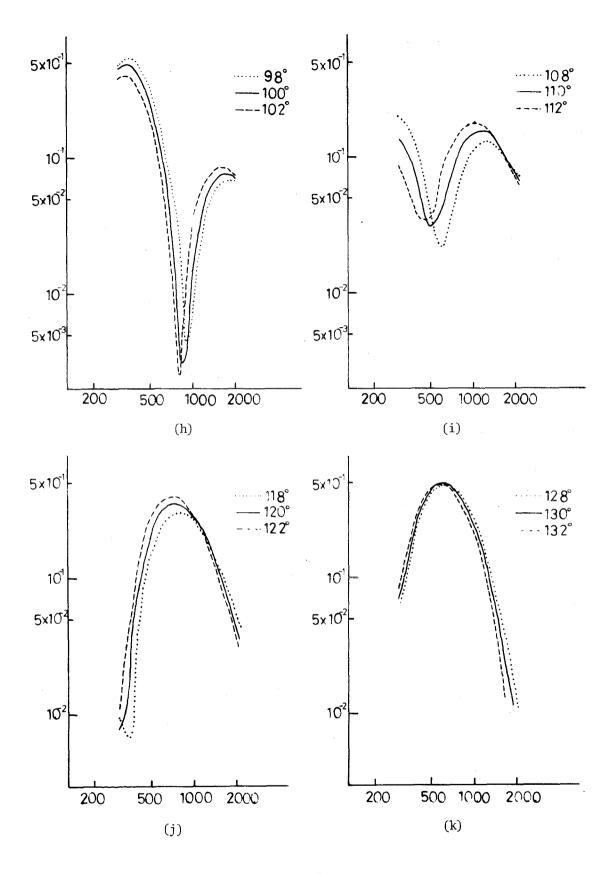
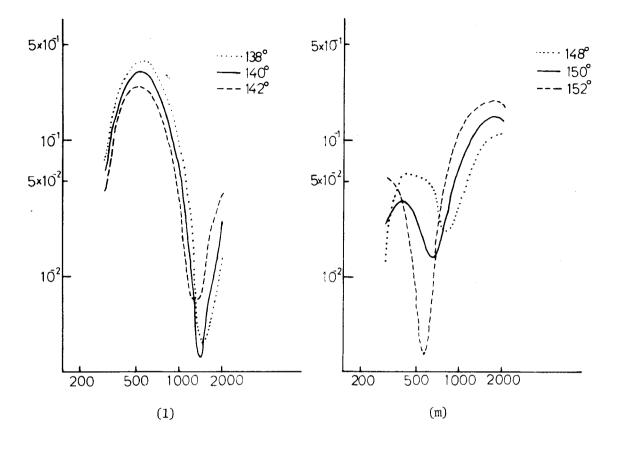


Fig. 2-6. Calculated results of differential cross section with respect to incident electron energy.







for both cases of the angular resolution of $\Delta\theta \leq 1$ and $\Delta\theta = 7$. This makes direct comparison with the measured spin polarization of a large acceptance angle possible(Bunyan and Schonfelder 1965). Fig.2-7 shows that the contours of constant polarization inclines to the left, i.e., the extremum points of ESP shift to lower angles as the energy increases. This corresponds to the fact that a diffraction angle becomes smaller as wave length shorter.

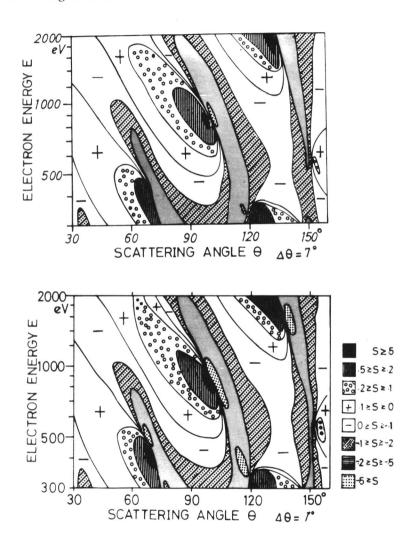


Fig. 2-7. Contours of constant polarization as function of scattering angle and electron energy with angular resolution $\Delta\theta \leq 1^{\circ}$ and $\Delta\theta = 7^{\circ}$

2-6. Application of Partial Wave Expansion to Monte-Carlo Simulation--Applicability of Conventional Screened Rutherford Cross Section for
keV Electrons and its Failure in Low Energy Region

Krefting and Reimer (1974) have pointed out that the Rutherford cross-section (see Appendix 3) is inaccurate in describing the elastic scattering of kilovolt electrons with atoms in solids for heavy elements, and is still rather poor approximation for elements as light as aluminum. They have compared the unscreened Rutherford cross-section which diverges at a scattering angle of θ = 0°, to the scattering cross-section obtained by a partial wave expansion method. However, the former method does not provide one with the total cross section, which is an important parameter in Monte-Carlo simulations. The screened Rutherford cross-section formula has been widely used in Monte-Carlo calculations (Heinrich et al. 1976), and it does provide us with the total elastic cross-section. Furthermore, Shimizu et al.(1976) have obtained close agreement between experimental and Monte-Carlo calculations based on the screened Rutherford cross-section. Hence, it is of interest to compare the partial wave expansion predictions with those obtained using screened Rutherford scattering.

From the theoretical viewpoint, although the differential cross-section for elastic scattering for electrons of energies below 1.5 keV (e.g. Fink and Yates 1970) and greater than a few tens of keV have been investigated (e.g. Sherman and Nelson 1959 and Bühring 1968b), the cross-section for intermediate energies has not yet, to our knowledge, been published. Hence it is of practical as well as theoretical use to determine the elastic scattering cross-section by partial wave expansion methods for electrons of energies between 1 and 20 keV, which are energies widely used for Monte-Carlo calculation as applied to electron microprobe and scanning electron microscopy. The differential cross-section was calculated using analytically expressed Hartree-Fock potential (T.G.Strand and Bonham 1964).

The results were compared with those published by Fink and Ingram and were found to be in satisfactory agreement with them in the region from 100 to 1500 eV.

Figures (2-8-a) and (2-8-b) show a comparison of differential cross-section for elastic scattering between the screened Rutherford and partial wave expansion calculations for aluminum at various electron energies of interest for the present study. The screening parameter β_N adopted in the present calculation was the one derived by Nigam et al. (Nigam et al.

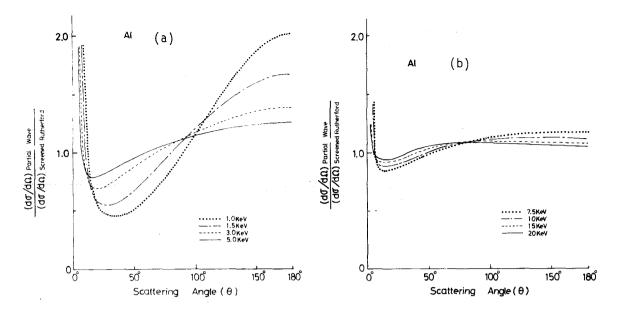


Fig. 2-8. The ratio of differential elastic scattering cross section obtained by partial wave expansion to that of screened Rutherford scattering as a function of the scattering angle θ and electron energy E for aluminum.

1959) using Thomas-Fermi potential and second Born approximation. This result shows that both the differential cross-sections are in close agreement between 10 and 20 keV and that the screened Rutherford can still be extended with fairly good accuracy down to 5 keV.

Below 5 keV, however, the descrepancy between the two becomes remarkable. So far as the excitation of high energy is concerned, such as K-ionization, for which electrons with energies higher than about 3 times of K-ionization energy plays important role in practical problem (in Aluminum 3×1.5 keV=4.5 keV), these electrons of low energies below 5 keV are no more significant source of signals, i.e. K-Xrays and/or KLL Auger electrons. However, if signals of low excitation energies are treated in the argument, we have to take into account the contribution of low energy electrons.

Thus in this case it is strongly recommended to use the differential cross section obtained from partial wave expantion calculation.

Another comparison for the total cross-section is shown in Fig.2-9. The screening parameter does not cause any marked changes in the differential cross-section for scattering angles larger than several degrees in the kV region. Hence, taking an appropriate value for the screening para-

meter, i.e. $0.48~\beta_N$ for aluminum, we can use the screened Rutherford scattering for energies ranging from 5 to 20 keV with considerable success in Monte-Carlo calculation. In Fig.2-10, total cross sections calculated by three methods are compared, i.e., partial wave expansion and first Born approximation using Hartree-Fock potential, and screened Rutherford scattering with Nigam's screening parameter β_N .

Although the partial wave expansion method is one of the most accurate theoretical approach to elastic scattering at present, it provides a differential cross-section with limited accuracy for scattering angles of less than 10 degrees because of ambiguity in the theoretical aotmic potential (Bromberg 1969). This ambiguity carries over to the total cross-section which one must use in Monte-Carlo calculation.

Thus, the present result suggests that the screened Rutherford scattering of kV electrons with considerable accuracy for a light element such as aluminum, particularly using an appropriate value of the screened parameter, e.g., $0.48~\beta_N$ for aluminum. Furthermore, since far better agreement between those two cross sections is theoretically expected for lighter elements, the Monte-Carlo calculation tech-

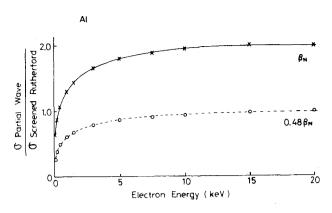


Fig.2-9. The ratio of the total cross section obtained by partial wave expansion to that of screened Rutherford scattering as a function of electron energy for different two values of the screening parameter β_N . (——after Nigam et al.(1959), ---- the best fit value.)

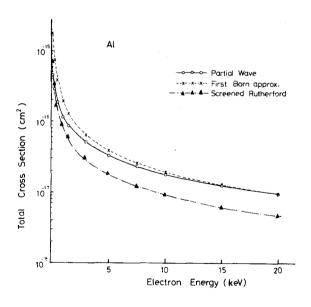


Fig. 2-10. Total cross sections obtained by partial wave expansion method, first Born approximation and screened Rutherford scattering as a function of electron energy.

nique using screened Rutherford scattering is a very useful approach for better understanding of electron penetration in organic and biological samples. However, this argument does not hold any more for such a low energy excitations as LVV Auger electron production in alminum. As a typical problem of practical importance, the application of the differential cross section obtained from partial wave expansion calculation to Monte-Carlo simulation of ${\rm Al}_{\rm LVV}$ Auger electron production will be briefly mentioned below.

Contribution of the secondary electrons to the energy distribution is seen in Fig.2-11. As is expected, the secondary electrons only contribute to the lower part of the energy distribution. The distribution

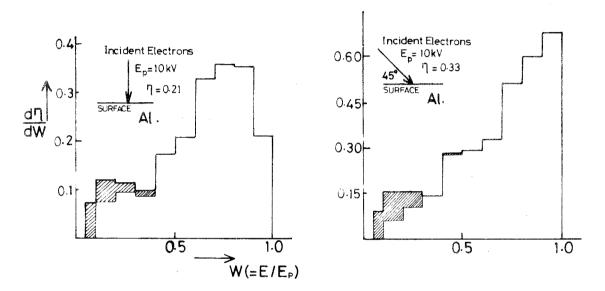


Fig. 2-11. Energy distribution of the backscattered and secondary electrons for 10-keV electrons impinging on aluminum at normal and oblique incidences. (Hatched area: signals generated by secondary electrons.)

of L-shell ionizations (corresponding to LVV- Auger electrons) produced by the secondary and backscattered electrons on the Al-specimen surface is shown in Fig.2-12 together with that of K-shell ionizations (corresponding to KLL-Auger electrons). It is worth nothing that almost half of the LVV-Auger electrons and about 30% of the KLL-Auger electrons are produced by the secondary and backscattered electrons. Another point to be noted

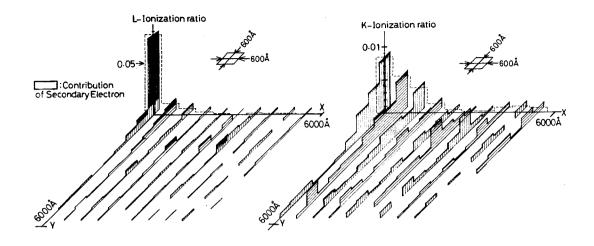


Fig. 2-12. Spatial distributions of K and L ionizations generated by 10 keV electrons in the surface layer of aluminum. The longitudinal axes indicate K - and L -ionization ratio of the sectional contributions per 600 Å, of backscattered and secondary electron to the contribution of an incident electron. (Solid area, signals generated by secondary electrons.)

a) L ionizations in the surface layer of 1 \mathring{A} by the contribution of one primary electron: 1.02×10^{-3} $/\mathring{A}$. L ionizations by the total contributions of backscattered and secondary electrons: 8.9×10^{-4} $/\mathring{A}$. (b) K ionizations in the surface layer of 1 \mathring{A} by the contribution of one primary electron: 6.5×10^{-6} $/\mathring{A}$. K ionizations by the total contributions of backscattered and secondary electrons: $2.7\times10^{-6}/\mathring{A}$.

is that the contribution of secondary electrons to L ionization is remarkable at the vicinity of the incident primary beam impact as is seen in Fig.2-12-b. This is quite understandable because the secondary electrons are generated almost normal to the direction of primary electrons of high energies, and, hence, they move parallel with the surface at the vicinity of the incident point leading to a high generation rate of L ionization in the surface layer in question.

CHAPTER 3 THEORY OF ELECTRON-MERCURY INELASTIC SCATTERING ---- APPLICATION OF DWB THEORY

3-1 Introduction

In electron-mercury scattering, similarities in the diffraction patterns of elastic and inelastic cases had been previously recognized by Mohr and Nicoll (1932), and Tate and Palmer (1932) for intermediate energies. Inelastic scattering experiments with an energy analyser of high energy resolution also showed a diffraction pattern similar to elastic scattering at inelastic channels of 6¹P excitation (Gronemeier 1970), and 6¹P and 6p'³P excitation channels (Hanne et al. 1972, Yamazaki et al. 1977c). These are the transitions of high scattering intensities in electron-mercury loss spectra. Polarization measurements of inelastic electrons have recently been made at 6¹P and 6p'³P excitation channels, which also resulted in patterns similar to the elastic cases (Eitel and Kessler 1970, 1971, Hanne and Kessler 1972).

Penny (1932) and Yavorskii(1947) treated the total cross sections for excitation of 6^1P and 6^3P states in mercury using Born-Oppenheimer approximation. McConnell and Moiseiwitsch (1968) refined the above treatments using Born-Ochkur approximation. In regards to oscillator strength, the above treatment gave $f(^1P_1 \rightarrow ^1S_1)=1.17$ and $f(^3P_1 \rightarrow ^1S_0)=0.037$ which were in close agreement to the experimental values 1.18 and 0.037 (Lulio 1965). According to development in ESP measurements of inelastic channels, theoretical calculations of differential cross section and ESP at the 6^1P channel would be highly expected. One theoretical calculation has been made and resulted in success in a certain aspect using distorted wave Born approximation (DWB approximation) (Madison and Shelton 1973). However, this calculation is confined to rather lower impact energies (50-180 eV) and failed to give correct cross sections.

In this chapter, the $6^{1}P$ excitation cross section of electron-mercury scattering is discussed. For this purpose, the DWB approximation is formulated in detail at $6^{1}P$ excitation for the mercury atom and calculations are made for incident electron energies of 50 to 500 eV. This may provide detailed information on the scattering process, particularly on spin polarization in unresearched areas.

The reason for adopting the DWB approximation are as follows; First, Born approximation is known to give inadequate information on the differential scattering cross section at large scattering angles and in every case predicts zero polarization (see Sec.2-2-2), thus in spite of its simplicity and clearness, Born approximation turns out to be useless. Second, the coupling between $6^{1}P$ excitation and elastic channels is generally weak (the intensity ratio between $6^{1}P$ excitation and elastic scattering is about 10^{-2} in both the energy and angular regions in question). This weak coupling implies that the scattering of electrons from the inelastic channels to the elastic channel is negligible. Thus, it may not be necessary to adopt an approximation as precise as the close-coupling approximation. Third, the similarity of diffraction patterns at elastic and $6^{1}P$ excitation scattering suggests that the elastic scattering plays a dominant role in the $6^{1}P$ excitation scattering.

This leads one to expect that the present DWB approximation would provide reasonable accuracy for the interpretation of 6¹P excitation scattering process. Furthermore, as there exist little theoretical results using DWB approximation except for the two works for heavy atoms (Sawada et al. 1971, Madison and Shelton 1973), it is interesting to apply the relativistic DWB approximation to the calculation of cross section and spin polarization of electron-mercury scattering.

3-2 DWB Approximation

As is shown in Sec.2-2-1, the formal solution for the wave equation $H\psi_{\alpha} = W_{\alpha}\psi_{\alpha}$ is written implicitly as

$$\psi_{\alpha}^{(\pm)} = \Phi_{\alpha} + \frac{1}{W_{\alpha} - K \pm i \varepsilon} V \psi_{\alpha}^{(\pm)} , \qquad (3-1)$$

$$K = H - V \tag{3-2}$$

The transition rate per unit time is given by (Gell-Mann and Goldberger 1953)

$$w_{ij} = 2\pi |T_{ij}|^2 \delta(W_i - W_j) , \qquad (3-3)$$

where

$$T_{ij} = \langle \boldsymbol{\phi}_{j} | V | \boldsymbol{\psi}_{i}^{(+)} \rangle . \tag{3-4}$$

In the case of $V = V_1 + V_2$, equation (3-4) is written

$$T_{ij} = \langle \mathbf{0}_j | V_1 + V_2 | \psi_i^{(+)} \rangle \qquad (3-5)$$

Introducing the eigenfunctions of K+V as

$$X_{\alpha}^{(\pm)} = \mathbf{0}_{\alpha} + \frac{1}{W - K \pm i \varepsilon} V_{1} X_{\alpha}^{(\pm)} , \qquad (3-6)$$

we can transform the equation (3-5) as follows,

$$\begin{split} T_{ij} = & < X_{j}^{(-)} - \frac{1}{W - K - i\varepsilon} V_{1} X_{j}^{(-)} | V_{1} + V_{2} | \psi_{i}^{(+)} > \\ & = < X_{j}^{(-)} | V_{1} + V_{2} | \psi_{i}^{(+)} > - < X_{j}^{(-)} | V_{1} - \frac{1}{W - K + i\varepsilon} (V_{1} + V_{2}) | \psi_{i}^{(+)} > \\ & = < X_{j}^{(-)} | V_{1} + V_{2} | \psi_{i}^{(+)} > - < X_{j}^{(-)} | V_{1} | \psi_{i}^{(+)} - \Phi_{i} > \\ & = < X_{j}^{(-)} | V_{2} | \psi_{i}^{(+)} > + < X_{j}^{(-)} | V_{1} | \Phi_{i} > . \end{split}$$

$$(3-7)$$

The ingoing distorted waves are related to outgoing waves by time reversal, which has the form (Satschler 1964)

$$\left(X_{\alpha}^{(-)}(\mathbf{k},\mathbf{r})\right)_{m',m} = (-1)^{m'-m} \left(X_{\alpha}^{(+)}(-\mathbf{k},\mathbf{r})\right)_{-m',-m}$$
(3-8)

(The appearance of the ingoing wave in scattering problem is qualitatively explained by Breit and Bethe (1954), and Wu and Ohmura (1962).) Considering the inelastic scattering of an electron-atom system, we can set v_1 as the atomic potential and v_2 as the interaction potential between the incident and atomic electrons (see Sec. 3-3). In this case, the second term of equation (3-7) vanishes because of the orthogonality of ground and excited states of atomic electrons. Then, equation (3-8) is written

$$T_{ij} = \langle X_j^{(+)} | V_2 | \phi_i^{(+)} \rangle . \tag{3-9}$$

Note must be made of the fact that equation (3-9) is an exact solution of the problem.

In equation (3-9), if the atomic potential v_1 is substantially larger than the interaction potential v_2 , then we may substitute $X_i^{(+)}$ for $\psi_i^{(+)}$ and get

$$T_{ij} = \langle X_j^{(-)} | V_2 | X_i^{(+)} \rangle. \tag{3-10}$$

Equation (3-10) is called distorted wave Born (DWB) approximation, since Born approximation is obtained if $X_{j}^{(-)}$ and $X_{i}^{(+)}$ are replaced by plane waves. That is, DWB approximation introduces the effect of distortion of plane wave by the core potential on inelastic scattering.

To clarify the physical aspects of the DWB approximation, we will view scattering of electrons with hydrogen atoms non-relativistically. The wave equation for the system is written

$$\left\{ \frac{1}{2} \cdot \left(p_{1}^{2} + p_{2}^{2} \right) + E + \frac{e^{2}}{r_{1}} + \frac{e^{2}}{r_{2}} - \frac{e^{2}}{r_{12}} \right\} \psi = 0 , \qquad (3-11)$$

where the incident electron is distinguished by the suffix 1, the atomic electron by the suffix 2. The energy E is the sum of the energy E_0 of the atomic electron in its ground state and of the kinetic energy of the incident electron. We may expand the function $\psi(\mathbf{r}_1, \mathbf{r}_2)$ in the form

$$\psi \left(\mathbf{r}_{1}, \mathbf{r}_{2}\right) = \left(\sum_{n} + \int \psi_{n}\left(\mathbf{r}_{2}\right) \cdot F_{n}\left(\mathbf{r}_{1}\right)\right) \tag{3-12}$$

where the functions ψ $\stackrel{(\mathbf{r})}{n}$ are the eigenfunction for the hydrogen atom, satisfying

$$(\frac{1}{2}\nabla^2 + E_n + e^2/r) \phi_n(r) = 0$$
 (3-13)

The integral sign denotes integration over the functions of the continuous spectrum. Substituting equation (3-12) in equation (3-11) using equation (3-13) and multiplying $\psi_n^*(\mathbf{r}_2)$ on both sides of this equation and integrating over the coordinate space of the atomic electron, we obtain

Writing

$$V_{nm}(\mathbf{r}_1) = \int \psi_{n}^*(\mathbf{r}_2) e^2 / r_{12} \cdot \psi_{m}(\mathbf{r}_2) d\mathbf{r}_2 , \qquad (3-15)$$

we have

$$(\nabla^2/2+E-E)$$
 $P_n = \sum_{m} V_{nm} P_m = \sum_{m} V_{nm} P_m$ (r). (3-16)

If $V_{nm} (n \ge 0 \text{ ,} m \ge 1 \text{ ,} n \ne m)$ is neglected in equation (3-16), then we obtain

$$(\nabla^2/2 + E - E_0 - V_{00}) F_0 = 0$$
 (3-17-a)

$$(\nabla^{2}/2+E-E_{i}-V_{ii})$$
 $F_{i}=V_{io}F_{o}$ (3-17-b)

Equation (3-17-a) is merely the ordinary equation for elastic scattering with atomic potential V_{00} , which can be solved by the same method developed in Sec.2-3. As F_0 is known, the equation (3-17-b) becomes a simple inhomogenious differential equation which can be easily solved (Mott and Massey 1965) as

$$F_{i}(r,\theta,\phi) \sim -\frac{1}{2\pi} r^{-1} e^{iK_{i}r} \int V_{i0}(r',\theta',\phi') \cdot F_{0}(r',\theta',\phi') f_{i}(r',\pi-\Theta) d\mathbf{r'}$$
(3-18)

where f_{i} satisfies

$$(\nabla^2/2 + E - E_i - V_{ii}) f_i(\mathbf{r}) = 0$$
, (3-19)

and $\cos (\theta) = \cos \theta \cos \theta' + \sin \theta \sin \theta' \cos (\phi - \phi')$.

As equation (3-18) equals equation (3-10), the essential points concerning DWB approximation are concluded as follows:

- 1) neglect of the scattering from inelastic states to the elastic state and
- 2) neglect of the interaction between the arbitral set of inelastic states. The ''Born'' of DWB stems from the approximation mentioned above.

From another view points, DWB approximation is one of the first order perturbation where K+V is chosen as the unperturbed Hamiltonian. On the other hand, Born approximation is the first order perturbation theory where K is chosen as the unperturbed Hamiltonian.

3-3. Application of DWB Approximation to Electron-Impact Excitation of $6^{1}P$ State of Mercury Atom

In this section, an attempt is made to rewrite the theoretical expression of DWB approximation in a more concrete form for practical use.

The electron configuration in the mercury atom is expressed as $(1s)^2$ $(2s)^2$ $(5d)^{10}(6s)^2$. In as far as the 6^1P excitation is concerned, the atomic electrons interacting directly with incident electrons are confined

to electrons in the 6s shell. Therefore, it is assumed that atomic electrons other than $(6s)^2$ do not interact directly with the incident electrons. Then, the total Hamiltonian H is written as

$$H = H_0(\mathbf{r}) + H_1(\mathbf{r}_1, \mathbf{r}_2) + \sum_{l=1,2} \frac{e^2}{|\mathbf{r} - \mathbf{r}_l|},$$
 (3-20)

where ${\bf r}$ and ${\bf r}_l$ (l=1,2) correspond to incident and 6s electrons respectively and

$$H_{\mathbf{0}}(\mathbf{r}) = K_{\mathbf{r}} + V_{z-2}(\mathbf{r}) \tag{3-21}$$

$$H_{1}(\mathbf{r}_{1},\mathbf{r}_{2}) = K_{\mathbf{r}_{1}} + K_{\mathbf{r}_{2}} + V_{z-2}(\mathbf{r}_{1}) + V_{z-2}(\mathbf{r}_{2}) + \frac{e^{z}}{|\mathbf{r}_{1} - \mathbf{r}_{2}|}, \quad (3-22)$$

where K is kinetic energy and V_{z-2} the atomic potential energy composed of a mercury nucleus and core electrons. We will rearrange the above Hamiltonian as follows.

$$H_{\alpha} = K_r + V_z^{\alpha}(r) + H_1(\mathbf{r}_1, \mathbf{r}_2)$$
 (3-23)

$$u_{\alpha} = -V_{z}^{\alpha}(r) + V_{z-2}(r) + \sum_{l=1,2} \frac{e^{2}}{|\mathbf{r} - \mathbf{r}_{l}|}$$
 (3-24)

where

$$V_{z}^{\alpha}(r) = V_{z-2}(r) + \langle \xi_{\alpha} | \sum_{l=1,2} \frac{e^{2}}{|\mathbf{r} - \mathbf{r}_{l}|} | \xi_{\alpha} \rangle$$
, (3-25)

and

$$H(\mathbf{r}_1, \mathbf{r}_2) \xi_{\alpha} = E_{\alpha} \xi_{\alpha} , \qquad (3-26)$$

where α takes values i and j according to the atomic states before and after scattering, respectively. The potential V_2 in equation (3-10) corresponds to the u_{α} of equation (3-24). Then, the distorted wave function X_{α} is written as

$$X_{\alpha}(\mathbf{r}, \mathbf{r}_{1}, \mathbf{r}_{2}) = X_{\alpha}^{0}(\mathbf{r}) \cdot \xi_{\alpha}(\mathbf{r}_{1}, \mathbf{r}_{2}) , \qquad (3-27)$$

and X^o_{α} satisfies

$$(K_{\mathbf{r}} + V_{\mathbf{z}}^{\alpha}) X_{\alpha}^{0} = (W - E_{\alpha}) X_{\alpha}^{0}.$$
(3-28)

The u_i and u_j differ outwardly from each other but have like effects on equation (3-10) because ξ_i and ξ_j belong to different eigenvalues of the same Hamiltonian. Namely, from equation (3-10)

$$\begin{split} T_{ij} &= < X_{j}^{0(-)} \, \boldsymbol{\xi}_{j} \, | \, -V_{z}^{\alpha} \, (r) \, +V_{z\,-\,2}(r) \, + \underset{l\,=\,1,2}{\boldsymbol{\Sigma}} \, \frac{e^{\,2}}{\, | \, r-r_{l}|} \big| X_{i}^{\,0(+)} \boldsymbol{\xi}_{i} \, > \\ &= < X_{j}^{0(-)} \big| < \boldsymbol{\xi}_{j} \, | \, \underset{l\,=\,1,2}{\boldsymbol{\Sigma}} \, \frac{e^{\,2}}{\, | \, \boldsymbol{r}-\boldsymbol{r}_{j}|} \, | \, \boldsymbol{\xi}_{i} \, > \, | \, X_{i}^{\,0\,(+)} \, > \, . \end{split} \tag{3-29}$$

For further calculation, we take ξ_i and ξ_j as $(6s)^2$ s ground state and (6s) $(6p)^1$ P excited state respectively. We may write the wave function ξ_i in the form

$$\xi_{i} = \phi_{0}(1,2) \cdot \zeta_{0}(1,2) \tag{3-30}$$

with

$$\phi_{o}(1,2) = Y_{oo}(\theta_{1},\phi_{1}) \cdot R_{oo}(r_{1}) \cdot Y_{oo}(\theta_{2},\phi_{2}) \cdot R_{oo}(r_{2}), \quad (3-31)$$

where $Y_{lm}(\theta,\phi)$ is a spherical harmonic, $R_{oo}(r)$ the radial wave function for the 6s electrons, and $\zeta_o(1,2)$ the singlet spin function associated with spin quantum number $S=M_S=o$. Concerning ξ_j , we ignore spin-orbit coupling for simplicity and introduce pure Russel-Saunders P-state wave functions given by

$$\xi_{j} = \sum_{M_{L}} C(J, 1, S; M_{L}, M_{S}) \cdot \phi_{1M_{L}}^{S}(1, 2) \cdot \zeta_{SM_{S}}(1, 2) , \qquad (3-32)$$

where the $C(J,1,S;M_L,M_S)$ are Clebsch-Gordan coefficients shown in Table 3-1,

$$\begin{aligned} \phi_{1M_{L}}^{S}(1,2) &= \frac{1}{\sqrt{2}} \left\{ Y_{oo}(\theta_{1},\phi_{1}) \cdot R_{1o}(r_{1}) \cdot Y_{1M_{L}}(\theta_{2},\phi_{2}) \cdot R_{11}(r_{2}) \right. \\ &+ Y_{oo}(\theta_{2},\phi_{2}) \cdot R_{10}(r_{2}) \cdot Y_{1M_{L}}(\theta_{1},\phi_{1}) \cdot R_{11}(r_{1}) \right\} \end{aligned}$$
(3-33)
$$(+: S=0, -: S=1)$$

are the spacial wave functions with radial functions $^R_{10}$ and $^R_{11}$ for the 6s and 6P electrons respectively and $^\zeta_{S\,M_S}$ is the spin function for the two electrons associated with spin quantum numbers S and M_S .

Table 3-1. Clebsch-Gordan coefficients $(J, 1, S; M-M_S, M_S)$.

$$\begin{split} & S = & M_{S} = 1 & M_{S} = 0 & M_{S} = -1 \\ & J + 1 & \left[\frac{(J + M) (J + M + 1)}{(2J + 1) (2J + 2)} \right]^{\frac{1}{2}} & \left[\frac{(J - M + 1) (J + M + 1)}{(2J + 1) (J + 1)} \right]^{\frac{1}{2}} & \left[\frac{(J - M) (J - M + 1)}{(2J + 1) (2J + 2)} \right]^{\frac{1}{2}} \\ & J & - \left[\frac{(J + M) (J - M + 1)}{2J (J + 1)} \right]^{\frac{1}{2}} & \frac{M}{[J (J + 1)]^{\frac{1}{2}}} & \left[\frac{(J - M) (J + M + 1)}{2J (2J + 1)} \right]^{\frac{1}{2}} \\ & J - 1 & \left[\frac{(J - M) (J - M + 1)}{2J (2J + 1)} \right]^{\frac{1}{2}} & \left[\frac{(J - M) (J + M)}{J (2J + 1)} \right]^{\frac{1}{2}} & \left[\frac{(J + M + 1) (J + M)}{2J (2J + 1)} \right]^{\frac{1}{2}} \end{split}$$

The inner parenthesis of equation (3-29) can be easily calculated since the operators in equation (3-29) do not contain spin operator and the matrix elements corresponding to different spin quantum numbers vanish (This means that one of the selection rules corresponding to the conservation of multiplicity holds in DWB approximation.). It is found that

$$\begin{split} & v_{10}^{M_L}(r,\theta,\phi) \equiv <\xi_i | \sum_{l} \frac{e^2}{|\mathbf{r}-\mathbf{r}_l|} | \xi_j > \\ & = \frac{(8\pi)^{\frac{1}{2}}}{3} e^2(\phi_{10},\phi_{00}) <\phi_{11} | F_1(r_1,r) | \phi_{00} > Y_{1,M_L}^*(\theta,\phi) \\ & \equiv v_{10} \cdot Y_{1,M_L}^*(\theta,\phi) \end{split}$$
(3-34)

$$F_{n}(r_{1},r) = \begin{cases} \frac{1}{r_{1}} \left(\frac{r}{r_{1}}\right)^{n} & r_{1} > r \\ \frac{1}{r} \left(\frac{r_{1}}{r}\right)^{n} & r > r_{1} \end{cases}$$

$$(3-35)$$

In equation (3-34) the following formulae are used

$$\frac{1}{|\mathbf{r} - \mathbf{r}_{1}|} = \left\{ \frac{1}{|\mathbf{r}_{1}|} \sum_{n=0}^{\infty} \left| \frac{\mathbf{r}_{1}}{\mathbf{r}_{1}} \right|^{n} P_{n} \left(\cos \gamma \right), r > r \right\}$$

$$\frac{1}{|\mathbf{r}|} \sum_{n=0}^{\infty} \left| \frac{\mathbf{r}_{1}}{\mathbf{r}} \right|^{n} P_{n} \left(\cos \gamma \right), r > r_{1}$$
(3-36)

where γ is an angle formed by the two vectors ${f r}$ and ${f r}$,

$$P_{n}(\cos\gamma) = \frac{4\pi}{2n+1} \sum_{m} Y_{n,m}(\theta_{1}, \phi_{1}) \cdot Y_{n,m}(\theta_{2}, \phi_{2})$$
 (3-37)

and

$$\int Y n_{1} \stackrel{*}{,} m_{1} \stackrel{Y}{,} 1, m \stackrel{Y}{,} n_{2} \stackrel{m}{,} m_{2} \stackrel{d}{,} \Omega = \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \left(\frac{2n_{2}+1}{2n_{1}+1}\right)^{\frac{1}{2}} C \left(n_{2}, 1, n_{1}; m_{2}, m\right) \\ + C \left(n_{2}, 1, n_{1}; 0, 0\right). \tag{3-38}$$

As can be seen from equations (3-34) and (3-35), the form factor $v_{0\,1}$, the radial part of the effective potential which causes $6^1\mathrm{S} \to 6^1\mathrm{P}$ excitation behaves like r^{-2} at large r, corresponding to the induction of the electric dipole moment. In general, the form factors appearing in various excitation processes behave like r^{-n} in correspondence to the various multipole moment induced. This also implies that among the various transitions, those corresponding to a momentum transfer of one unit may be relatively strong since the form factor corresponding to these transitions decreases most slowly.

The wave functions $X^{(+)}$ and $X^{(-)}$ can be easily written using the equation (2-17) for the two initial spin states in Sec.2-2-1 as

$$X_{i} \stackrel{(-)}{=} 4\pi \left\langle \sum_{l=0}^{L} \frac{e^{i\frac{\pi}{2}} l}{2l+1} \left\{ (l+\mu+\frac{1}{2}) G_{l} e^{-i\eta}_{l+} (l-\mu+\frac{1}{2}) G_{-l-1} e^{-\eta}_{-l-1} \right\} \cdot \left(-\sum_{l=1}^{L} \frac{e^{i\frac{\pi}{2}} l}{2l+1} (l-\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (l+\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (-G_{l} e^{-\eta}_{l+G_{-l-1}} e^{-i\eta}_{-l-1}) \cdot \left(-\frac{1}{2} \frac{e^{-i\frac{\pi}{2}} l}{2l+1} (l-\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (l+\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (-G_{l} e^{-\eta}_{l+G_{-l-1}} e^{-i\eta}_{-l-1}) \cdot \left(-\frac{1}{2} \frac{e^{-i\frac{\pi}{2}} l}{2l+1} (l-\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (l+\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (-G_{l} e^{-\eta}_{l+G_{-l-1}} e^{-i\eta}_{-l-1}) \cdot \left(-\frac{1}{2} \frac{e^{-i\frac{\pi}{2}} l}{2l+1} (l-\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (l+\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (-G_{l} e^{-\eta}_{l+G_{-l-1}} e^{-i\eta}_{-l-1}) \cdot \left(-\frac{1}{2} \frac{e^{-i\frac{\pi}{2}} l}{2l+1} (l-\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (l+\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (-G_{l} e^{-\eta}_{l+G_{-l-1}} e^{-i\eta}_{-l-1}) \cdot \left(-\frac{1}{2} \frac{e^{-i\frac{\pi}{2}} l}{2l+1} (l-\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (l+\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (-G_{l} e^{-\eta}_{l+G_{-l-1}} e^{-i\eta}_{-l-1}) \cdot \left(-\frac{1}{2} \frac{e^{-i\frac{\pi}{2}} l}{2l+1} (l-\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (l+\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (-G_{l} e^{-\eta}_{l+G_{-l-1}} e^{-i\eta}_{-l-1}) \stackrel{1}{}^{\frac{1}{2}} (l+\mu+\frac{1}{2}) \stackrel{1}{}^{\frac{1}{2}} (l+\mu+\frac{$$

$$X_{i\downarrow}^{(-)} = 4\pi \left(-\sum_{l=1}^{\Sigma} \sum_{\mu} \frac{e^{i\frac{\pi}{2}l}}{(2l+1)} (l + \mu + \frac{1}{2})^{\frac{1}{2}} (l - \mu + \frac{1}{2})^{\frac{1}{2}} (-G_l e^{-i\eta} l + G_{-l-1} e^{-i\eta} - l - 1) \right)$$

$$= \left(\sum_{l=0}^{\Sigma} \sum_{\mu} \frac{e^{i\pi n_2} l}{(2l+1)} \{ (l - \mu + \frac{1}{2}) G_l e^{-i\eta} l + (l + \mu + \frac{1}{2}) G_{-l-1} e^{-i\eta} - l - 1 \} \right)$$

$$= Y_{l, \mu - \frac{1}{2}} (\theta, \phi) \cdot Y_{l, \mu + \frac{1}{2}} (\theta', \phi')$$

$$= Y_{l, \mu - \frac{1}{2}} (\theta, \phi) \cdot Y_{l, \mu - \frac{1}{2}} (\theta', \phi')$$

$$= Y_{l, \mu - \frac{1}{2}} (\theta, \phi) \cdot Y_{l, \mu - \frac{1}{2}} (\theta', \phi')$$

$$= Y_{l, \mu - \frac{1}{2}} (\theta, \phi) \cdot Y_{l, \mu - \frac{1}{2}} (\theta', \phi')$$

$$= Y_{l, \mu - \frac{1}{2}} (\theta, \phi) \cdot Y_{l, \mu - \frac{1}{2}} (\theta', \phi')$$

$$= Y_{l, \mu - \frac{1}{2}} (\theta, \phi) \cdot Y_{l, \mu - \frac{1}{2}} (\theta', \phi')$$

$$= Y_{l, \mu - \frac{1}{2}} (\theta', \phi') \cdot Y_{l, \mu - \frac{1}{2}} (\theta', \phi')$$

and using $Y_{l0} = [(2l+1)/4\pi]^{\frac{1}{2}}$

$$X_{j\uparrow}^{(+)} = (4\pi)^{\frac{1}{2}} \left\{ \sum_{l=0}^{\infty} \frac{e^{i\frac{\pi}{2}l}}{(2l+1)^{\frac{1}{2}}} \left\{ l g_{l} e^{i\delta_{l}} + (l+1) \cdot g_{-l-1} e^{i\delta_{-l-1}} \right\} Y_{l,0} (\theta^{i}, \phi^{i}) \right\}$$

$$= \frac{e^{i\frac{\pi}{2}l}}{(2l+1)^{\frac{1}{2}}} \cdot (l+1)^{\frac{1}{2}} \cdot l^{\frac{1}{2}} \cdot (-g_{l} e^{i\delta_{l}} + g_{-l-1} e^{i\delta_{-l-1}}) Y_{l,1} (\theta^{i}, \phi^{i})$$

$$= (3-40-a)$$

$$X_{j}^{(+)} = (4\pi)^{\frac{1}{2}} \left(\sum_{l=1}^{2} \frac{e^{i\frac{\pi}{2}l}}{(2l+1)^{\frac{1}{2}}} \cdot (l+1)^{\frac{1}{2}} \cdot l^{\frac{1}{2}} \cdot (g_{l}e^{i\delta_{l}} + g_{-l-1}e^{i\delta_{-l-1}}) \cdot Y_{l,-1}(\theta^{\dagger}\phi^{\dagger}) \right)$$

$$\sum_{l=0}^{2} \frac{e^{i\frac{\pi}{2}l}}{(2l+1)^{\frac{1}{2}}} \cdot \left\{ l \cdot g_{l} \cdot e^{i\delta_{l}} + (l+1) \cdot g_{-l-1} \cdot e^{i\delta_{-l-1}} \right\} \cdot Y_{l,0}(\theta^{\dagger}\phi^{\dagger})$$

$$(3-40-b)$$

where the notation $G_{\mathcal{K}}$ and $\eta_{\mathcal{K}}$ are used for the state elastically scattered by the potential of the excited-state atom in the direction $\mathbf{k} = (K_f, \theta, \phi), g_{\mathcal{K}}$ and $\delta_{\mathcal{K}}$ for the state elastically scattered by the potential of the ground-state atom in the direction of $\mathbf{k}' = (K_i, 0, 0)$ and the coordinates of the incident or scattered electrons are represented by $\mathbf{r}' = (r, \theta', \phi')$. The suffix 0 of X is omitted for simplicity (see equation (3-29)). The sign in front of $\eta_{\mathcal{K}}$ changes depending upon the boundary conditions of incoming waves.

Using the
$$a \stackrel{\imath}{l}_{\mu}$$
 and $b \stackrel{\imath}{l}_{\mu}$ defined by

$$a_{l\mu}^{1} = \frac{4\pi e^{i\frac{\pi}{2}l}}{2l+1} \left\{ (l+\mu+\frac{1}{2}) \cdot G_{l} \cdot e^{-i\eta}l + (l-\mu+\frac{1}{2}) \cdot G_{-l-1} \cdot e^{-i\eta}-l-1 \right\}$$
(3-41-a)

$$b_{l\mu}^{1} = -\frac{4\pi e^{i\frac{\pi}{2}l}}{2l+1} \cdot (l-\mu+\frac{1}{2})^{\frac{1}{2}} \cdot (l+\mu+\frac{1}{2})^{\frac{1}{2}} \cdot (-G_{l} \cdot e^{-i\eta}l + G_{-l-1} \cdot e^{-i\eta}-l-1)$$
(3-41-b)

$$a_{l}^{2} = \frac{(4\pi)^{\frac{1}{2}} e^{i\frac{\pi}{2}l}}{(2l+1)^{\frac{1}{2}}} (l \cdot g_{l} \cdot e^{i\delta_{l}} + (l+1) \cdot g_{-l-1} \cdot e^{i\delta_{-l-1}})$$
(3-42-a)

$$b_{l}^{2} = \frac{(4\pi)^{\frac{1}{2}} e^{i\frac{\pi}{2}l}}{(2l+1)^{\frac{1}{2}}} (l+1)^{\frac{1}{2}} \cdot l^{\frac{1}{2}} \cdot (-g_{l} \cdot e^{i\delta}l + g_{-l-1} \cdot e^{i\delta}-l-1), \qquad (3-42-b)$$

we can rewrite equations (3-39) and (3-40) as follows;

$$X_{i \uparrow}^{(-)} = \left(\sum_{l=0}^{\Sigma} \sum_{\mu} a_{l\mu}^{1} \cdot Y_{l,\mu+\frac{1}{2}} (\theta, \phi) \cdot Y_{l,\mu+\frac{1}{2}}^{*} (\theta', \phi') \right)$$

$$\left(\sum_{l=1}^{\Sigma} \sum_{\mu} b_{l\mu}^{1} \cdot Y_{l,\mu+\frac{1}{2}} (\theta, \phi) \cdot Y_{l,\mu-\frac{1}{2}}^{*} (\theta', \phi') \right)$$
(3-43-a)

$$X_{i}^{(-)} = \left(\sum_{l=1}^{\Sigma} \sum_{\mu} b_{l\mu}^{1} \cdot Y_{l,\mu-\frac{1}{2}}(\theta, \phi) \cdot Y_{l,\mu+\frac{1}{2}}^{*}(\theta', \phi') \right)$$

$$\left(\sum_{l=0}^{\Sigma} \sum_{\mu} a_{l,-\mu}^{1} \cdot Y_{l,\mu-\frac{1}{2}}^{*}(\theta, \phi) \cdot Y_{l,\mu-\frac{1}{2}}^{*}(\theta', \phi') \right)$$
(3-43-b)

$$X_{j}^{(+)} = \begin{pmatrix} \sum_{l=0}^{\mathcal{L}} a_{l}^{2} \cdot Y_{l,0} & (\theta^{\scriptscriptstyle l}, \phi^{\scriptscriptstyle l}) \\ \sum_{l=1}^{\mathcal{L}} b_{l}^{2} \cdot Y_{l,1} & (\theta^{\scriptscriptstyle l}, \phi) \end{pmatrix}$$

$$(3-44-a)$$

$$X_{j}^{(+)} = \begin{pmatrix} \sum_{l=1}^{\mathcal{L}} b_{l}^{2} \cdot Y_{l,-1} & (\theta', \phi') \\ \sum_{l=0}^{\mathcal{L}} a_{l}^{2} \cdot Y_{l,0} & (\theta', \phi') \end{pmatrix}$$

$$(3-44-b)$$

Then T-matrix of equation (3-29) for various spin states are expressed as

$$\begin{split} T^m_{\uparrow\uparrow} &= \langle \, X^{(-)}_{i\,\uparrow} \, | \, V^m_{\,0\,1} \, | \, X^{(+)}_{j\,\uparrow} \, \rangle \\ &= \sum_{l \,=\, 0} \sum_{l \,=\, 0} \sum_{\mu} \, (a^{1*}_{l\,\mu} \, | \, v_{0\,1} \, | \, a^2_{l'}) \, (Y_{l\,,\mu+\frac{1}{2}}, Y^*_{1m} \cdot Y_{l',0}) \, Y^*_{l\,,\mu+\frac{1}{2}} \, (\theta \, , \phi) \\ &+ \sum_{l \,=\, 1} \sum_{l \,=\, 1} \sum_{\mu} \, (b^{1*}_{l\,\mu} \, | \, v_{0\,1} \, | \, b^2_{l\,,}) \, (Y_{l\,,\mu-\frac{1}{2}}, Y^*_{1m} \cdot Y_{l',1}) \, \cdot \, Y^*_{l\,,\mu+\frac{1}{2}} \, (\theta \, , \phi) \end{split}$$

$$\begin{split} &= \sum_{l=1}^{L} \left(a_{l} \sum_{,-l/2+m}^{1} |v_{01}| |a_{l-1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \frac{l}{2l+1}\right)^{\frac{1}{2}} C \ (l-1,1,l;0,m) \ Y_{l,m}^{*} \\ &- \sum_{l=0}^{L} \left(a_{l} \sum_{,-l/2+m}^{1} |v_{01}| |a_{l+1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \frac{l+1}{2l+1}\right)^{\frac{1}{2}} C \ (l+1,1,l;0,m) \ Y_{l,m}^{*} \\ &+ \sum_{l=1}^{L} \left(b_{l} \sum_{,-l/2+m}^{1} |v_{01}| |b_{l+1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \frac{l+1}{2l+1}\right)^{\frac{1}{2}} C \ (l+1,1,l;0,m) \ Y_{l,m}^{*} \\ &- \sum_{l=2}^{L} \left(b_{l} \sum_{,-l/2+m}^{1} |v_{01}| |b_{l-1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \frac{l}{2l+1}\right)^{\frac{1}{2}} C \ (l-1,1,l;0,m) \ Y_{l,m}^{*} \\ &- \sum_{l=2}^{L} \left(b_{l} \sum_{,-l/2+m}^{1} |v_{01}| |b_{l-1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \frac{l}{2l+1}\right)^{\frac{1}{2}} C \ (l-1,1,l;0,m) \ Y_{l,m}^{*} \\ &= \sum_{l=1}^{L} \sum_{l=0}^{L} \sum_{l} \left(b_{l,-l/2+m}^{1} |v_{01}| |a_{l-1}^{2}\right) \left(Y_{l,\mu+\frac{1}{2}} Y_{l,m}^{*} Y_{l',l}^{*}\right) Y_{l,\mu-\frac{1}{2}} \left(\theta,\phi\right) \\ &= \sum_{l=1}^{L} \sum_{l=0}^{L} \sum_{l} \left(a_{l,-\mu}^{1} |v_{01}| |a_{l-1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \left(\frac{l}{2l+1}\right)^{\frac{1}{2}} C \ (l-1,1,l;0,m) \ Y_{l,m-1}^{*} \\ &- \sum_{l=1}^{L} b_{l,-\frac{1}{2}+m}^{1} |v_{01}| |a_{l-1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \left(\frac{l+1}{2l+1}\right)^{\frac{1}{2}} C \ (l+1,1,l;0,m) \ Y_{l,m-1}^{*} \\ &+ \sum_{l=0}^{L} \left(a_{l,-m+\frac{1}{2}} |v_{01}| |a_{l-1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \left(\frac{l+1}{2l+1}\right)^{\frac{1}{2}} C \ (l+1,1,l;0,m) \ Y_{l,m-1}^{*} \\ &+ \sum_{l=0}^{L} \left(a_{l,-m+\frac{1}{2}} |v_{01}| |a_{l-1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \left(\frac{l+1}{2l+1}\right)^{\frac{1}{2}} C \ (l+1,1,l;0,m) \ Y_{l,m-1}^{*} \\ &+ \sum_{l=0}^{L} \left(a_{l,-m+\frac{1}{2}} |v_{01}| |a_{l-1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \left(\frac{l+1}{2l+1}\right)^{\frac{1}{2}} C \ (l+1,1,l;0,m) \ Y_{l,-1+m}^{*} \\ &- \sum_{l=1}^{L} \left(a_{l,-m+\frac{1}{2}} |v_{01}| |a_{l-1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \left(\frac{l+1}{2l+1}\right)^{\frac{1}{2}} C \ (l+1,1,l;0,m) \ Y_{l,-1+m}^{*} \\ &- \sum_{l=1}^{L} \left(a_{l,-m+\frac{1}{2}} |v_{01}| |a_{l-1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \left(\frac{l+1}{2l+1}\right)^{\frac{1}{2}} C \ (l+1,1,l;0,m) \ Y_{l,-1+m}^{*} \\ &- \sum_{l=1}^{L} \left(a_{l,-m+\frac{1}{2}} |v_{01}| |a_{l-1}^{2}\right) \left(\frac{3}{4\pi}\right)^{\frac{1}{2}} \left(\frac{l+1}{2l+1}\right)^{\frac{1}{2}} C \ (l+1,1,l;0,m) \ Y_{l,-1+m}^{*} \\ &+ \sum_{$$

$$\begin{split} T^{m}_{\downarrow\uparrow} &= < X^{(-)}_{i\uparrow} \mid V^{m}_{01} \mid X^{(+)}_{j\downarrow} > \\ &= \sum_{l=0}^{S} \sum_{l'=1,\mu} (a_{l,\mu}^{-1*} \mid v_{01} \mid b_{l'}^{2}) (Y_{l,\mu+\frac{1}{2}}, Y_{1m}^{*} \mid Y_{l',-1}^{*}) \mid Y_{l,\mu+\frac{1}{2}}^{*} (\theta, \phi) \\ &+ \sum_{l=1}^{S} \sum_{l'=0,\mu} (b_{l,\mu}^{-1*} \mid v_{01} \mid a_{l'}^{2}) (Y_{l,\mu-\frac{1}{2}}, Y_{1m}^{*} \mid Y_{l',0}^{*}) \mid Y_{l,\mu+\frac{1}{2}}^{*} (\theta, \phi) \\ &= \sum_{l=0}^{S} (a_{l,m+\frac{1}{2}} \mid v_{01} \mid b_{l+1}^{-2}) (\frac{3}{4\pi})^{\frac{1}{2}} (\frac{l+1}{2l+1})^{\frac{1}{2}} C(l+1, 1, l; 1, m) \mid Y_{l,m+1}^{*} \\ &- \sum_{l=2}^{S} (a_{l,m+\frac{1}{2}} \mid v_{01} \mid b_{l-1}^{-2}) (\frac{3}{4\pi})^{\frac{1}{2}} (\frac{l}{2l+1})^{\frac{1}{2}} C(l-1, 1, l; 1, m) \mid Y_{l,m+1}^{*} \end{split}$$

(3-45-b)

$$+ \sum_{l=1}^{\mathcal{L}} (b_{l,m+\frac{1}{2}}^{1 *} | v_{01}^{1} | a_{l-1}^{2}) (\frac{3}{4\pi})^{\frac{1}{2}} (\frac{l}{2l+1})^{\frac{1}{2}} C (l-1,1,l;0,m) Y_{l,m+1}^{*} \\ - \sum_{l=1}^{\mathcal{L}} (b_{l,m+\frac{1}{2}}^{1 *} | v_{01}^{1} | a_{l+1}^{2}) (\frac{3}{4\pi})^{\frac{1}{2}} (\frac{l+1}{2l+1})^{\frac{1}{2}} C (l+1,1,l;0,m) Y_{l,m+1}^{*}$$

$$(3-45-c)$$

$$T_{\downarrow\downarrow}^{m} = \langle X_{i\downarrow}^{(+)} | V_{01}^{m} | X_{j\downarrow}^{(+)} \rangle$$

$$= \sum_{l=1}^{L} \sum_{l=1}^{L} \sum_{\mu} \langle b | l_{1}^{1*} | v_{01} | b | l_{1}^{2} \rangle \langle Y_{l,\mu+1/2}, Y_{1m}^{*} Y_{l,-1} \rangle Y_{l,\mu-1/2}^{*} \langle \theta, \phi \rangle$$

$$+ \sum_{l=0}^{L} \sum_{l=0}^{L} \sum_{\mu} \langle a | l_{1,-\mu}^{1*} | v_{01} | a | l_{1}^{2} \rangle \langle Y_{l,\mu-1/2}, Y_{1m}^{*} Y_{l,0} \rangle Y_{l,\mu-1/2}^{*} \langle \theta, \phi \rangle$$

$$= \sum_{l=1}^{L} \langle b | l_{1,m+1/2}^{1*} | v_{01} | b | l_{1}^{2} \rangle \langle \frac{3}{4\pi} \rangle^{1/2} \langle \frac{l+1}{2l+1} \rangle^{1/2} C \langle l+1,1,l;1,m \rangle Y_{l,m}^{*}$$

$$- \sum_{l=2}^{L} \langle b | l_{1,m+1/2}^{1*} | v_{01} | b | l_{1}^{2} \rangle \langle \frac{3}{4\pi} \rangle^{1/2} \langle \frac{l}{2l+1} \rangle^{1/2} C \langle l-1,1,l;1,m \rangle Y_{l,m}^{*}$$

$$+ \sum_{l=1}^{L} \langle a | l_{1,-m-1/2}^{1*} | v_{01} | a | l_{1}^{2} \rangle \langle \frac{3}{4\pi} \rangle^{1/2} \langle \frac{l}{2l+1} \rangle^{1/2} C \langle l-1,1,l;0,m \rangle Y_{l,m}^{*}$$

$$- \sum_{l=0}^{L} \langle a | l_{1,-m-1/2}^{1*} | v_{01} | a | l_{1}^{2} \rangle \langle \frac{3}{4\pi} \rangle^{1/2} \langle \frac{l+1}{2l+1} \rangle^{1/2} C \langle l+1,1,l;0,m \rangle Y_{l,m}^{*}$$

$$- \sum_{l=0}^{L} \langle a | l_{1,-m-1/2}^{1*} | v_{01} | a | l_{1}^{2} \rangle \langle \frac{3}{4\pi} \rangle^{1/2} \langle \frac{l+1}{2l+1} \rangle^{1/2} C \langle l+1,1,l;0,m \rangle Y_{l,m}^{*}$$

$$- \langle a | l_{1,-m-1/2}^{1*} | v_{01} | a | l_{1}^{2} \rangle \langle \frac{3}{4\pi} \rangle^{1/2} \langle \frac{l+1}{2l+1} \rangle^{1/2} C \langle l+1,1,l;0,m \rangle Y_{l,m}^{*}$$

$$- \langle a | l_{1,-m-1/2}^{1*} | v_{01} | a | l_{1}^{2} \rangle \langle \frac{3}{4\pi} \rangle^{1/2} \langle \frac{l+1}{2l+1} \rangle^{1/2} C \langle l+1,1,l;0,m \rangle Y_{l,m}^{*}$$

$$- \langle a | l_{1,-m-1/2}^{1*} | v_{01} | a | l_{1}^{2} \rangle \langle \frac{3}{4\pi} \rangle^{1/2} \langle \frac{l+1}{2l+1} \rangle^{1/2} C \langle l+1,1,l;l;0,m \rangle Y_{l,m}^{*}$$

$$- \langle a | l_{1,-m-1/2}^{1*} | v_{01} | a | l_{1}^{2} \rangle \langle \frac{3}{4\pi} \rangle^{1/2} \langle \frac{l+1}{2l+1} \rangle^{1/2} C \langle l+1,1,l;l;0,m \rangle Y_{l,m}^{*}$$

$$- \langle a | l_{1,-m-1/2}^{1*} | v_{01} | a | l_{1,-m-1/2}^{2} \rangle \langle \frac{3}{4\pi} \rangle^{1/2} \langle \frac{l+1}{2l+1} \rangle^{1/2} C \langle l+1,1,l;l;0,m \rangle Y_{l,m}^{*}$$

$$- \langle a | l_{1,-m-1/2}^{1*} | v_{01} | a | l_{1,-m-1/2}^{2} \rangle \langle \frac{3}{4\pi} \rangle^{1/2} \langle \frac{l+1}{2l+1} \rangle^{1/2} C \langle l+1,1,l;l;0,m \rangle Y_{l,m}^{*}$$

Here the equation (3-38) and Table 3-1 are used.

It is easily shown that

$$T_{M}^{1} = i \phi_{=-} T_{U}^{-1} e^{-i \phi_{=-}} T_{1}^{1}$$
 (3-46-a)

$$T_{\uparrow\uparrow}^{0} = -T_{\downarrow\downarrow}^{0} = T_{1}^{0} \tag{3-46-b}$$

$$T_{\uparrow\uparrow}^{-1} e^{-i\phi} = T_{\downarrow\downarrow}^{1} e^{i\phi} = T_{1}^{-1}$$
 (3-46-c)

$$T_{11}^{1} = 2i\phi = T_{11}^{-1} e^{-2i\phi} = T_{2}^{1}$$
 (3-46-d)

$$T_{\downarrow\uparrow}^{0} \quad e^{i\phi} = -T_{\downarrow\downarrow}^{0} \quad e^{-i\phi} = T_{2}^{0}$$
 (3-46-e)

$$T_{\downarrow\uparrow}^{-1} = T_{\uparrow\downarrow}^{1} = T_{2}^{-1} \tag{3-46-f}$$

Comparison of the equations (3-41) and (3-42) with the equation (2-40) shows that the coefficients $a_l{}^i(b_l{}^i)$ represent the direct scattering (spin-flip) during the elastic processes occuring before and after the inelastic single process. Hence, the processes occuring during inelastic scattering are explained schematically from equation (3-45), e.g. $T_{\text{N}(\text{M})}^m$ represents the process that initially, an incident electron undergoes a direct (spin-flip) elastic process followed by another single inelastic process and finally undergoes a spin-flip(direct) elastic process once more.

The relationship between T-matrix and scattering amplitude is given by (Schiff 1955)

$$f = -\frac{1}{2\pi}T. (3-47)$$

Differential cross section and spin polarization are derived from the same procedures shown in Sec. 2-3. For the initial electron beams of $\phi_i = \binom{A}{B} e^{iKz}$ having polarization $\mathbf{p} = (p_x, p_y, p_z)$ the cross section is represented as,

$$\frac{\mathrm{d}\,\sigma_{ine\,l}}{\mathrm{d}\,\Omega} = \frac{1}{4\,\pi^{2}} \frac{K_{f}}{K_{i}} \langle \Sigma_{j=1,0,j-1} \left\{ |AT_{11}^{j} + BT_{11}^{j}|^{2} + |BT_{11}^{j} + AT_{11}^{j}|^{2} |^{2} \right\} >
= \frac{1}{4\pi^{2}} \frac{K_{f}}{K_{i}} \sum_{j=1,0,j-1} \left\{ \sum_{l=1,2} |T_{l}^{j}|^{2} - 2 \operatorname{Im} \cdot (T_{1}^{j*} \cdot T_{2}^{j}) \cdot (-p_{x} \sin\phi + p_{y} \cos\phi) \right\}$$
(3-48)

where K_i and K_f are wave numbers of incident and scattered electrons. The comparison to equation (2-45) in Sec.2-3 shows a similar relation between the elastic and inelastic scattering cross section. Then the Sherman function S_{inel} in inelastic scattering, the quantity relating to left-right asymmetry, may also be defined as

$$S_{inel} = -2 \sum_{j=-1,0,1}^{I} Im(T_1^{j*} T_2^{j}) / \sum_{l=1,2}^{I} \sum_{j=1,0,-1}^{I} |T_l^{j}|^2$$
(3-49)

One the other hand, the ESP of inelastically scattered electrons are expressed as

$$P_{inel} = \langle \sigma \rangle$$

$$= \sum_{i=1}^{n} (A_{i}^{*} T_{i}^{i} + B_{i}^{*} T_{i}^{i} + B_{i}^{*} T_{i}^{i} + A_{i}^{*} T_{i}^{i} + A_{i}^{*} T_{i}^{i} + B_{i}^{*} T_{i}^{i} + B_{i}^{*$$

where σ denotes the Pauli matrix and < > denotes averages over all incident spin directions. The actual calculation shows that the S_{inel} equals the P_{inel} .

As can be easily seen from equations (3-49) and (3-51), the effects of ESP becomes inexistent if all T^l_j is a real or pure imaginary number i.e. the phase shifts η_{κ} and δ_{κ} related to elastic scattering play an essential roles on the polarization effect of inelastic scattering.

3-4. Choice of Atomic Wave Function

The atomic potential used is the non-relativistic Hartree potential analytically expressed by Byatt (1956) (See Sec.2-2-3). The radial wave function of the ground state (6s)² and the excited state (6s)(6p) of the mercury atom used are those calculated by McConnell and Moiseiwitsch (1968) using the Coulomb approximation, since the results obtained using these wave functions were in excellent agreement with experiments as has been referred to in Sec.3-1. McConnell and Moiseiwitsch (1968) fitted these wave functions to a sum of exponentials

$$R_{00} = A_{0} \exp(-a_{0}r) + B_{0} \exp(-b_{0}r)$$

$$R_{10} = rA_{0}' \exp(-a_{0}'r) + B_{0}' \exp(-b_{0}'r)$$

$$R_{11} = r(A_{1} \exp(-a_{1}r) + B_{1} \exp(-b_{1}r)), \qquad (3-52-a)$$

with

$$A_0 = 0.907 \times 10^{-4}$$
, $a_0 = 0.612 \times 10^{-2}$, $B_0 = -0.425 \times 10^{-4}$, $b_0 = 0.144 \times 10^{-1}$
 $A_0' = 0.786 \times 10^{-6}$, $a_0' = 0.884 \times 10^{-2}$, $B_0' = -0.131 \times 10^{-3}$, $b_0' = 0.196 \times 10^{-1}$
 $A_1 = 0.103 \times 10^{-6}$, $a_1 = 0.410 \times 10^{-2}$, $B_1 = 0.303 \times 10^{-6}$, $b_1 = 0.164 \times 10^{-1}$, (3-52-b)

and evaluated the total $6^{1}P$ and $6^{3}P$ excitation cross section. The results calculated for these wave functions are shown in Fig.3-1, together with the

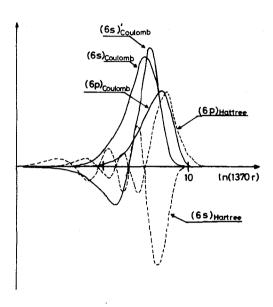


Fig.3-1. Radial wave functions for mercury, $(6s)_{Coulomb}$; Coulomb approximation for (6s) electron in $(6s)^2$ state, $(6s)'_{Coulomb}$; Coulomb approximation for (6s) electron in (6s)(6p) state, $(6p)_{Coulomb}$; Coulomb approximation for (6p) electron in (6s)(6p) state, $(6s)_{Hartree}$; Hartree approximation for (6s) electron in $(6s)^2$ and (6s)(6p) electron states and $(6p)_{Hartree}$; Hartree approximation for (6p) electron in (6s) (6p) state. (McConnell and Moiseiwitsch (1968) and Mishra (1952)).

results of self-consistent wave functions using Hartree field for the 6s orbital of the normal state $(6s)^2$ of neutral Hg (Mishra 1952). Note that the axis of abscissa is written in log-scale i.e. the departure between functions near $r \sim 0$ is emphasized too much.

It was assumed in the Coulomb approximation that the active electrons

(6s and 6p electrons in the present case) behave like the electrons moving in a Coulomb field C/r having the same binding energy as the actual one, C being the excess charge on the nucleus when the active electrons are removed. Although the wave functions obtained in this way are not the eigenfunctions of the Coulomb field, it is expected that they have satisfactory profiles and magnitudes except those near $r \sim 0$ (Bates and Damgaard 1949). This approximation is justified because the probability of the electrons in question, which exist in the inner part of the atom where the potential departs from C/r, is slight. This can be demonstrated for the oscillator strength by comparing

$$\int_{0}^{r_{b}} R_{i} R_{f} r^{3} dr , \qquad (3-53-a)$$

and

$$\int_{r_{b}}^{\infty} {R_{i} R_{f} r^{3} dr}$$
(3-53-b)

where r_b is the boundary value of r at which the atomic potential behaves like $^{C}/r$, ^{R}i and ^{R}f initial and final radial wave functions respectively. Table 3-2 gives the relevant data for two cases of s-p transistions calculated using self-consistent wave functions (Bates and Damgaard 1949).

Table 3-2.

System	Transition	r_b (in unit of a_0)	$\int_0^{\mathbf{r}} \mathbf{b}$	$\int_{r_{b}}^{\infty}$
Na I	3s-4p	1.5	0.004	0.386
O II	3s-3p	2.0	0.05	4.02

Calculated results by McConnell and Moiseiwitsch agree well with the experiments. This confirms the usefulness of the Coulomb approximation, even though the 6s wave function used behaves like 1s or 2s electrons. The oscillator strength for the ${}^1P_1 \!\!\to\!\! {}^1S_0$ transitions are given by the formulae

$$f = 2 S^2 \sigma^2 / \lambda$$
 , (3-54-a)

where

$$\sigma^{2} = 1 \times 3 \left\{ \int_{0}^{\infty} R_{00} R_{11} r^{3} dr \right\}^{2}$$
 (3-54-b)

$$S = \int_0^\infty R_{00} R_{10} r^2 dr , \qquad (3-54-c)$$

and λ is the wave length of the radiation. Formula (3-54) results in the values

$$f_{coulomb} = 1.17 \tag{3-55-a}$$

$$f_{Mishra} = 4.76 \tag{3-55-b}$$

$$f_{Madison} = 8.8 \tag{3-55-c}$$

corresponding to the wave functions of Coulomb approximation (McConnell and Moiseiwitsch 1965), of self-consistent approximation by Mishra(1952) and of self-consistent approximation by Madison and Shelton (1973). Madison and Shelton calculated the wave function as the eigenfunction of relativistic atomic ground-state potential. $f_{Coulomb}$ is in close agreement with the experimental value 1,18 of Lulio (1965). This implies that the Coulomb approximated wave functions can closely represent the states of the real atomic electrons, particularly their spacial distribution.

3-5. Adopted Numerical Calculation Procedures

The calculation procedures of g_{κ} and G_{κ} in equation (3-42) are like those in Sec. 2-3, but here both the phases ϕ_{κ} and amplitudes A_{κ} will be estimated by the fourth order Lunge-Kutta process. ' B_{0} ', the normalization factor in equation (2-54-b) is determined by the first row of the equation (2-34).

The potential V(r) is expressed using the charge distribution ρ as

$$V'(r) = \frac{1}{r} \int_{0}^{r} \rho(r') r'^{2} dr' + \int_{r}^{\infty} \rho(r') r' dr'. \qquad (3-56)$$

The first and second term are called inner and outer shielding, respectively (Slater 1960). From equation (3-56) and ${}^{\rho}{}_{i(f)}(r)=e^2\mid R_{i(f)}\mid^2$ we can construct the potential field of an excited state atom, which is necessary for evaluation of G_{κ} in equation (3-39). The V_{01} changes very slowly and is greater than the atomic potential V_g and V_e at $r \ge 340$ and $r \ge 390$ respectively. This is because V_{01} behaves like r^{-2} asymptotically at large r, as has been pointed out in Sec.3-3. As the form factor is the long range potential,

the number of partial waves necessary for the evaluation of T-matrix becomes quite large in comparison to those of elastic scattering. However, the number of partial waves distorted by the atomic potential is like those necessary in elastic scattering calculations. Contributions from the distorted partial waves are estimated as follows: 1) Equations (2-51-a) and (2-51-b) are solved numerically by the fourth order Lunge-Kutta process (see Sec.2-4), and the integrations necessary to evaluate T-matrix are performed by trapezoidal rulefrom r=0.1 to $r=r_0$ where $V(r_0)\sim 0$. 2) The phase shifts are estimated at $r=r_0$ and the T-matrix is again integrated numerically to $r=r_1$ using the first row of equation (2-34), the expression of g_{κ} at large r and we took $r_1=13700$ in most cases. Contributions to the T-matrix from the higher order partial waves originate from only the asymptotic region of the form factor, then analytical expression of these is possible using the formula (Watson 1966).

$$\int_{0}^{\infty} \int_{\mu} (ax) \cdot J_{\nu}(bx) \cdot x^{\lambda} dx$$

$$= \frac{2^{\lambda} \cdot b^{\nu} \Gamma(\alpha)}{a^{\lambda+\mu+1} \Gamma(\nu+1) \cdot \Gamma(1-\beta)} F(\alpha, \beta, \nu+1; b^{2}/a^{2}) , \qquad (3-57-a)$$

where J_{μ} is the Bessel function of μ -th order, $\operatorname{Re}(\lambda)<1$, $\operatorname{Re}(\lambda+\mu+\nu)>-1$, a>b>0, $\alpha=(\lambda+\mu+\nu+1)$ /2, $\beta=(\lambda-\mu+\nu+1)$ /2 and F (α , β , γ ; x) the hypergeometric function defined by

$$F(\alpha,\beta,\gamma;z) = \frac{\Gamma(\gamma)}{\Gamma(\alpha)\Gamma(\beta)} \sum_{n=0}^{\infty} \frac{\Gamma(\alpha+n)\Gamma(\beta+n)}{\Gamma(\gamma+n)} \frac{z^n}{n!} \cdot (3-57-b)$$

Spherical harmonics are evaluated at each scattering angle using the recurrence relation as

$$Q_{l+1}^{m} = \left[\frac{(2l+1)(2l+3)}{(l+m+1)(l-m+1)}\right]^{\frac{1}{2}} \cdot z \cdot Q_{l}^{m} - \left[\frac{(2l+3)(l+m)(l-m)}{(2l-1)(l+m+1)(l-m+1)}\right]^{\frac{1}{2}} \cdot Q_{l-1}^{m}, (3-58)$$

where $Q_{l}^{m}(\theta) = Y_{l}^{m}(\theta,\phi) \, \mathrm{e}^{-i\,m\,\phi}$ with initial conditions

$$Q_0^0 = (1/4\pi)^{\frac{1}{2}} \tag{3-59-a}$$

$$Q_1^0 = (3/4\pi)^{1/2} \cos \theta \tag{3-59-b}$$

$$Q_1^{-1} = (3/8\pi)^{\frac{1}{2}} \sin \theta \tag{3-59-c}$$

$$Q_2^0 = (5/4\pi)^{\frac{1}{2}} (3\cos^2\theta - 1)/2$$
 (3-59-d)

$$Q_{2}^{-1} = (15/8\pi)^{1/2} \sin\theta \cdot \cos\theta$$
 (3-59-e)

$$Q_{2}^{-2} = (15/32\pi)^{\frac{1}{2}} \sin^{2}\theta \qquad (3-59-f)$$

which are derived from

$$Q_l^m = \frac{1}{2^l l!} (-\sin\theta)^m (d/d\cos\theta)^{l+m} (\cos^2\theta - 1)^l . \tag{3-60}$$

The flow chart and the list of program for the present calculation is shown in Appendix 6.

3-6. Results and Discussion

The DWB calculations are performed for two form factors F_C and F_M , where F_C is obtained using the Coulomb approximated wave functions and F_M is obtained from that used by Madison and Shelton (1973) with a slight modification (see Fig.3-2) which is performed to fit F_M to analytical form for convenience in computer calculation. Actual calculation shows that the modification of this kind incurs little difference on calculated cross section and spin polarization. The calculated results are shown in Figs.

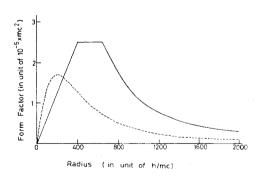


Fig.3-2. Form factor for mercury,—; calculated using Coulomb approximated wave functions, ---- used by Madison and Shelton (1973) (calculated using Hartree wave function) with a little modification.

3-3 to 3-7 for electron impact energies between 50 and 500 eV. Each figure gives 1) a DWB calculation using F_C , 2) a DWB calculation using F_M , 3) an elastic scattering calculation of energy E eV using atomic ground-state potential, 4) an elastic scattering calculation of energy E-6.7 eV using atomic excited-state potential and 5) experimental data when available. The experimental data are that of Hanne et al.(1972), Gronemeier (1970) and Yamazaki et al. (1977-c).

The elastic data of Gronemeier is normalized to the present theoretical results at θ =80° (E=100 eV) and at θ =90° (E=300 eV). The number of partial waves estimated numerically ranged from 15 at an incident electron energy of 50 eV, to 43 at an incident electron energy of 500 eV. The total number of partial waves ranged from 125(141) to 522(994) for F_C (F_M) case in the same energy regions.

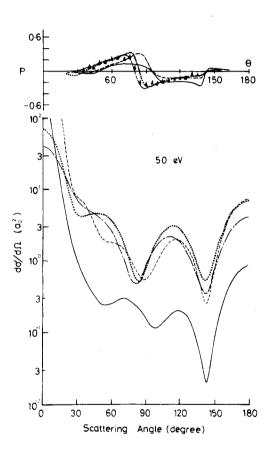


Fig.3-3. Spin polarization and differential cross section for mercury at incident electron energy of 50 eV. (——: DWB calculation for $6s6p^1P$ excitation using F_C , ----: DWB calculation for $6s6p^1P$ excitation using F_M , elastic scattering by ground-state atomic potential,: elastic scattering by excited-state atomic potential, \triangle : experimental results of spin polarization for 6^1P excitation (Hanne et al. 1972).

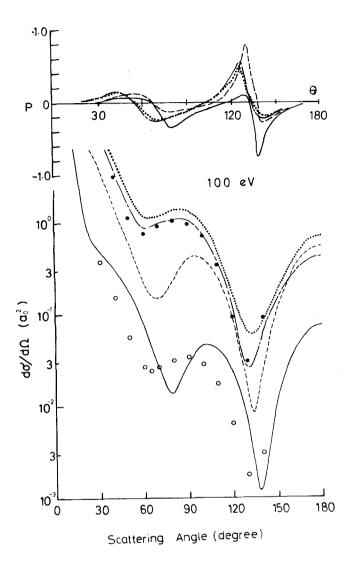


Fig.3-4. Same as Fig.3-3 except here the energy is 100 eV. (\bullet : experimental results for the elastic scattering cross section normalized to theoretical results at θ =80° and \circ : experimental results for the 6¹P excitation cross section (Gronemeier 1970)).

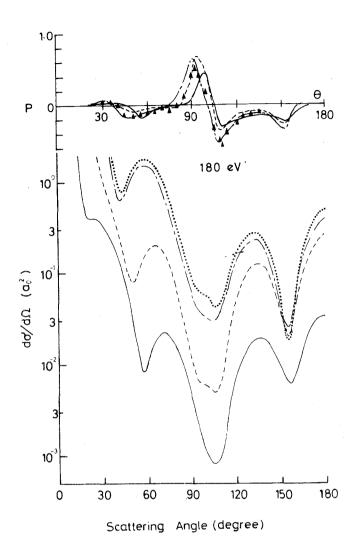


Fig.3-5. Same as Fig.3-3 except here the energy is 180 eV. The curve of spin polarization for elastic scattering by excited-state atomic potential is almost similar to that by ground-state atomic potential and is neglected for simplicity. (A:experimental results of polarization for 6¹P excitation (Hanne et al. 1972))

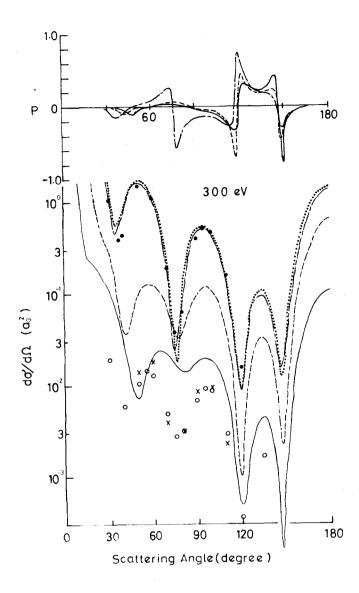


Fig. 3-6. Same as Fig. 3-3 except here the energy is 300 eV. (•: experimental results for the elastic scattering cross section normalized to theoretical results at θ =90°, o: experimental results for the 6¹P excitation cross section (Gronemeier 1970) and ×: experimental results for the 6¹P excitation cross section (Yamazaki et al. 1977c) The curve of spin polarization for elastic scattering by excited state atomic potential is neglected for simplicity.)

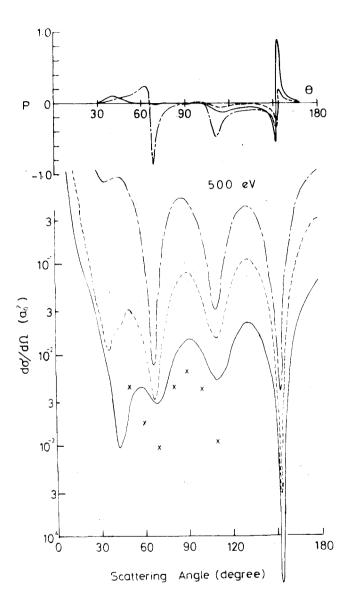


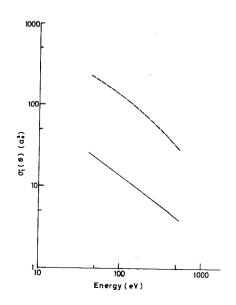
Fig.3-7. Same as Fig.3-3 except here the energy is 500 eV. (The curves of spin polarization and cross section for elastic scattering by excited-state atomic potential are neglected for simplicity).

Figures 3-3 to 3-7 show that the DWB calculation using F_M gives a differential cross section several times larger than that using $F_{\rm C}$. As is seen in Fig. 3-2, these differences originate from the remarkable difference between the form factors. The atomic wave functions used to calculate F_M were determined by Madison and Shelton as the bound state eigenfunction of the Hartree field, in order to assure the orthogonality between the atomic and free-state wave functions, which reduces computing time drastically if exchange scattering is taken into account. The atomic wave functions obtained in this way spread over a broad radial region causing overestimations of the differential and total cross sections. On the other hand, the atomic wave functions used to calculate $F_{\mathcal{C}}$ are determined as the solution of the Coulomb field, having the same binding energy as the actual one (see Sec. 3-4), which provide differential and total cross sections in close agreement with experiments. The extremum points of the cross section calculated using ${\it F}_{\it C}$ shift to higher scattering angles at forward scattering in comparison to that using F_M throughout the present calculations. In the case of ${\it F_{C}}$, the order of partial waves which contribute primarily to the T-matrix shifts lower as compared to F_M , which can be seen in Fig. 3-2. This situation means that the "effective impact energy" in the case of F_C is smaller than that in the case of F_M for forward scattering where higher order partial waves play important roles, which results in shifts of the extremum points.

A comparison to experiments is discussed in Chapter 5.

In regard to the total cross section, the results obtained using F_C agree well with McConnell and Moiseiwitsch, while the results using F_M are about 10 times greater than those using F_C (see Fig. 3-8).

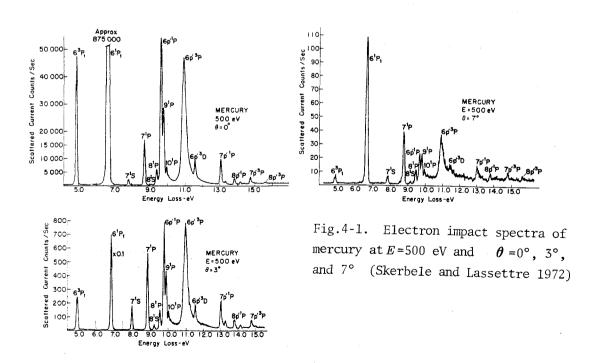
Fig. 3-8. Total cross sections for $6^{1}P$ excitation of mercury by electron impact calculated using DWB approximation (———; F_{C} ,———; F_{M}).



CHAPTER 4. MEASUREMENT OF LOSS SPECTRA

4-1 Introduction

Table 1-1 shows that a few experimental data exist concerning the loss spectra of mercury at intermediate impact energies and at large scattering angles. This situation is very surprising considering that the electron-mercury system was one of the most popular and accessible, due to its large scattering cross section and suitable vapour pressure at room temperature with little influence on the gun heater in the early stages of scattering experiments. A primary reasons for this may be deficiencies of the theoretical investigations. Theoretical treatments of inelastic scattering for heavy elements have been very difficult because of the complexities of the atomic structure and scattering process at intermediate energies. The recently developed high speed digital computer, however, makes it possible to treat accurate and complex theories, as is given in Chapter 3. Furthermore, in recent experiments on electron-mercury scattering at impact energies of several hundreds of eV at forward scattering, it was found that the relative



intensities between various excitation channels changed rapidly as a function of scattering angles (0° to 7°) (Skerbele and Lassettre 1972), causing interest on the behaviour of the loss spectra at large scattering angles. Fig.4-1 shows that transitions to P-state are strong in contrast to the other transitions as is surmised in Sec.3-3.

Also, from a practical viewpoint, knowledge concerning the differential cross section of inelastic scattering at large angles for mercury is of basic importance for experimental arrangement of the ESP detector using mercury vapour as a target. Optimum conditions of the ESP detector such as impact energy, scattering angle and angular resolution, can be determined by theoretical calculation of elastic differential scattering cross section and spin polarization. However, the optimum condition of energy resolution for the ESP detector can be estimated only by the cross section of inelastic scattering.

This chapter aimed at obtaining the impact spectra for mercury at intermediate energies and large scattering angles, which leads to better understanding of the optimum conditions for the ESP detector in practical use as well.

4-2 Apparatus — Design and Performance

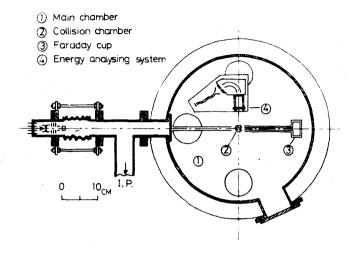
4-2-1 Vacuum System

The apparatus used consists of a primary beam source, a gas cell as a collision chamber and 127° cylindrical type energy analyser system.

The loss spectra were measured by scanning the deflecting voltage of the analyser. An outer view of the apparatus is shown in Fig.4-2 by removing the top cover of the vacuum chamber and the mercury reservoir.

Fig.4-3 shows cross sectional drawings of the system. The vacuum chamber is a 20 cm high cylinder and 40 cm in diameter, evacuated by a Fig.600 %/s oil diffusion pump with

Fig.4-2. Top view of the main chamber removing the top covers of the chamber and energy analyser.



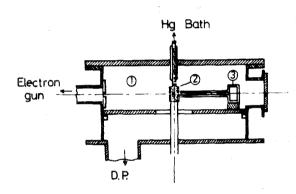


Fig.4-3. Cross section of the apparatus

a liquid nitrogen cooled baffle. The actual pumping speed is reduced to about 100 ℓ s by the baffle and the connection tube to the chamber, which provides a residual gas pressure of 10^{-7} Torr. Gas pressure increases to 10^{-5} Torr during operation due to mercury vapour. The vacuum system is sealed with Viton O-rings.

The collision chamber at the center of the vacuum chamber, shown in Fig.4-4, consists of two tight concentric cylinders. The outer cyclinder C_1 is static and the inner C_2 rotatable. The inner cylinder is 40 mm high and 18 mm of inner diameter. The collision chamber is pumped through four apertures A_2 , A_3 , A_4 and A'_4 so that the incident and scattered electrons may pass. The collision chamber provides a scattering angle from 50° to

130° by utilization of the two apertures, A₄ and A'₄. The majority parts in the chamber were made of stainless steel to avoid amalgamating with mercury vapour and an excessive magnetic field. However, some parts are made of gold plated copper to avoid charging-up effects.

Tungsten ribbon (0.025 \times 0.75 mm²) was used as a cathode filament of the electron gun, which provides an electron beam current of 2-20 μ A at the accelerating energies of 300-2000 eV with a beam diameter of less than 3 mm/s at a relative distance of 300 mm from the electron gun.

As can be seen in Fig.4-3, the gun is mechanically adjustable from outside the vacuum by means of three screws. The beam can be additionally adjusted by an electrostatic defector.

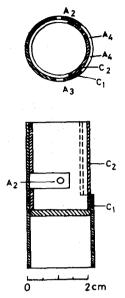


Fig.4-4. Cross section of the collision chamber.

The electron beam current is stabilized to about 0.1% for all beam current and accelerating energy ranges by controlling the filament current automatically (see Sec.4-2-5). The gun assembly is differentially pumped from the main chamber through 3 mm/s round slits by a 40 ℓ /s ion pump to approx. 5×10^{-7} Torr to avoid instability caused by mercury vapour and to get longer life time of the filament.

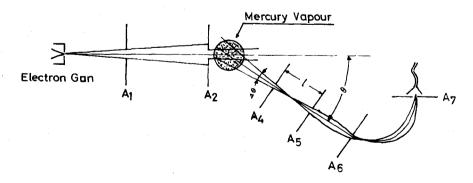


Fig.4-5. Scattering geometry (A_1 and A_2 ; round slit, A_4 , A_5 , A_6 and A_7 ; rectangular slit).

The scattering geometry is shown in Fig.4-5. Apertures A_1 , A_2 and A_3 are round and have diameter of 3,2 and 3 mm respectively, while A_4 , A_5 , A_6 and A_7 are rectangular, A_4 is 0.7 \times 5 mm² and the slit widths of A_5 , A_6 and A_7 vary from 0.1 to 3 mm with 5 mm height and set usually at 0.1 mm. The rectangular slits were adopted to obtain a high scattering intensity even in high angular resolution experiments. The distance between A_4 and A_5 was usually set at 50 mm, so the angular resolution $\Delta\theta$ is \approx 1°.

The scattering angle θ is defined as the angle formed by the line through the centers of the collimating apertures (A₁ and A₂) for the incident beam, and the line through the centers of the acceptance apertures at the collision chamber and in front of the decelerating asymmetric lens. It was estimated that the reproducibility of the scattering angle was $\pm 0.5^{\circ}$

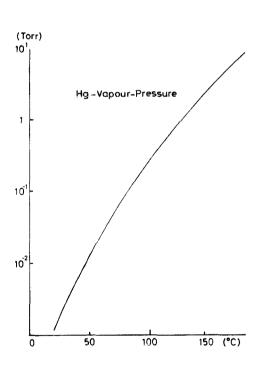


Fig.4-6. Relation of Hg vapour pressure to temperature (Weast 1972).

and the shift from the true scattering angle was less than $\pm 2^{\circ}$, taking into account the residual magnetic field as well. The mercury vapour is produced in a mercury bath which is automatically controlled to maintain a constant temperature of about 60° C resulting in vapour pressure $\approx 10^{-2}$ Torr (see Fig.4-6), and is led to the collision chamber by a pyrex tube whose temperature is higher than the mercury bath's to prevent condensation. All the heaters used are wound so as to be inductionless.

4-2-2. Magnetic Field

Charged particles in a magnetic field ${\it B}$ make a circular motion of radius ${\it r}$

$$r = \frac{\sqrt{2mE}}{qB} \quad , \tag{4-1}$$

where m is the mass of the charged particles, E the kinetic energy and q the charge of the particles. Then, the shift Δx of the charged particles is expressed as

$$\Delta x = \frac{x^2}{2r} = \frac{q B x^2}{2 \sqrt{2mE}}$$
 (4-2)

where x is the path length of the electron beam (see Fig.4-7). To make the angular shift smaller than the angular resolution $\varDelta\theta$, the terrestrial magnetic field B_t should be reduced to

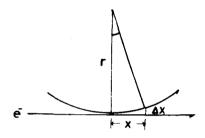


Fig.4-7. Relation between path length x and shifted distance Δx of electron in magnetic field.

$$B_t \leq \frac{2\sqrt{2mE \cdot \Delta\theta}}{qx}$$
 (4-3)

Using equation (4-3), the maximum residual magnetic field allowed in the present experiments is shown in Fig.4-8 for two path lengths.

The magnetic field is corrected by a Helmholz coil of 150 cm diameter and 40 cm height.

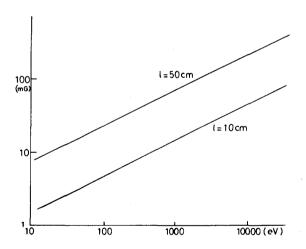


Fig.4-8. The maximum residual magnetic field allowable in the present experiments.

4-2-3 Energy Analyzer

The energy analyser is composed of a decelerating asymmetric three-slit lens, cylindrical 127° sector-type analyser and electron multiplier, as is shown in Figs.4-9 and 4-10. All gaps of the case of the energy analyser are sealed except for the slits, in order to prevent the secondary or backscattered electrons from straying into the electron multiplier.

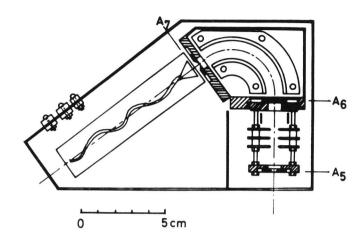


Fig.4-9. Cross section of the energy analyser composed of three-slit asymmetric lens, 127° sector type analyser and electron multiplier.

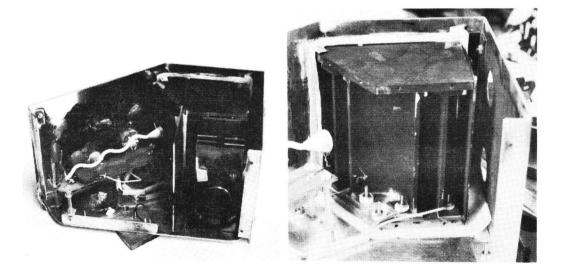


Fig.4-10. Outer view of the energy analyser removing the top and front covers (a), and sector-type 127° analyser removing the side covers (b).

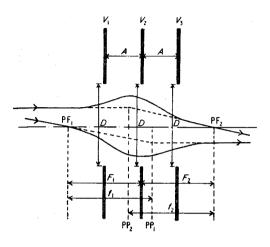


Fig.4-11. Geometry of the asymmetric three-aperture lens studied by Read (1970)

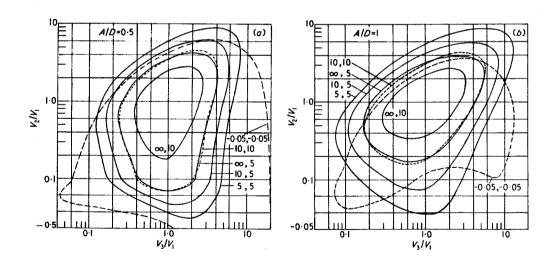


Fig.4-12. The focusing condition of the asymmetric three-aperture lens having A/D=0.5 and 1. The sets of numbers given in the figures show the distances between objective plane and lens, and between imaging plane and lens in unit of aperture diameter (Read, 1970).

An asymmetric three-slit lens is used to assure high energy resolution at rather high incident energies. The deflector plates are located behind this lens system for correction of the electron path.

The construction of the three-slit lens system was determined using the results calculated for the asymmetric three-aperture lens system by Read (1970,1971). The lens system studied by Read is shown in Fig.4-11, and the relationship between V_2/V_1 and V_3/V_1 is shown in Fig.4-12, where V_1 , V_2 and V_3 are the lens potential of the entrance, mediate and exit electrodes, measured with respect to the potential at which the electrons have zero kinetic energy. It can be seen that two focusing conditions generally exist and that the ratio of acceleration (deceleration) has an upper (lower) limit corresponding to the construction of the lens system. As there are no theoretical or experimental investigations for an asymmetric three-slit lens system, the focusing conditions were examined ex-

perimentally (see Fig.4-13). The deflecting voltage is swept sinusoidally from positive to negative values in order to sweep the image across the aperture in front of the Faraday cup (F.C.), and then the current to the

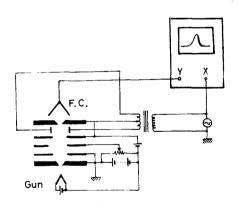


Fig.4-13. Schematic diagram of the electric circuit for the investigation of the focusing condition of the asymmetric three-slit lens.

Faraday cup goes from zero, to its maximum, and back to zero again. The shape of the curve of current measured with a Faraday cup against deflector voltage is displayed on an oscilloscope screen. The focusing condition is determined from the curve obtained in this way as conditions that provide the most high and narrow peak. The results are shown in Fig.4-14 where the dotted line shows that the theoretical results for the

0.5 0 0.5 1.0

Fig.4-14. Focusing condition of the three-slit lens for V = 300 eV (o) and $500 \text{ eV}(\times)$. (Dashed line shows theoretical results for an asymmetric three-aperture lens having similar construction as the three-slit lens (Read 1970).

asymmetric three-aperture lens having a similar construction to the slit lens used in the present experiments. (Read 1970).

The outer and inner radius of the sector analyser are 30 and 20 mm, respectively, and the height is 50 mm. As the width of slit A_5 , A_6 and A_7 is set at about 0.1 mm, this analyser provides an energy resolution of $E/\Delta E \sim r/2 \Delta r \sim 100$ where E is electron energy entering the slit of the sector analyser, ΔE energy resolution, r central radius of the slit of the analyser, and Δr width of the slit of the analyser, and the value is confirmed experimentally by the FWHM of the elastic scattering peak (see Fig.4-22).

The sector is coated with soot produced by burning liquid benzene, to minimize the generation of secondary electrons.

4-2-4 Detector

The energy analysed scattered electrons are detected by a channeltron electron multiplier (Murata Co., Ceratron Type EMW-1081E, see Fig.4-10) with an acceptance cone. The multiplier pulses are inductively coupled from the analysing system at a high voltage potential into a pre-amplifier

at earth potential. The pulses the pass through a pulse height analyser and are counted by a multi-channel scaler (M.C.S.).

The pulse height distributions (P.H.D.) are shown in Fig.4-15 as a function of the multiplier voltage. The multiplier is operated at 4500 eV to

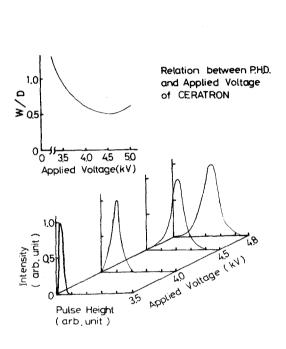


Fig.4-15. Relation between P.H.D. and applied voltage of Ceratron, and a pulse height resolution W/D of Ceratron as a function of applied voltage, where W is FWHM of P.H.D. and D the mean value of pulse height.

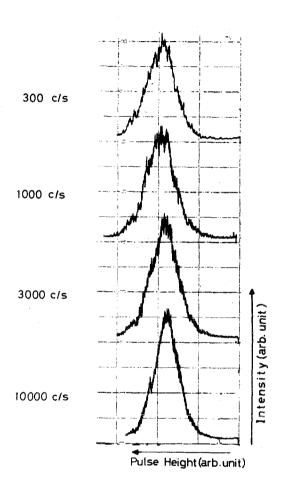


Fig.4-16. Relation between R.H.D. and count rate of Ceratron.

ensure a pulse height resolution maximum, which is defined as the ratio between the mean value of pulse height and the FWHM of P.H.D. (see Fig.4-15)

As is seen in Fig.4-16, the P.H.D. of the multiplier depends slightly on the count ratio if it is less than 10 4 c/s. During the present experiments this condition was always satisfied.

The multiplier efficiency is not uniform over the entrance plane. For example, if an electron enters along the channel axis, it may penetrate quite a distance into the multiplier before releasing secondary electrons resulting in a lessened gain. Thus, it was always set off-axis from electron path to attain a higher pulse height. The dark current of the multiplier is less than 0.1 pulse per minute.

4-2-5 Measurement System

A schematic diagram of the electric circuit used in the analysing system is shown in Fig.4-17.

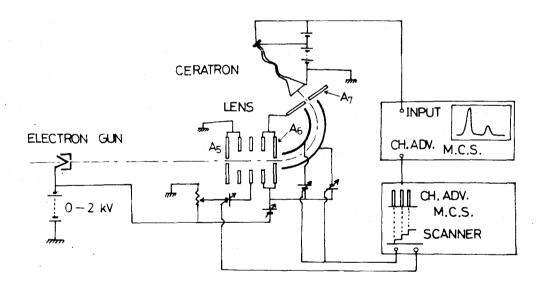


Fig.4-17. Electric circuit of the analyser system for measurements of loss spectra.

The loss spectra were obtained by scanning the potential of the sector and the lens, to obtain the best fit for the focusing condition. These potentials varied synchronously with the channel advance signal of the multi-channel-scaler (MCS) as is shown in Fig.4-17 (Ino-Tech TI-5200).

The whole electric circuit has a stability of about 0.01%. The primary electron beam current is stabilized by monitoring the current to the Faraday cup (see Fig.4-18). The monitored current using this circuit

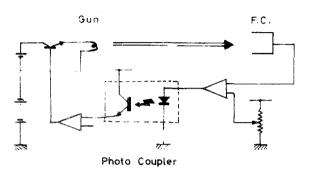


Fig.4-18 Schematic diagram of the beam current stabilized circuit.

is shown in Fig.4-19, together with the current obtained using a heater current stabilized circuit. As is shown in Fig.4-20, the MCS scanner is composed of a 1 MHz oscillator. counters, photo-couplers and 10-bit D-A converters (1024 steps). It serves the dwell time of 10^{-3} to 8 sec for each channel, and the scanning may be started or stopped at every 64 steps. The sector potential is swept linearly with regard to the MSC scanner output, however the lens potential should be swept non-linearly as can be seen in Fig.4-14. To simulate the curve, a non-linear amplifier was con-

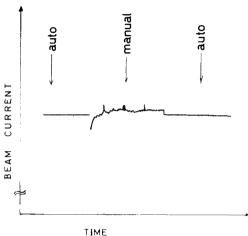


Fig.4-19 Stability of electron beam current (auto; beam-current-stabilized mode, manual; gun-heater-current stabilized mode).

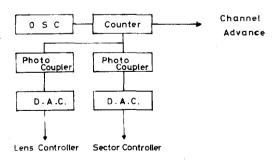


Fig.4-20. Schematic diagram of MCS scanner.

structed (see Fig.4-21). As the sweeping voltage of the sector potential is small compared to the sector potential itself, one would expect the circuit shown in Fig.4-21 to provide good results.

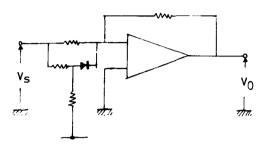
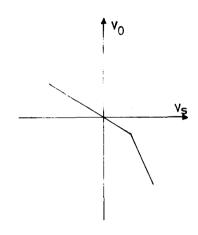


Fig.4-21. Schematic diagram of lens voltage controller.



4-3. Results and Discussion

4-3-1 Calibration

An example of the measured results of the loss spectra is shown in Fig.4-22 (E=300 eV, $\theta=60^{\circ}$). Many peaks corresponding to various excitation processes can be observed, i.e. the excitations for $(6s)(6p)^{3}P$ (4.9 eV), $(6s)(6p)^{1}P$ (6.7 eV), $(6s)(7s)^{1}S$ (7.9 eV), $(5d)^{9}(6s)^{2}(6p)^{1}P$ (9.8 eV) and $(5d)^{9}(6s)^{2}(6p)^{3}P$ (11.0 eV) states.

The background is estimated as the average number of electrons counted at each channel of the M.C.S. corresponding to loss energies between 2 and 4 eV, for the lowest excited state of mercury atom exists at 4.9 eV above the ground state.

The relative transmission efficiency α of the analysing system was determined by measuring the scattering intensity of elastic electrons by varying the incident energies from E to $E-\Delta E$. The standard transmission efficiency α_8 was determined for each incident energy at the scattering angle where the differential cross section of an elastic scattering remains almost constant for both the variation of the incident energy and scattering angle (e.g. 300 eV 100° , 400 eV 90° etc. see Figs.2-5 to 2-7. The relative transmission efficiency α was measured for each incident energy

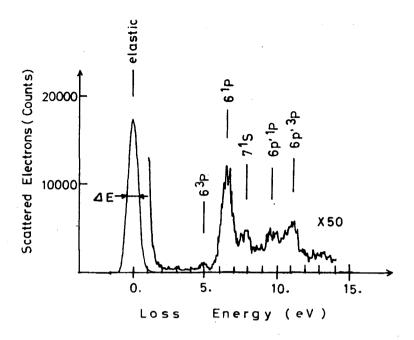


Fig.4-22. Example of the measured results of the loss spectra (E=300 eV and $\theta=60^{\circ}$)

and scattering angle, the profiles of which were compared to α_8 to assure a correct position for the analyser. Using the transmission efficiencies thus obtained, the ratio of the elastic and inelastic scattering cross section was determined correctly for each incident energy and scattering angle.

4-3-2 Loss Spectra

Fig.4-24 show the electron impact spectra for mercury corresponding to the incident electron energies from 300 eV to 1000 eV, scattering angles from 50° to 110° and loss energies from 0 eV to 15 eV. Elastic peaks are abbreviated for simplicity. Each spectrum shown in Fig.4-23 is obtained from the measured results (an example is shown in Fig.4-22) through the following procedures; 1) Transmission efficiency α was measured and compared with α_s .2) The ratio between the background and the peak counts of 6¹P excitation was established to be less than 10 % (usually the ratio was less than 5%), otherwise the data was omitted. 3) The background was subtracted from each channel intensity and then the intensity of each channel was corrected by the transmission efficiency α . 4) The loss spectra were normalized by the elastic scattering intensity. Finally, the data thus obtain-

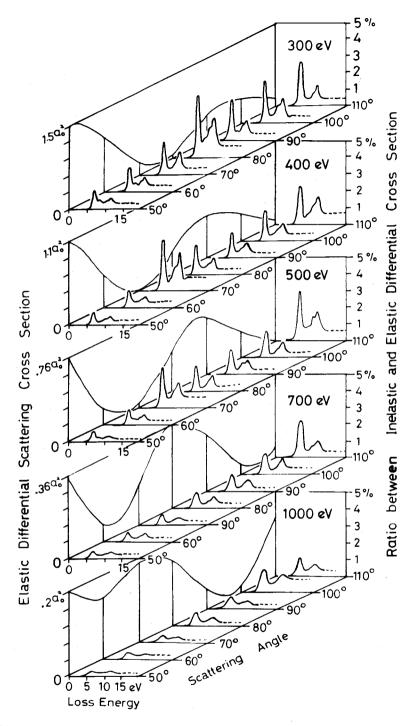


Fig.4-23. Energy loss spectra for mercury (The spectra are normalized by the elastic scattering intensity having the same impact energy and scattering angle).

ed which correspond to the same conditions as to impact energy and scattering angle were summed up and averaged to reduce the statistical deviation.

Concerning the ratio between 6¹P excitation and elastic scattering, it was estimated that error was less than 20 % including statistical error and the error induced by both the background and variation of transmission efficiencies. During measurement, the actual energy resolution was varied from 0.7 eV to 1.8 eV(FWHM) by controlling the electron energy entering the sector analyser in accordance with impact energy increases from 300 eV to 1000 eV. As has already been pointed out in Sec.2-4, the profiles of the theoretically calculated cross section of the elastic scattering agree well with experimental results, except that the extremum points of the calculated cross sections shift slightly to scattering angles smaller than the experimental (Walker 1969). Therefore, in Fig.4-23, the calculated results of the elastic scattering cross section, shown in Fig.2-5 are used instead of the experimental ones to avoid inaccuracies stemming from difficulties of measuring absolute transmission efficiency for various scattering angles. Concerning the absolute values of the cross section, the comparison between the experimental data and the calculated results shows that the latter is about 1.5 times larger than the former at scattering angles larger than 30° (see Sec.2-4). Thus the absolute values of the inelastic scattering cross section obtained from Fig.4-23 provides only the coarse evaluation which are probably a few times larger than the true values.

Two inelastic peaks corresponding to 6¹P((5d)¹⁰(6s)(6p)) and 6p³P ((5d)⁹(6s)²(6p)) excitations (6.7 eV and 11.0 eV energy losses respectively), appeared clearly in every spectrum, as is shown in Fig.4-23. These were also reported in a forward scattering experiment by Skerbele and Lassettre (1972). Fig.4-23 also shows that each elastic scattering intensity varies 2 or 3 orders of magnitude as a function of scattering angle, while the ratio between inelastic and elastic intensities remains in the same order of magnitude (a few percent) for dominant inelastic scatterings. Hence these oscillatory features, which are remarkable for elastic scattering in these energy regions, also appear in each dominant inelastic scattering, although they become smoother than that for elastic scattering.

Fig.4-24 shows the ratio of intensity between 6¹P excitation and elastic scattering. That for 300 eV electrons agrees well with the results reported by Gronemeier (1970) (see Fig.3-6).

At other inelastic channels, in the impact energies between 300 eV

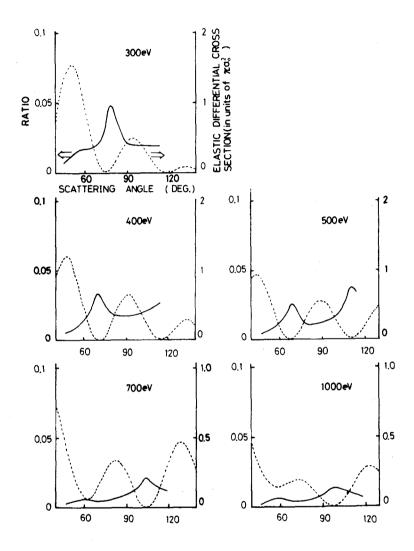


Fig.4-24. The intensity ratio of $6^{1}P$ excitation and elastic cross section (solid line) and differential cross section of elastic scattering (dashed line).

and 500 eV, $7^1S(7.9 \text{ eV})$ and $6p^{11}P(9.8 \text{ eV})$ excitations were observed at shoulders of 6^1P and $6p^{13}P$ peaks. The intensity of the strictly forbidden 7^1S excitation was larger than that of the 6^3P (4.9 eV) excitation (allowed due to spin-orbit coupling), however at forward scattering the latter was much larger than the former. The intensity ratio of 6^3P and 6^1P was equal to or less than $\sim 10^{-2}$ at the incident energy of 300 eV, and at higher impact energies 6^3P excitation was no longer observed because of a lower scattering intensity. The 7^1P excitation, the intensity of which was larger than that of 7^1S excitation at forward scattering, was rarely observed in the present experiment. For the ionization channels, particularly loss energy of more than about 13 eV, it seems that the variation of the intensity ratio in regard to scattering angles was not as clear as that of the excitation scattering to discrete levels.

CHAPTER 5, 6 P EXCITATION ---- COMPARISON OF THEORY AND EXPERIMENT

5-1 Introduction

In this chapter the theoretical and experimental results will be compared. It was found that the DWB approximation provides results in close agreement with experiments. Moreover, in regard to spin polarization, the DWB approximation predict a new phenomena at an electron impact energy greater than 300 eV.

As has already been discussed in Sec.4-3-2, the differential cross section of 6¹P excitation shows oscillatory features. This may be explained qualitatively by the following processes; the incident electron undergoes the inelastic process at a small angle followed by large angle elastic process, or vice versa, since the inelastic scattering cross section is very large at only forward scattering. Since this model breaks down the inelastic scattering into two elementary processes including the elastic process, the oscillatory features appearing in the inelastic scattering may be attributed to the elastic process. Futhermore, if one takes into account that the inelastics scattering at forward scattering is confined almost to optically allowed transitions, this model may also explain the dominance of the 6¹P excitation. Concrete theoretical treatment of this model is embodied by DWB approximation in Sec.3-2.

5-2 Comparison of Theory and Experiment

Figs.3-4, 3-6 and 3-7 show that the cross sections calculated using F_C provide values that agree well with the experimental data for each incident energy. However, concerning the profiles, the cross sections using F_M give results superior to those using F_C . These results suggest that the actual form factor has a profile similar to F_M and a value similar to F_C . This means that 1) the actual atomic field effectively acting on a 6s or 6p electron may be weak compared to the field of the Coulomb approximation, which may result in spreading of the atomic electrons over wide radial region and may originate from exchange effect and mutual shielding (see Fig.3-1), 2) the actual radial wave functions R_{00} and R_{10} (see equations (3-31) and (3-33)) may be much more isolated from each other than those used in F_M . This results in the reduction of the value of (R_{10},R_{00}) appearing in the

form factor having the form (see equations (3-34) and (3-35))

$$v_{01} = \frac{(8\pi)^{\frac{1}{2}}}{3} (R_{10}, R_{00}) (R_{11} | F_{1} | R_{00}) , \qquad (5-1)$$

with

$$(R_{11} | F_1 | R_{00}) = \frac{1}{r^2} \int_0^R R_{11} R_{00} r_1^3 dr_1 + r \int_R^\infty R_{11} R_{00} dr_1 .$$
 (5-2)

Concerning the spin polarization, as is seen in Figs.5-1 and 5-2 the calculations using \boldsymbol{F}_{M} provide results in closer agreement to the experimen-

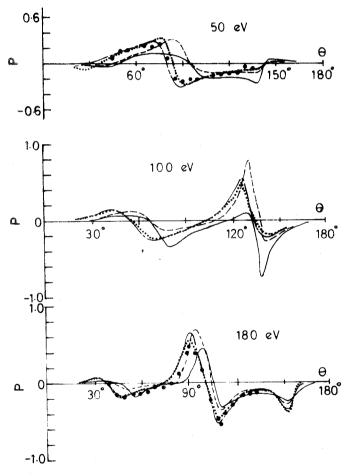


Fig.5-1. Spin polarization for mercury at incident electron energies of 50, 100 and 180 eV (——:DWB calculation for $6^1\mathrm{P}$ excitation using F_C (see Sec. 3-6), ---: DWB calculation for $6^1\mathrm{P}$ excitation using F_M , ----: elastic scattering by ground-state atomic potential, ...: elastic scattering by excited-state atomic potential and •:experimental results for $6^1\mathrm{P}$ excitation (Hanne et al. 1972).

tal results than that using $F_{\rm C}$, as would be expected from the profiles of the cross section (Note that spin polarization depends not on values of cross section but on profiles of cross section. See e.g. equations (2-42),(3-51) or (7-3)). However, it should be mentioned that the experimental results of spin polarization for 6¹P excitation are best expressed by the calculation

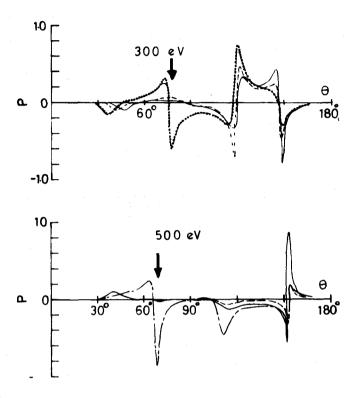


Fig.5-2. Same as Fig.5-1 except here the energies are 300 and 500 eV (Note that sharp peaks of the spin polarization appearing in the elastic scattering at the scattering angle of about 75° (300 eV) and 70° (500 eV), disappear in $6^{1}P$ excitation scattering.).

for elastic scattering in the present calculation. This is not the case for the calculation by Madison and Shelton (1973). They obtained results in close agreement to experimental results for incident energies between 50 and 180 eV(see Fig.5-3). It is thought that this is primarily a result of the difference in form factor used (as is seen from Fig.3-2, the profiles of F_M are simplified for convenience in the present calculation).

Although the spin polarization for incident energy of 100 eV had not been measured until presently, the profiles given in Fig. 5-1 are thought to be reasonable and conceivable considering that the experimental results of spin polarization for 6^1P excitation were most like that of elastic scattering. However, for incident energy of 300 eV and 500 eV, it is notable that the sharp peaks of the spin polarization appearing in the elastic cases at the scattering angle of about 75° and 70°, respectively, disappear in calculations of 6^1P excitations using both F_C and F_M (see Fig.5-2). For 6^1P excitation scattering and incident electron energy over 180 eV, because no experimental data on spin polarization have been reported until currently

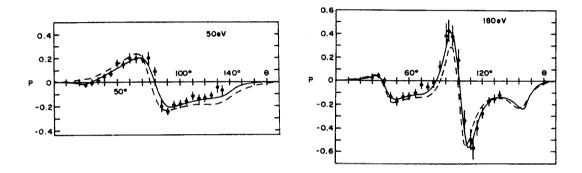


Fig. 5-3. Spin polarization for $6^{1}P$ excitation scattering at incident energies of 50 and 180 eV calculated by Madison and Shelton (1973) using DWB approximation for Mayer's potential (solid line, 1957), Coulthard's potential (dashed line, 1967) and experimental data by Eitel and Kessler (1970).

it is uncertain as to whether the drastic departure of spin polarization between the elastic and $6^{1}P$ excitation scattering means new phenomena or a breakdown of the DWB approximation. However, generally speaking, the DWB approximation provides better results at higher incident energies where a large number of partial waves contribute to forward scattering, most of which have nearly zero polarization, thus the reduction of the spin polarization is thought to be reasonable.

Further measurements of spin polarization in these energy regions would be highly desirable.

PART II. ESP-DETECTOR USING MERCURY VAPOUR

CHAPTER 6. INTRODUCTION

Currently, ESP experiments are being carried out by several groups in various regions of physics. These ESP experiments except for that listed in Tables 1-1 and 1-2 are summarized in Table 6-1 classifying into 5 groups, i.e. 1) the group entitled "Field Emission" treating ESP experiments or theories of field emitted electron beam usually from ferromagnetic materials, 2) the group "Photo Emission (solid)" treating those of photo electrons from ferromagnetic materials or of photo electrons from solid excited by circularly polarized light, 3) the group "LEED" treating those of diffracted electron beam in low energy electron diffraction, 4) the group "Photo Emission (vapour)" treating those of photo electrons from polarized atomic beam or photo electrons excited by circularly polarized light from unpolarized atomic beam and 5) the group "Others". In these experiments, spin polarization is usually detected using scattering of polarized electron beam with heavy atoms (Au-foil or Hg-vapour), the efficiency of which is equal to or less than 10^{-5} (The principle of the detector is given in Chapter 7.). It should be noted that the value is quite small compared with that of light.

A simple question arises as to whether or not a usual magnetometer can detect a direction of electron spin. Incapability of detecting electron spin with macroscopic magnetometer is qualitatively described in Appendix 2 according to Mott's consideration together with incapability of polarizing electrons with macroscopic magnetic field.

Since the first measurement of spin polarization using double scattering by gold thin film at 340 keV (Shull et al. 1943), the detection of electron spin in high energy electrons is usually performed using scattering with gold thin film, which is called Mott detector (see Fig.6-1). On the other hand, the first ESP measurement for low energy electrons was performed using

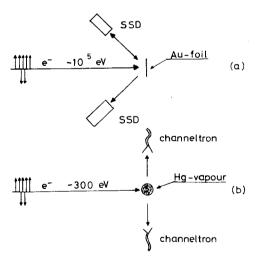


Fig.6-1. Schematic diagram of ESP detector using (a) Au-foil (Mott detector) and (b) Hg-vapour.

mercury vapour (Deichsel 1961). The ESP detector of this type is widely used for various ESP experiments such as e -rare gas elastic scattering and e -Ne resonance scattering. Mott detector was first used by Jost and Kessler (1965, 1966) for low energy experiments. Schematic diagrams of these two types of ESP detector are shown in Fig.6-1. Because of a high efficiency and ease of treatment in a high vacuum, the Mott detector has been widely used not only in atomic physics but also in surface physics, where ultra-high-vacuum $(10^{-10} \sim 10^{-11})$ Torr) is necessary. However, it should be noted that a Mott detector which uses high energy electrons (~100keV) is not suitable for the experiments of low and mediate energy regions in which major ESP experiments concentrate. Hence the present study attempts to develop an ESP detector suitable for low and mediate energy regions utilizing the electron-mercury scattering, which can also be used as a source of polarized electrons for e.g. surface physics study (see Sec. 8-3).

Optimum conditions of ESP detector using mercury vapour are discussed and determined systematically in Chapter 7 using the results in Chapter 2, 3, 4 and 5. In Chapter 8, ESP detector and apparatus for double scattering experiments constructed according to the line shown in Chapter 7 is described. Also described in this chapter is high beam current Pierce type electron gun using single LaB₆ crystal as a cathode for double scattering experiments.

Another possibilities of detecting electron spin are proposed by several authors (Tolhoek 1956, Feder 1975):

- 1) Measurement of the spin angular momentum carried by electrons with longitudinal polarization in a mechanical way. This may be realized by measuring a torque of a suspended disk where polarized electrons are falling (A kind of Einstein-de-Haas effect).
- 2) Measurement of the polarization of emitted light from an atom which is excited by polarized electrons.
- 3) Measurement of intensity asymmetry of diffracted beams in LEED (low energy electron diffraction) experiments. The principle is like that of a Mott detector and a detector using mercury vapour as scatterer. The methods of 2) and 3) may be more practical than that of 1).

Table 6-1

Field Emission

Exp.	Gd (polycrystal)	Hofmann et al.	1967
Theor.	Gd	Müller et al.	1967
Exp.	Ni(single)	Gleich et al.	1971
Exp.	EuS-coated W	Müller et al.	1972
Exp.	W(single)	Regenfus and Sütsch	1974
Exp.	Ni(single)	Müller	1975
Theor.	Effect due to external field	Eckstein and Müller	1975
Exp.	Ni(single)	Eib and Alvarado	1976
Exp.	EuS coated W	Kiskev et al.	1976
Exp.	Fe, Ni, Co, rare-earth metal	Chrobok et al.	1977
Exp.	Ni(100)	Landolt and Campagna	1977
Theor.	W(001) with adatom	Feder	1977

Photo Emission (Solid)

Exp.	Ni(single,poly)	Bänninger et al.	1970
Exp.	Alkali metal	Heinzmann et al.	1971
Theor.	Ni(single)	Smith and Traum	1971
Theor.	Ni,Co	Anderson	1971
Theor.	Ni,Co	Wohlfarth	1971
Exp.	Alkali metal (circularly po.light)	Heinzmann et al.	1972
Exp.	Со	Busch et al.	1972
Theor.	Ferromagnetic metal	Murao	1972
Exp.	Ni,Co,Fe	Adler et al.	1973a
Exp.	Ferro magnetic metal	Adler et al.	1973b
Theor.	EuO(100)	Eastmann	1973
Summary		Campagna et al.	1973
Theor.	Ferromagnetic metal	Murao	1974
Exp.	EuO(La doped)	Meier et al.	1975
Exp.	EuO	Sattler and Siegmann	1975
Exp.	GaAs	Pierce et al.	1975
Exp.	Ferrite (Fe ₃ O ₄ , Li _{0.5} Fe _{2.5} O ₄)	Alvarado et al.	1975b
Exp.	La-doped EuO	Meier et al.	1975

TI	0. h	Variable and Marin	1075
Theor. Theor.	Ce by circularly po. light Photo Emission	Koyama and Merz	1975 1975
meor.	(circularly po light)	Koyama	19/5
Theor.	Ni(single)	Wohlfarth	1975
LEED			
Theor.		Jennings	1970
Theor.	E(001)	Jennings	1971
Theor.		Jennings	1972
Theor.	Fe(001)	Feder	1973
Theor.	W(110), W(001)	Feder	1974
Exp.	W(001)	O'Neill et al.	1975
Theor.	W(001)	Jennings	1975
Theor.	W(001)	Feder	1976
Theor.	W(001)	Feder et al.	1976
Theor.	Ni(111)	Feder	1977
Photo Emiss:	ion (vapour)		
Theor.		Fano	1969
Exp.	Се	Heinzmann et al.	1970
Exp.	Po. Alkali Atom	W. Hughes et al.	1972
Exp.	Ce Po.light	Drachenfels et al.	1974
Exp.	Th	Heinzmann et al.	1975
Exp.	Се	Granneman et al.	1976
Theor.		Feder	1977
04 h n			
<u>Others</u>			
Theor.	exchange scattering	Byrne and Farago	1965
Theor.	Ne(resonance scattering)	Franzen and Gupta	1965
Exp.	K, exchange scattering	Farago and Siegmann	1966
Theor.	electron-magnon scattering	DeWames and Vredevoe	1967
Exp.	K, exchange scattering	Campbell et al.	1971
Theor.	excitation process of po. atom	K1einpoppen	1971

Exp.	Ne(resonance scattering)	Heindorff et al.	1973
Theor.	Ne(resonance scattering)	Suzuki and Tanaka	1973
Theor.	excitation process of po. atom	Blum and Kleinpoppen	1974
Theor.	Ne(resonance scattering)	Suzuki et al.	1975
Theor.	surface of ferromag- netic metal	Penn	1975
	Hg(resonance scattering)	Düweke et al.	1976
Exp.	Hg(exchange scattering)	Hanne and Kessler	1976
Theor.	Hg(exchange scattering)	Hanne	1976

CHAPTER 7. OPTIMUM CONDITIONS OF THE ESP DETECTOR

7-1. Introduction

The ESP detector constructed by Deichsel (1961) is shown in Fig.7-1. It consists of a mercury reservoir, two sector type energy analysers and two electron multipliers. This was used to investigate the spin polarization of the electrons elastically scattered by the mercury atom. The energy resolution was set at less than 4.9 eV, the lowest excitation energy of mercury corresponding to 6³P excitation. The scattering angle and angular resolution were set at 90° and 6° respectively. However, the

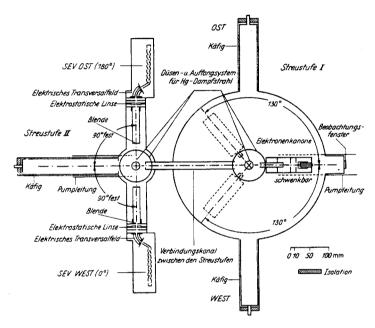


Fig.7-1. Electron spin polarization (ESP) detector (left side chamber) and polarizer (right side chamber) used by Deichsel (1961).

theoretical basis for these values was not shown with the exception of the energy resolution for the ESP detector.

Gronemeier (1970) measured the 6¹P excitation scattering, which is usually the most dominant inelastic process in electron-mercury scattering for electron impact energies between 20 and 300 eV and Yamazaki et al. (1977c) measured the loss spectra of mercury atom for electron impact energies between 300 and 1000 eV (see Secs. 3-6 and 4-3-2). The results

show that these inelastic electrons have little influence on the determination of the spin polarization when used in hundreds eV energy regions.

In this chapter, optimum conditions of the ESP detector using electron-mercury scattering are systematically studied and a high efficient ESP detector of simple construction is proposed.

7-2. Determination of E, θ and $\Delta\theta$

From equation (2-45), we can see that transverse spin polarization of electrons (i.e. spin polarization perpendicular to the scattering plane which is described by primary beam and direction of observation) can be analyzed by the scattering asymmetry. Substituting $\theta=0$ and π , and $\mathbf{P}=(0,P,O)$ in equation (2-45), we obtain

$$\sigma_L = \sigma_0 (1+SP) \tag{7-1}$$

$$\sigma_R = \sigma_0 (1 - SP), \qquad (7-2)$$

respectively (see Fig.7-2-a). Equations (7-1) and (7-2) lead to

$$N_R/N_L = (1-PS) / (1+PS)$$
, (7-3)

where $^{N}_{R\ (L)}=^{N}_{i\,n}\cdot^{N}_{H\,g}\,\,^{\sigma}_{R\ (L)}\,\mathrm{d}\,\mathcal{Q}$, $^{N}_{i\,n}$ is the number of incident electrons per unit area, $^{N}_{H\,g}$ the number of mercury atom in collision volume, and $\mathrm{d}\,\mathcal{Q}$ the acceptance solid angle of electron detector. Thus, we can determine the polarization of incident electrons by measuring the ratio of left-right asymmetry $^{N}_{R}/^{N}_{L}$.

Fig.7-2-b shows the differential cross section for a totally polarized incident electron beam of 300 eV. It seems that the grater the absolute value of the Sherman function, the greater the detectability of spin polarization becomes. However, from a practical point of view it should be noted that in these energy and angular regions, the differential cross section becomes extremely small, so the efficiency of the detector is reduced. Moreover, the Sherman function S in these regions is in general rapidly varying for both the scattering angle and the impact energy (see Figs.7-3 to 7-6). This makes it difficult to estimate the Sherman function both theoretically and experimentally. The theoretical value of Sherman function differs considerably from the experimental one in these regions.

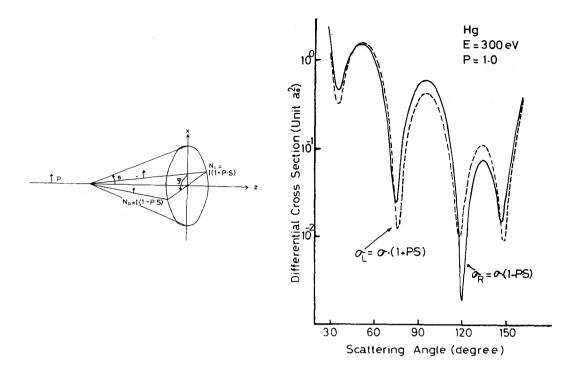


Fig.7-2. (a) Schematic diagram of left-right scattering asymmetry of a beam polarized perpendicular to scattering plane.

(b) Cross section for a totally polarized electron beam scattered by mercury atom at $E=300~{\rm eV}$.

Furthermore, experimentally determined Sherman function in these regions depends strongly on the accuracy of the scattering angle and the angular resolution of the system.

To determine the best condition of the ESP detector systematically from these various parameters, first, the statistical error of the measured polarization is estimated from equation (7-3) as

$$\Delta P_{rel} = (2N)^{\frac{1}{2}} \cdot \Delta P / P \sim \left\{ (\sigma P^{2} S^{2})^{-1} - \sigma^{-1} \right\}^{\frac{1}{2}}$$
 (7-4)

Calculating the right hand side of equation (7-4) and taking into account both the differential cross section and ESP we can estimate the suitable regions for the energy, scattering angle and angular resolution necessary for the detector. Examples of the results are shown in Figs.7-3 to 7-6, together with the cross section and spin polarization. The results are summarized in Fig.7-7 for cases of the two different angular resolutions.

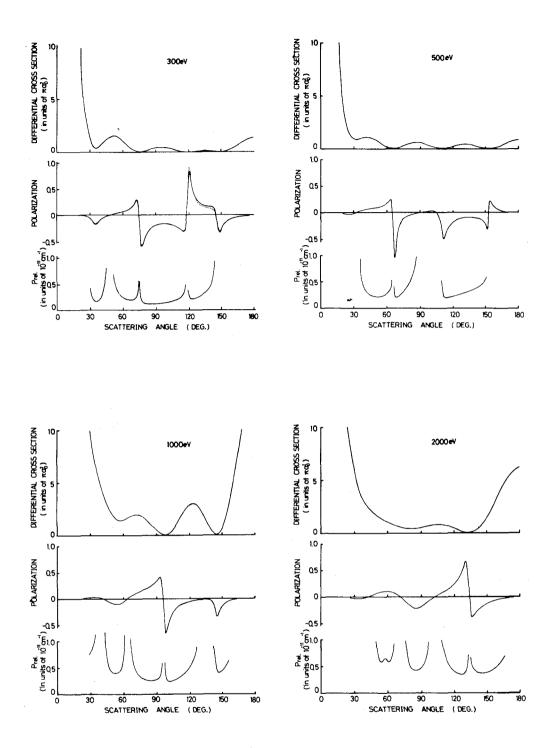
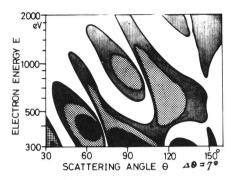


Fig.7-3 to 7-6. Relation between cross section, spin polarization and ΔP_{rel} for initial spin polarization of P=0.1.



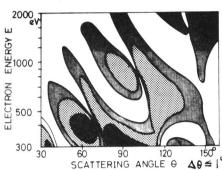




Fig.7-7. Contours of constant Δ^P_{rel} for initial polarization of P=0.1 as function of scattering angle and electron energy for angular resolution of $\Delta\theta \leq 1^\circ$ and $\Delta\theta = 7^\circ$.

These results show that the optimum conditions do not concentrate around extremum points of Sherman function, but exist around 1) 300 eV, 90°, 2) 400 eV, 70°, 3) 600 eV, 120° and 4) 1000 eV, 90°. In these energy and angular regions, particularly at 300 eV, both the cross section and Sherman function are slowly changing functions with respect to scattering angle, so it is concluded that high angular resolution and high accuracy of angular setting are not necessary for the ESP detector to achieve high ESP resolution.

Other important points are 1) the Sherman function necessary for determination of polarization has nearly the same value for several theoretical calculations and experiments in these energy and angular regions, so the accurate Sherman function can be easily obtained both theoretically and experimentally, 2) S/N ratio may increase because of high scattering intensity.

It was concluded that an electron energy of 300 eV and a scattering angle of about 95° is the best condition for the optimum operation of the ESP detector in the hundreds eV energy regions.

As can be seen in equation (7-3), the left-right asymmetry remains constant over the region of scattering angle where Sherman function S remains constant. From equation (7-3), for the angular resolution of $\Delta\theta$, the

observed spin polarization $P_{\ o\ b\ s}$ is expressed as

$$P_{0bs}/P = 1 + \frac{(\Delta\theta)^2}{24} \left(\frac{S''}{S} + \frac{2\sigma'S'}{\sigma S} \right)$$
 (7-5)

where

$$S' = \partial S/\partial \theta$$
, $\sigma' = \partial \sigma/\partial \theta$ and $S'' = \partial^2 S/\partial \theta^2$

From equation (7-5), the error caused by the variation of the Sherman function in the angular range of 90° to 105° for incident energy of 300 eV is estimated to be less than about 1%.

The number of doubly scattered electrons N_2 may be roughly estimated as

$$N_{2}(\alpha) = N_{i\pi} N_{Hq}^{2} \int \sigma (\theta) \sigma (\alpha - \theta) d\theta$$
 (7-6)

where α and θ are the final and intermediate scattering angle respectively. Equation (7-6) shows that ratio of double scattering to single scattering is proportional to mercury vapour density, so in general sufficiently low density of mercury vapour is required for precise measurement of spin polarization (W. Eitel et al. 1968). Fig. 7-8 shows $\sigma(\theta) \sigma(\alpha - \theta)$ as a function of θ for α = 95° and 75°. It shows that for $\alpha = 95^{\circ}$, the probability of the double scattering is dominant only near $\theta \sim 0^{\circ}$ or 95°. A polarization P of incident electron is transformed to P_s after scattering according to the equation (2-48). Equation (2-48) shows that at forward scattering, initial polarization p is conserved during scattering, because $S \sim U \sim 0$ and $T \sim 1$ at forward scattering as is seen from Figs.7-9 and 2-9.

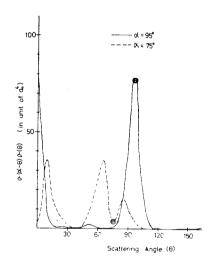


Fig.7-8. Contribution of doubly scattered electrons for incident electron energy of E = 300 eV and final scattering angle of α = 95° (solid line) and α = 75° (dashed line) as a function of scattering angle of first scattering.

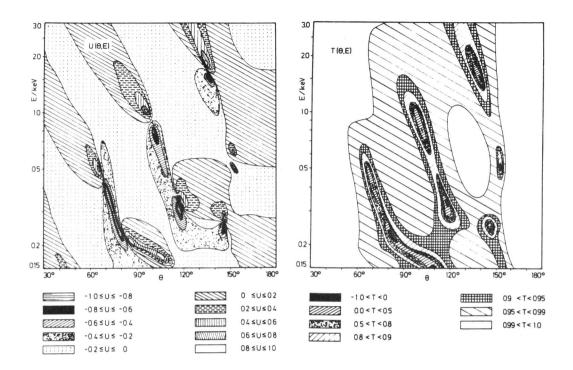


Fig.7-9. Contours of constant U(a) and T(b) for mercury as function of scattering angle and electron energy. U describes the rotation of the polarization out of its initial plane. T describes the reduction of the polarization component due to scattering (Kessler 1976).

(Note that $S^2+U^2+T^2=1$). This affects little on the determination of spin polarization. It is not the case at α =75° where an effective Sherman function originating from double scattering is modified by the Sherman function at θ =65° and 85°. It is concluded that the region of large cross section is desirable to make the affect of double scattering relatively less.

7-3. Determination of ΔE

In this section, the energy resolution necessary for an ESP detector is investigated. From equation (7-3), the observed spin polarization $P_{\mbox{\it obs}}$ is expressed as

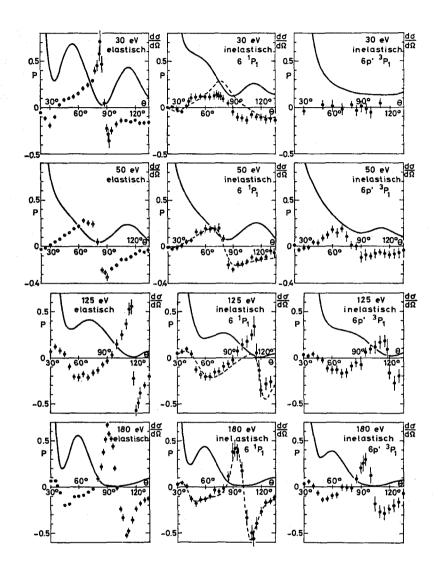


Fig.7-10. Experimental results of cross section and spin polarization for $6^{1}P$ and $6p'^{3}P$ excitation scattering.

$$P_{obs} \cdot S = (N_R - N_L + n_R - n_L) / (N + n)$$

$$= P \cdot S \cdot \{ 1 - S_{inel} / S \} n / N \} , \qquad (7-7)$$

where n_{R} (1) is the number of inelastically scattered electrons to the right (left) side, s_{inel} the Sherman function of inelastically scattered electrons

$$N = N_R + N_L$$

$$n = n_R + n_L$$

$$(7-8-a)$$

$$n = n_R + n_L \tag{7-8-b}$$

From equation (7-7), if $P_{inel}=0$, i.e. inelastically scattered electrons are not polarized, the error induced by these electrons is estimated to be n/N, the ratio of inelastic electrons to elastic ones.

As was experimentally investigated in Chapter 4, the ratio n/N for a hundreds eV electron remains within a few percent (see Fig. 4-24). It increases when elastic cross section decrease. This implies that the error induced by inelastic electrons can be reduced if we adopt a condition where the elastic cross section is large.

Moreover, as was experimentally investigated by Hanne et al. (1972), inelastically scattered electrons corresponding to 6 1 P and 6p 3 P excitations are polarized to some extent and show the similar profiles of spin polarization to elastically scattered electrons (see Fig. 7-10). These facts suggest that the error originating from inelastic scattering can be less than n / N(see equation 7-7).

It is concluded that the energy resolution of \sim 13 eV (6.7 eV \times 2) or more may not cause significant error (less than 2% see Fig.4-24) in the ESP detector, particularly at region near the maximum points of cross section.

7-4. Conclusion

The optimum condition proposed in this chapter is of practical importance for reducing unnecessary labor in both the construction of the ESP detector and precise measurement of spin polarization. From the discussions developed in Secs. 7-2 and 7-3, it is concluded that

$$E \sim 300 \text{ eV}$$

$$\Delta E \sim 13 \text{ eV}$$

$$\theta \sim 95^{\circ}$$

$$\Delta \theta \sim 15^{\circ}$$
(7-9)

may give the best condition for the ESP detector. Advantages of the condition are summarized as follows;

- 1) In this region, the Sherman function can be determined accurately.
- 2) The high accuracy of angular setting is not necessary, which results in simple construction of the ESP detector.
- 3) A large acceptance angle is allowable which results in high efficiency of the ESP detector.
- 4) The scattering cross section is large which results in better S/N ratio.
- 5) The ratio of inelastic to elastic scattering cross section is small which results in high efficiency and simple construction of the ESP detector.
- 6) The affect of multiple scattering is small which allows high density mercury vapour so results in high efficiency of the ESP detector. For this condition and the mercury density of $10^{15}/\mathrm{cm}^3$ (corresponding to the vapour pressure of $\sim 3 \times 10^{-2}$ Torr), the efficiency α_{eff} of the ESP analyser amount to approx. 10^{-6} where

$${}^{\alpha}eff = S_{eff}^{2} . I/I_{0} , \qquad (7-10)$$

 S_{eff} is an effective Sherman function and I/I_0 the intensity ratio of scattered to incident electrons. Equation (7-10) is derived from equation (7-4) taking into account the usual experimental condition of $S \cdot P \ll 1$. A common Mott detector provides an efficiency of approx. 10^{-5} (see e.g. Kessler 1976) which is about one order larger than the value now obtained. However, the ESP detector using mercury has various advantages, primarily 1) electrons need not be accerelated to energies as high as 100 keV, which results in simple construction and easy operation of ESP detector, 2) this detector can also be used as a polarized electron source (see Chapter 8).

CHAPTER 8. DOUBLE SCATTERING EXPERIMENT

8-1 Introduction

The optimum conditions of the ESP detector have been systematically determined in Chapter 7. In this chapter, the apparatus for double scattering experiments will be described (see Fig.8-1).

The first and second scattering is for production and detection of polarization, respectively. The arrangement of the ESP detector, the

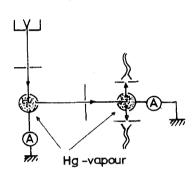


Fig. 8-1. Schematic diagram of the double scattering experiment for mercury vapour.

second scattering, is determined according to the line shown in Chapter 7. As a standard polarized electron beam source, electron-mercury elastic scattering is used, because the spin polarization in the electron mercury elastic scattering has been investigated in detail by several authors (see Tables 1-1 and 1-2). Since the intensity of an electron beam after double scattering is extremely weak, a Pierce-type electron gun of high intensity was constructed using a single crystal LaB6 cathode.

8-2. Apparatus -- Design and Performance

8-2-1. Construction

The apparatus consists of an electron beam source, a first vacuum chamber as an electron spin polarizer and a second vacuum chamber as an ESP detector. An outer view of the apparatus shown in Fig.8-2 removing the top cover of the vacuum chamber. Fig. 8-3 shows cross sectional drawings of the system. The scattering angle at the first chamber is set at $\sim 100^{\circ}$ where highly polarized electrons are provided at E ~ 850 eV (see Fig.2-5). Fig.8-4 shows the block diagram of the vacuum system.

The first vacuum chamber is a 20 cm high cylinder of 12.4 cm inner diameter pumped by a 120 ℓ /s oil diffusion pump evacuating the system to residual gas pressure of 10^{-5} Torr, but the pressure increases to 5×10^{-5} Torr during operation due to mercury vapour. The gun part is differential-

ly pumped by a 600 ℓ s oil diffusion pump which provides a residual gas pressure of ~5 \times 10⁻⁶ Torr. In the center of the second chamber, a collision chamber is set which is also used as the mercury reservoir and the Faraday cup from monitoring the primary electron beam current. The density of the mercury vapour is controlled by the inductionless heater wound around the

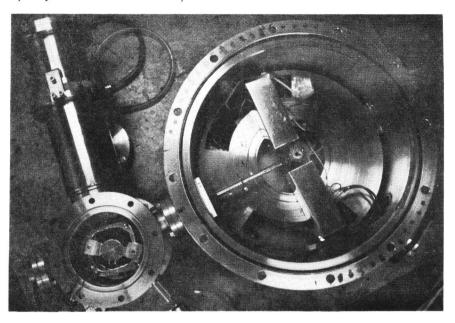


Fig. 8-2. Top view of the apparatus for the double scattering removing the top cover of both 1st and 2nd chambers.

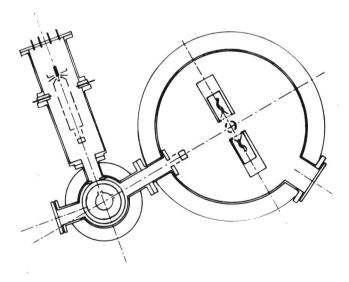
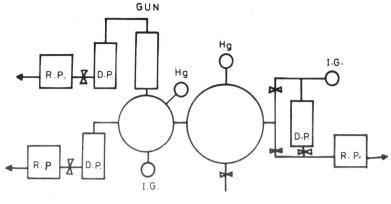


Fig.8-3. Schematic diagram of the apparatus constructed for the double scattering.



1st CHAMBER 2nd CHAMBER

Fig. 8-4. Schematic diagram of the vacuum system.

collision chamber which is pumped through two apertures (inner diameter of 4mm) which allow the incident and scattered electrons to pass.

The construction of the second chamber is like that used in Chapter 4 except the energy analyser and the collision chamber which is also used as a Faraday cup. Two energy analysers are set in the left and right sides of the collision chamber (in the scattering plane) at symmetric position with respect to incident beam axis at a scattering angle of approx.95°.

The cross sectional drawings of the energy analyser are shown in Fig. 8-5. The energy analysis is performed by a twofold retarding mesh (gold plated tungsten of 100 mesh) instead of a sector type analyser, the construction of which is confirmed by the investigation in Chapter 7. (It was shown that even energy resolution of approx.13 eV was still practically feasible). The outer view of the analyser is shown in Fig.8-6.

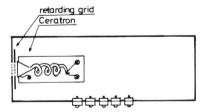


Fig.8-5. Schematic diagram of the energy analyser to the ESP detector.

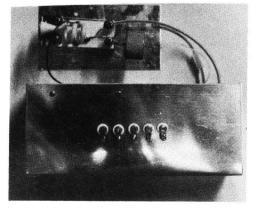
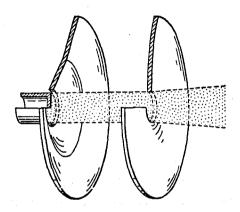


Fig. 8-6. View of the electron multiplier and the case of energy analyser.

The electron multiplier used is a kind of channeltron (Murata Co., Ceratron Type EMS-6081B) with an acceptance cone and a holding stage.

8-2-2. Pierce-Type Electron Gun Using LaB $_6$ Single Crystal as a Cathode

As the intensity of an electron beam after double scattering is extremely weak, an electron gun of high beam intensity is necessary for double scattering experiment. For this purpose, a Pierce-Type electron gun of high beam intensity was constructed (Pierce 1954). The Pierce-Type electron gun is designed for use in space-charge limited regions and provides a parallel electron beam. The main part of this gun consists of a cathode with flat



Oscillator
1kHz

Insulating
Strip
Cathode
Cathode
Cathode
Electrode
Electrode

Electrolyte
Tank

Electrolyte
Tank

Field)

Fig.8-7. Schematic diagram of cathode and anode electrodes of Pierce type electron gun (Pierce 1954).

Fig.8-8. Schematic diagram of the electrolytic tank.

surface, a cathode electrode and an anode electrode as is schematically shown in Fig.8-7. The actual shapes of these electrode are determined using an electolytic tank (see Fig.8-8). It was concluded that the shape of the cathode electrode should have the same shape as the usual Pierce gun with an angle of 67.5° between the electrode and the beam axis.

The cathode are heated by electron-bombardment. To prevent the bombarding electrons from straying into the electron beam from the cathode, a shielding electrode is set between the cathode electrode and the heater for electron bombardment. Parts of both the cathode and shielding electrodes near the cathode consist of Ta to obtain stable performance during operation at high temperatures. Fig.8-9 is a cross sectional drawing of the Pierce

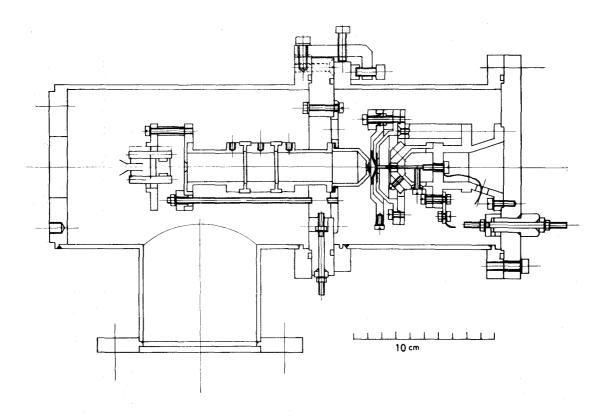


Fig.8-9. Cross section of the Pierce-type electron gun with einzel lens and deflector, and its vacuum chamber.

gun constructed. An asymmetric three cylindrical lens with deflector is set in front of the anode electrode.

 LaB_6 single crystal is used as a cathode because of its high emission current and stable performance over a long period of time (long service life) which originates from the low values of both the work function and the vapour pressure (J.M. Lafferty 1951). Moreover, the LaB_6 single crystal has flat surface plane of stochiometric uniformity (T. Tanaka et al. 1975) which enables one to obtain a beam of higher current intensity with good parallelism and spatial uniformity.

The cathode consists of a LaB₆ single crystal rod with a diameter of 2mm and length of 7mm held in a Ta cylinder. The Ta cylinder is connected to a 2mm diameter W-rod with three spot welded Ta wires in order to limit power consumption. Furthermore, this prevents the gun assembly from deteriorating the vacuum by heating the area surrounding the cathode. The distance between the anode and the cathode was 5.5 mm and the perveance was $2.42 \times 10^{-7} \text{ A/V}^{3/2}$. Two Ta ribbons $(0.025 \times 0.75 \text{ mm})$ were held around the LaB₆ cathode. The two Ta ribbons had heating currents of opposite direction in order to reduce the current-induced magnetic field around the emitter.

Fig.8-10 is an outer view of the cathode and bombarding system with both the cathode and the shielding electrode removed.

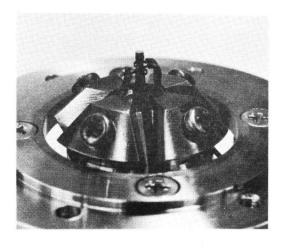


Fig.8-10. View of the single crystal LaB_6 cathode and its holding system removing anode, cathode and shielding electrodes.

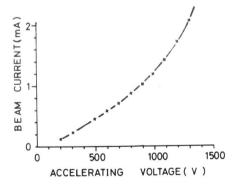


Fig.8-11. Relationship between beam current and accelerating voltage (x: beam current).

To evaluate the performance, LaB₆ was heated up to ~1600°C with accelerating voltage range of 200-1300 eV. With these operating conditions, the gun was being operated in the space charge limited region, with approx. 12W of power consumed. During operation, evaporated LaB₆ is continually deposited on the Ta-ribbons which reduces the work function of the ribbons, which in turn reduces the heating power to approx. 6 W. The beam diameter was observed with a fluorescent screen situated 10 cm along the beam path from the anode. The spot size of the beam was found to be 3-4 mm in diameter for the above accelerating voltages. The beam current was measured by a Faraday cup having an inner diameter of 4 mm at a vacuum pressure of 3×10^{-6} Torr. Fig. 8-11 shows the relationship between the beam current and the accelerating voltage. The rapid variation of the beam current in current stability measurements was rarely observed and the beam current drift was less than 0.1 %. As in seen in Fig.8-11 the actual perveance was found to be 3.8×10^{-8} A/V^{3/2}.

8-2-3. System of Measurement

A schematic diagram of the electric circuit used for the double scattering experiment is seen in Fig.8-12. The memory section of M.C.A. was devided into two parts to treat the signals of the two origins. A pulse is at first amplified and then arrives at A.D.C. input in the M.C.A. through the mixer. At the same time, the memory region is selected based

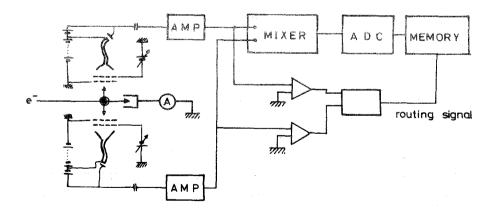


Fig. 8-12. Schematic diagram of the electric circuit for double scattering experiment

on which multipliers the pulse originates. This is a successful method when counting ratio of both the multipliers are low because switching time or dead time of M.C.A. has little effect on measurements. Moreover, we can correct the external and internal background by direct observation of P.H.D.

The system used was Ortec "Spectroscopy Amplifier 472A (\times 2), Ortec "Dual Sum and Invert Amplifier, 433A", and Ino-Tech IT-5200 Multi-Channel-Analyser.

8-3. Proposal for an Application of Electron-Mercury Scattering to a Polarized Beam Source

As is shown in Sec.2-3 and Appendix 3, polarizing and analysing powers are expressed by the same function S (Sherman function) in the case of elastic scattering. In a certain type of scattering experiment, an intensity measurement using an initially polarized electron beam is superior to a polarization measurement using initially unpolarized electron beam.* This is precisely the case in studies of surface physics, where primary electron beam should be sufficiently weak so as not to damage a sample surface.

Kessler (1976) summarized various polarized sources and estimated its beam qualities, which is shown in Table 8-1. $'P^2I'$, appearing at the top of the 5th column in Table 8-1, may serve as a kind of parameter for an estimation of beam quality (see Sec.7-4, where the similar quantity α_{eff} is used for the estimation of efficiency of the ESP detector.). The 6-th column Beam quality q is determined by

$$q = \frac{P^{2}I}{r_{0}^{2}\alpha_{0}^{2}E_{0}} , \qquad (8-1)$$

* Recently, an experiment of similar conception is reported to be in progress (Unert1 et al. 1977) where photo electrons from GaAs surface are used as a polarized electron source for LEED study.

where r_0 is the radius of a beam-cross-section minimum, α_0 the corresponding semi-aperture of the beam and E_0 the energy of electrons leaving the source. We can see that q takes into account the polarization, intensity and collimation of the beam. From Table 8-1, the beam source using "scatter-

Method	P	I		P ² I	Beam
		d.c. (Ampere)	pulsed($\approx 1 \mu s$) (el./pulse)	(Ampere)	quality <i>q</i> Eq. (7.19)
Scattering from unpolarized targets	0.2	3.5-10-8		10-9	Medium
Exchange scattering from polarized atoms	0.5 0.2		10 ⁴ 10 ⁷	2·10 ⁻¹⁴ 7·10 ⁻¹²	Low to
Photoionization of polarized atoms	0.76		8·10 ⁸	10-8	Medium
Fano effect	0.65 0.9	1.5·10-9	3·109	6·10 ⁻¹⁰ 2·10 ⁻¹¹	Medium
Collisional ionization			3 10	2.10	
in optically pumped He discharge	0.3	5-10-7		5.10-8	Medium
Field emission from ferromagnets	0.89	10-6		8-10-7	to high High

Table 8-1. Comparison of various sources of polarized electrons (Kessler 1976).

ing from unpolarized targets" is ranked "medium". Thus, the ESP detector using mercury vapour may work well as a polarized beam source, if an electron gun is mounted together with the electron multiplier.

It is worth noting that this system provides precise information on the scattering process by comparing the polarizing and analysing power, i.e., these two values are not equal to each other e.g. in exchange scattering as is shown in Appendix 4.

SUMMARY

The present work consists of two parts, Part I which consists of Chapter 1-5 and Part II, Chapter 6-8. The main subject of Part I is "Electron-Mercury Scattering" and that of Part II, "ESP detector using Mercury Vapour". The results obtained in the present study are summarized chapter by chapter as follows.

Part I Electron-Mercury Scattering

Chapter 1; Introduction

- 1) The characteristics of electron-heavy atom scattering are briefly described.
- 2) A historical view of electron-mercury scattering is given together with bibliographies. It becomes apparent that the studies have been strongly biased toward elastic scattering for both experimental and theoretical studies.

Chapter 2; Theory of Electron-Mercury Elastic Scattering --- Modification and Extention of Current Theory

- 1) Particular attention needed for the theoretical treatment of electronheavy atom scattering is described.
- 2) e -Hg elastic scattering is treated relativistically using a non-relativistic Hartree potential. The scattering amplitude is written down for an arbitral incident direction of electron beam.
- 3) The efficient and accurate computer program is developed for electronatom elastic scattering. Theoretical calculation is made for both the
 differential cross section and spin polarization of the incident electron energy between 300 and 2000 eV. In these energy regions, the
 calculated results agree well with both experimental results and other
 theoretical results calculated by more accurate but complex theories,
 which include exchange effect between incident and atomic electrons, and
 distortion of atom by electric field of incident electrons.
- 4) The cross section calculated in this way provides important information concerning study on the behaviour of Auger electrons in solids using Monte-Carlo calculation. Because the screened Rutherford scattering formula which is usually used in the Monte-Carlo calculation breaks down for low energy electron scattering.

Chapter 3; Theory of Electron-Mercury Inelastic Scattering --- Application of DWB Theory

- 1) DWB approximation is applied to electron-impact excitation of 6¹P state of mercury.
- 2) The computer program is developed for electron-atom inelastic scattering using the DWB approximation. The DWB calculation is performed for atomic wave functions constructed using Coulomb approximation and Hartree approximation in the incident electron energy of 50 to 500 eV.
- 3) It is shown that at an impact energy greater than 300 eV, the spin polarization of inelastic electrons differs considerably from that of elastic electrons at scattering angles less than 90° for both the atomic wave functions.

Chapter 4: Measurement of Loss Spectra

- 1) Construction of an apparatus for the measurement of loss spectra is described.
- 2) The loss spectra of electron-mercury scattering are obtained in the energy region between 300 and 1000 eV at a scattering angle of 50 to 110°.
- 3) Allowed transitions such as 6¹P and 6p'³P excitation are dominant in these energies and scattering angles, and show similar diffraction pattern to elastic scattering. However, the transition rate to 7¹S state (strictly forbidden transition) is higher than that to 6³P state, and 6³P state is higher than that to 7¹P state (allowed transition).

Chapter 5; 6¹P Excitation --- Comparison of Theory and Experiment

- 1) The results in Chapters 3 and 4 are compared.
- 2) The DWB calculation using Coulomb approximated atomic wave function provides values of cross section in close agreement with experiment, however, the DWB approximation using Hartree atomic wave function provides profiles of angular dependence of cross section and spin polarization in close agreement with experiment.
- 3) From this result, it is conjectured that the actual 6s and 6p wave functions of mercury may have similar profiles to that of Hartree wave functions. However, (6s) wave function for (6s)² state and that for (6s)(6P) state may be much more isolated from each other in the actual case than in Hartree case.

Part II. ESP-Detector Using Mercury Vapour

Chapter 6; Introduction

1) Studies on ESP experiments and ESP detectors used for these experiments are briefly reviewed.

Chapter 7; Optimum Conditions of the ESP Detector.

- 1) Optimum conditions of ESP detector are systematically investigated utilizing the results in Chapters 2,3 and 4.
- 2) The conclusions obtained are E=300 eV, $\theta=95^{\circ}$, $\Delta E\approx13$ eV and $\Delta\theta\approx10^{\circ}$.
- 3) The spin-polarization detector using mercury is compared to the conventional Mott detector to draw out the conclusion that the former type is more appropriate for wider application.

Chapter 8; Double Scattering Experiment

- 1) An apparatus for double scattering experiments is described, using the conclusion derived in Chapter 7.
- 2) The Pierce-type electron gun using LaB₆ single crystal cathode is designed and constructed for double scattering experiment.
- 3) It is proposed that an ESP detector of this type may be also used as a polarized electron source which provides a powerful method particularly in the region of surface physics.

APPENDIX 1. QUALITATIVE EXPLANATION OF THE DIFFRACTION EFFECT IN @-ATOM SCATTERING

One of the most important reason for the occurrence of the diffraction effect is that a wave length of low and intermediate energy electrons is comparable to the radius of an atom as has already been mentioned in Sec.1-1. Although the atomic radius of various elements is comparable with each other, the diffraction effect becomes clear and complex for heavier elements. Furthermore, the maximum impact energy for the diffraction effect to occur shifts to higher energies for heavier elements. For example they are 6 eV for H and 15 eV for He (Mott and Massey 1965), however, higher than 10 keV for Hg. The following consideration provides a qualitative explanation for these phenomena. The diffraction pattern appears if only several partial waves with considerable values of phase shifts contribute to scattering. For this, atomic potential should be narrow and deep enough, and attractive. This is because for attractive case, atomic potential can pull in considerable cycles of wave if the deepness of the potential is sufficient, which results in large phase shift. This is not the case for narrow and repulsive potential because the cycles that can be swept out of the potential region are very small, which results in small phase shift. If the potential is long range, a number of partial waves contribute to scattering, so diffraction phenomena can not be observed for both attractive and repulsive potentials.

The radial wave equation is written as

$$\frac{\mathrm{d}^{2}L}{\mathrm{d}r^{2}} + \frac{2}{r} \frac{\mathrm{d}L}{\mathrm{d}r} + (K^{2} - U(r) - \frac{l(l+1)}{r^{2}}) L = 0 , \qquad (A-1-1)$$

for non-relativistic case (cf. equation 2-32). It is seen that an effective potential consists of an attractive atomic potential and repulsive centrifugal potential. Putting $U(r) = -2 \frac{Z e^2}{r} \exp(-r/a_0)$ for simplicity, we obtain condition for atomic number,

$$Z > l (l+1) /a_0 \cdot e^2 \sim l (l+1),$$
 (A1-2)

which is the condition that the atomic potential dominates the centrifugal potential in a certain radial regions. In equation (A1-2), the screening parameter a_0 is assumed to be the order of Bohr radius. It is seen from equation (A1-2) that the number of partial waves which undergo an atomic potential dominantly becomes larger as the z-number increases. This means

that the diffraction pattern becomes complex for heavier element. Furthermore, a main part of an \boldsymbol{l} -th partial wave exists around the principal region of the effective potential if

$$Ka_0 < 1$$
 , (A1-3)

where K is a wave number of incident electron. From equation (A1-2) and (A1-3), the maximum impact energy where the diffraction effect occurs clearly is estimated as i.e. 13 eV for H and 1000 eV for Hg. Large discrepancy for mercury will be reduced if the depth of the atomic potential is taken into consideration.

APPENDIX 2. INCAPABILITY OF POLARIZING AND ANALYZING ELECTRON SPIN BY MACROSCOPIC METHOD

Let us consider at first producing polarized electrons by macroscopic field (a kind of Stern-Gerlach experiment).

Suppose that a beam of electrons travels along the z-axis with velocity v_z in an unhomogeneous magnetic field \mathbf{H} . It is assumed that H_z is everywhere zero, and that in the xz-plane H_y is also zero i.e. an actual shape of magnet—has a same cross section with respect to xy-plane along z-axis and is symmetric with respect to xz-plane (see Fig.A-1). The force on the electron tending to split the beam is

$$e = \frac{\partial H_x}{\partial x}$$
 (A2-1)

On the other hand, because of the finite breadth of the electron beam, electrons travelling at a distance Δy from the xz-plane will be subject to a force

$$e v_z H_y$$
, (A2-2)

in the x-direction. Considering that

$$div (\mathbf{H}) = 0 , \qquad (A2-3)$$

equation (A2-2) can be rewritten as

$$e \ v_z \ \partial H_x / \partial x \cdot \Delta y$$
 (A2-4)

This force causes a spreading of the beam, so should be smaller than (A2-1), i.e.,

$$e v_z \partial H_x / \partial x \cdot \Delta y < e \partial H_x / \partial x$$
. (A2-5)

However, the uncertainity principle states, that

$$\Delta v_y \cdot \Delta y \sim 1$$
 . (A2-6)

Inequality (A2-5) therefore leads to the inequality

$$\Delta v_y > v_z$$
 (A2-7)

That is to say, the slit must be so narrow (of the order of the de Broglie wave length) that we have not got a beam at all, but a cylindrical wave emerging from it (Mott 1929).

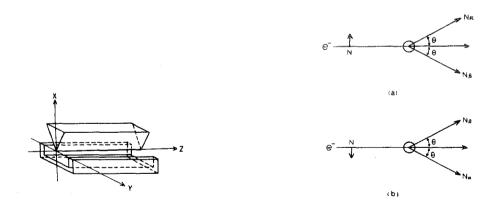


Fig A-1 Schematic diagram of the magnet.

Fig. A-2. Scattering asymmetry for totally polarized incident electron beam.

The situation is similar for detecting electron spin. Suppose the electron was at distance R from the magnetometer, then the order of magnitude of the magnetic field due to the spin is

$$e/R^3$$
 . (A2-8)

There may be a magnetic field due to the motion of the electron, the order of which is

$$e \ v/R^2$$
 , (A2-9)

where v is the velocity of the electron. From the uncertainity principle

$$\Delta R \quad \Delta v \sim 1$$
 (A2-10)

where ΔR and Δv are the uncertainties in our knowledge of R and v. Now in order that equation (A2-8), the effect of the spin, shall be observable, it must be greater than the uncertainty in equation (A2-9). That is to say,

$$e/R^3 > e \Delta v/R^2$$
, (A2-11)

Hence from equation (A2-10)

$$\Delta R > R$$
 (A2-12)

Measurement will therefore be impossible (Mott 1929).

APPENDIX 3. RELATIVISTIC RUTHERFORD SCATTERING FORMULA

For Coulomb potential $-Z\,e^2/r$, the integral in equation (2-26) can be performed and results in

$$\begin{split} f_{Born} &= Z e^{2} \left\{ H(\mathbf{k}_{f}) + W \right\} / (\mathbf{k}_{i} - \mathbf{k}_{f})^{2} \cdot u(\mathbf{k}_{i}) \\ &= Z e^{2} / (4 \mathbf{k}^{2} \cdot \sin^{2}\theta / 2) \left\{ H(\mathbf{k}_{f}) + W \right\} u(\mathbf{k}_{i}), \end{split} \tag{A3-1}$$

where $\phi_j(r^*) = \mathrm{e}^{i\,\mathbf{k}} i^{\mathbf{r}} u(\mathbf{k}_i)$ and $w + H(\mathbf{k}_f) = w - \mathbf{a}\,\mathbf{k}_f - \beta$. The operator $w + H(\mathbf{k}_f)$ gives 0 when operated to negative energy states and gives finite value when operated to positive energy states, which assures the final states being in positive energy states. Thus

$$d\sigma/d\Omega = |f_{Born}|^2 = \{Ze^2/(4K^2 \cdot \sin^2\theta/2)\}^2 2Wu(\mathbf{k}_i)^+ \{H(\mathbf{k}_f) + W\}u(\mathbf{k}_i)^- \}$$
(A3-2)

The linearly independent solution of free states can be written as

$$u_{1}(\mathbf{k}_{i}) = \sqrt{(W+1)/2W} \begin{cases} 1 \\ 0 \\ K_{iz}/(W+1) \\ (K_{ix}+iK_{iy})/(W+1) \end{cases}, \tag{A3-3}$$

and

$$u_{2}(\mathbf{k}_{i}) = \sqrt{(W+1)/2W} \begin{cases} 0 \\ 1 \\ (K_{i}x^{-i}K_{i}y)/(W+1) \\ -K_{i}z/(W+1) \end{cases}, \tag{A3-4}$$

which is proved by direct substitution. For the state expressed by equation (A3-3), equation (A3-2) gives

$$\begin{split} \mathrm{d}\,\sigma/\mathrm{d}\,\mathcal{Q} &= \frac{Z^2 \ e^4}{4\,K^4 \ \sin^4\theta/2} \cdot \frac{1}{2} \left\{ (W^2 + 1) + (\mathbf{k}_i, \mathbf{k}_f) \right\} \\ &= \frac{Z^2 \ e^4}{4\,K^4 \ \sin^4\theta/2} \left(W^2 - K^2 \cdot \sin^2\theta/2 \right) \\ &= \frac{Z^2 \ e^4}{4\,v^4 \sin^4\theta/2} \left(1 - v^2 \cdot \sin^2\theta/2 \right) (1 - v^2) \end{split}$$
(A3-5)

where v=K/W Equation (A3-5) is just equal to equation (2-27). The calculation for the state expressed by equation (A3-4) also results in the same equation as (A3-5), this means that Sherman function always equals to zero in Born approximation. So for the analysis of phenomena concerning spin polarization, the Born approximation is an ineffective approximation.

To investigate the origin of the second factor of equation (A3-5), we shall treat a spin 0 particle by Klein-Gordon equation, i.e.

$$\{(W-V)^2-(\mathbf{p}^2+1)\}\ \psi=0 \tag{A3-6}$$

A similar procedure adopted in Sec.2-2-1 gives the integral equation of (A3-6) as follows; The Lippmann-Schwinger equation of (A3-6) is written as

$$\psi = \mathbf{0} + \frac{1}{W^2 - \mathbf{D}^2 - 1 + i \cdot \epsilon} (2WV - V^2) \psi. \tag{A3-7}$$

Using equation (2-21),

$$\psi = \boldsymbol{\phi} - \frac{1}{4\pi} \frac{e^{iKr}}{r} \int e^{-i\mathbf{k}_f \mathbf{r'}} (2WV(\mathbf{r'}) - V(\mathbf{r'})^2) \psi(\mathbf{r'}) d\mathbf{r'}, \quad (A3-8)$$

the notation used here is same as that used in Sec.2-2-1.

Introducing first Born approximation, i.e. $\psi \to \phi$, $2^{WV} + V^2 \to 2^{WV}$ equation (A3-8) results in

$$\psi = \mathbf{\Phi} - \frac{e^{iKr}}{r} \cdot Z e^{2} 2W / (\mathbf{k}_{i} - \mathbf{k}_{f})^{2} . \tag{A3-9}$$

Thus

$$f_{KG} = -Z e^2 W / (2K^2 \cdot \sin^2 \theta / 2)$$
 (A3-10)

and

$$\left(\frac{\mathrm{d}\,\sigma}{\mathrm{d}\,\Omega}\right)_{KG} = \frac{Z^2 e^4}{4K^4 \sin^4 (\theta/2)} W^2
= \frac{Z^2 e^4}{4v^4 \sin^4 (\theta/2)} (1-v^2) .$$
(A3-11)

The comparison with equation (A3-5) or (2-27) shows that the factor $(1-v^2 \cdot \sin^2\theta/2)$ is dropped out in the case of spin 0 Klein-Gordon particle. It may be concluded that this factor reflects the effect of electron spin (Nishijima, 1973).

APPENDIX 4. QUALITATIVE EXPLANATIONS OF THE TWO ROLES OF SHERMAN FUNCTION

Let scattering efficiencies be α and β for spin-up electrons scattered to left and right side respectively, then α and β are also the scattering efficiencies for spin-down electrons scattered to right and left side respectively (see Fig.A-2). Then for an initially unpolarized electron beam, the spin polarization P_L after scattering to left side may be expressed as

$$P_{L} = \frac{N\alpha - N\beta}{N\alpha + N\beta} = \frac{\alpha - \beta}{\alpha + \beta} \tag{A4-1}$$

On the other hand, the left-right asymmetry for a totally polarized incident electron beam (spin-up state) may be expressed as

$$N_R/N_L = \beta/\alpha = (1-P_L)/(1+P_L)$$
 (A4-2)

From equation (3-7), it is seen that ${\it P}_{\it L}$ plays also a role of Sherman function.

On the other hand, for example in the case of exchange scattering, P and S are not equal to each other. Putting direct and exchange scattering amplitude as $f(\theta)$ and $g(\theta)$, we have the cross section for an unpolarized electrons scattered by totally polarized atoms as follows (Kessler 1976);

for spin-up and spin-down atomic state respectively. Then the spin polarization P of initially unpolarized electrons scattered by totally polarized spin-up atoms is expressed as

$$P = \frac{|f(\theta) - g(\theta)|^{2} + |g(\theta)|^{2} - |f(\theta)|^{2}}{|f(\theta) - g(\theta)|^{2} + |f(\theta)|^{2} + |g(\theta)|^{2}}.$$
(A4-5)

On the other hand, the scattering intensity of totally polarized spin-up and spin-down electrons scattered by totally polarized spin up atoms are $|f(\theta) - g(\theta)|^2$ and $|f(\theta)|^2 + |g(\theta)|^2$, respectively. So the value corresponding to the value P in equation (A3-5) may be expressed as

$$S = \frac{|f(\theta) - g(\theta)|^2 - |f(\theta)|^2 - |g(\theta)|^2}{|f(\theta) - g(\theta)|^2 + |f(\theta)|^2 + |g(\theta)|^2}$$
(A4-6)

It is worth noting that this is not a left-right asymmetry but a "spin-up-down" asymmetry (Kessler, 1976).

APPENDIX 5. VARIOUS CALCULATION PROCEDURES FOR THE ESTIMATION OF PHASE SHIFT

- 1) A direct integration of equation (2-28) by Runge-Kutta process was performed by Bunyan (1962). This method was usually used in the calculation of atomic wave function. (e.g. Mayer 1957)
 - 2) Putting $g_{\kappa} = a^{1/2} G_{\kappa} / r$ and substituting in equation (2-32) one gets

$$d^{2}G_{l} / dr^{2} + \left[K^{2} - l (l+1) / r^{2} - U_{l}(r)\right]G_{l} = 0,$$
(A5-1)

where $-U_l = 2WV + V^2 + \frac{(l+1)}{r} \frac{a'}{a} - \frac{3}{4} \frac{a'^2}{a^2} + \frac{1}{2} \frac{a''}{a}$.

Equation (A5-1) shows that the difference from the non-relativistic equation is only the potential that should be adopted. This method is quite suitable if there has already existed a computer program for non-relativistic equation (Madison and Shelton 1973) or if one wants to compare the results between relativistic and non-relativistic calculations. (Meister and Weiss 1968).

3) Another method is the power expansion method developed by Bühring (1965). He divided the radial region into three and put

$$V^{I}(r) = \sum_{m=-1}^{\infty} v_{m}^{I} r^{m}$$
 (A5-2-a)

$$V^{M}(r) = \sum_{n=1}^{\infty} v_{m}^{M}(y) (r-y)^{m}$$
(A5-2-b)

$$V^{E}(r) = v_{-1}^{E} r^{-1}$$
 (A5-2-c)

and

$$\begin{pmatrix} f^{I}(r) \\ g^{I}(r) \end{pmatrix} = \alpha r^{-1+s} \begin{cases} \sum_{n=0}^{\infty} a_{n}^{I} r^{n} \\ \sum_{n=0}^{\infty} b_{n}^{I} r^{n} \end{cases} \tag{A5-3-a}$$

$$\frac{f (r)}{g (r)} = r^{-1} \begin{cases} \sum_{n=0}^{\infty} a_n^M (r-y)^n \\ \sum_{n=0}^{\infty} b_n^M (r-y)^n \end{cases}$$
(A5-3-b)

$$\frac{f^{E}(r)}{g^{E}(r)} \sim C e^{tr} r^{s} \begin{cases} \sum_{n=0}^{\infty} a_{n} r^{-n} \\ \sum_{n=0}^{\infty} b_{n} r^{-n} \end{cases} \tag{A5-3-c}$$

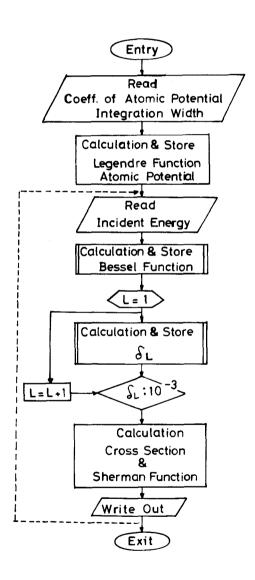
corresponding to the three regions. Substituting in equation (2-28), one obtains series of coefficients. This method provides one a method to escape from truncation errors.

4) Fourth method is the one developed by Lin et al. (1963) and used by Bunyan and Schonfelder (1965), and in the present calculation (see Sec. 2-4). As is shown, equation (2-51), is a non-linear equation, so it is very difficult to treat it in an analytical manner. However, this method separates the wave function into two parts i.e. amplitude and phase parts, in order to obtain a slowly changing variables. Furthermore, these equations are first order differential equations and for the evaluation of phase shift, it suffices to treat only the former. (see equation (2-51-a)).

It is expected that the fourth method provides a sufficient accuracy and simple calculation procedures for the calculation using high speed digital computer.

APPENDIX 6. COMPUTER PROGRAM LIST

a) Elastic scattering case



```
0004
0004
0006
0006
0007
0008
0009
0011
0012
0013
0015
0016
0017
                 TANDL (N,2)=0.0
                 FJ(N)=0.0
                 FNEU(N) =0.0
          1100 CONTINUE
                 NX1=50+10=NX
                FNX=NX1
FNX=FNX=0.01745329252
                 XECOS (FNX)
                 P0=1.0
0018
0019
0020
0021
                P1=X
FL10=0.C
                 FL20=0.0
0022
0023
0024
0025
                 FL11=X+1,0
                 FL21=X-1.0
FL1(NX,1)=FL10
                 FLI (8x, 2) =FL11
                 FLJ(NX.1) #FL20
0026
0027
                FLJ(NX,2)=FL21
DD 10 NY=3,300
 0028
0029
0030
                 FLI(NX,NY)=((2,0,FNY,3,0)*X#FL11~(FNY-1,0)*FL10~(1,0+X)*P0)/(FNY-2
                1.0)
FLJ(NX.NY)=((2.0#FNY-3.0)#X#FL28~(FNY-1.0)#FL20~(1.0-X)#P0)/(FNY-2
 0031
               1.0)
P2=((2_0#FNY=3.0) #X#P1=(FNY=2.0) #P0)/(FNY=1.0)
 0032
0033
                 FL10=FL11
                 FL11=FLI(NX,NY)
 0034
                 FL20=FL21
FL21=FLJ(NX,NY)
 0036
                 PO=P1
             P1=P2
10 CONTINUE
 0038
0039
 9040
9041
9042
9043
                 DO 20 NY=3:10
                 FNYANYI
                 FNY2=FNY+2.
 0045
                 NYIANY
 9046
                 P(NX)=(FL1(NX1,NY)+FLJ(NX1,NY))/FNY2
 0047
0048
0048
             30 CONTINUE
WRITE (6,200) NY1, (P(NX), NX*1,7)
             200 FORMAT ( 140 . 12 . 7E15 . 7)
 0050
             20 CONTINUE
12YO DE LEGENDRE NO KEISAN OWARISSES
 0051
0052
0053
0054
0055
0056
0056
0058
                 PB1=PB1+3.553022E-2
                  PR2=PR2#3.553022E-2
                  PB3=PB3+3.553022E-2
                 PA1=PA1+.58377491
PA2=PA2+.58377491
PA3=PA3+.58377491
                  Z0=PA1+PA2+PA3
                  Z1=PA1+PB1+PA2+PB2+PA3+PB3
                  Z2=PA1*PB1*PB1*PA2*PB2*PB2*PA3*PB3*PB3
                  Z3=PA1*PB1**3.0.PA2*PB2**3.0.PA3*PB3**3.0
                  21=-21
 0061
0062
0063
0064
0065
0066
0067
0068
0069
                 Z1=-Z1
Z2=Z2#0,5
Z3=-Z3/6,
RACIUS=RADIUS/10.0**8.0
RADIUS=RADIUS/3.88145E-41
                  RAD=.1
                  RAFI=5.
                 RADIU=200.
ERADI=RAD=EXP(RADI)
                  FFN=RADI/H#2.#ERADI...1
  3071
3072
                  NN=1HT(FFN)
                  NN=Nt-/2#2+1
                  HI=RAPI/FLOAT (NO-1)
```

```
DO 40 N#1:NN
FF#FLOAT(N+1:#H1
RR(N)#RAD#EXP(FF)
                    ZZ(N) =PA1=EXP(=PB1=RR(N))+PA2=EXP(=PB2=RR(N))+PA3=EXP(=PB3=RR(N))
9078
9079
9080
9081
9082
9083
               40 CONTINUE
                    H1=2.+H1
                    NN1=NN+1
00 41 NENN1+10000
                    RR (N) = , 0
                    22(N) = . 0
               41 CONTINUE
                      FFNN= (RADIU-ERADI) /H#2.+.1
                    NANEINT (FFNN)
0086
                   NNN=NNN/2+2+1
H2# (RADIU-ERADI) /FLOAT (NNN-1)
9088
                    HaH2#2,
                   DO 42 N#1, NNN
FFEFLOAT (N-1) #H2+ERADI
                   ZZZ (N) mPA1#EXP (-PB1#FF) +PA2#EXP (-PB2#FF) +PA3#EXP (-PB3#FF)
0093
                   NNN1=NNN+1
DD 43 N#MMNI-15000
0096
0097
0098
                    ZZZ (N) = , 0
               43 CONTINUE
                   FFNN= (RADIUS_RADIU) /H/2.+.1
                   NNNN=INT (FFNNN)
H3=(RADIU5-RADIU)/FLDAT(NNNN-1)
ŎŎ99
0100
            H3 (RAD1U5-KAD1U)/FLOAT (NINN)

WRITE (6.94001H, H1, H2, H3, NN, NAN, NNN

9400 FORMAT (//LHO, 4615, 7, 3115)'

HRITE (6.94501 (RR(N), NR1, 1201, 200)

HRITE (6.94501 (ZZZ(N), NR1, 1201, 200)

MRITE (6.94501 (ZZZ(N), NR1, 1201, 200)
0102
0103
0104
0106
            9450 FORMAT (7E15.6)
RADIU1=P81=RADIU
RADIU2=P82=RADIU
0108
0109
0110
                    RADIU3=PB3*RADIU
                   NADIUSEFOSARADIU
DO=PALeEXP(=RADIU1)+PA2eEXP(=RADIU2)+PA3eEXP(=RADIU3)
D1=PALeEXP(=RADIU1)+PA2ePB2eEXP(=RADIU2)+PA3ePB3eEXP(=RADIU3)
ÓLII
                    RACIUU#PADIUS-RADIU
Q112
                   D1=RADIUURD1
D2=PA1=PB1=PB1=EXP(=RADIU1)+PA2=PB2=PB2=EXP(=RADIU2)+PA3=PB3=PB3=PB3=F
0113
0114
                   1XP (-RADIUS)
0115
0116
                    D2=RADIUU+RADIUU+D2
                    SGM=D2+.5-D1+3.+D0+6.
FMUU=-D2+D1+5.-D0+8.
0117
0118
                     FMUU-FMUU
            FMUUS-FMUU

FMUUS-FMUUS-S-01*2,*D0*3,

MRITE[6,9500]RADIURADIUS,$GM,FMUU,FMUU

9500 FORMATI(7M RADIUS-E10,3,8M RADIUS-E10,3,5M SGM=,E10,3,6M FMUU=,E1
0120
0121
                   10.3.6H FNUU=,E10.3)
0122
            READ (5,9000) NEN
            9000 FORMAT([10]

NENN=1

9200 READ(5,9100)NENERG

9100 FORMAT([10]

WRITE(6,900) MENERG
 0124
 0125
0126
              G128
 6129
 0130
                    FK=FK##0.5
RK=RADIUS#FK
 0131
 0132
               CALL BESSEL MRITE(14,300) KR 3CC FCPMAT(1140,300) KR 3CC FCPMAT(1140,300) KEISANSARETA BESSEL NO JISU #,14,5H DESU)
 0133
 0134
 0135
 0136
                     WRITE (6,350) HK
               35C FORMAT(140,16H HASU * RADIUS *,E15.7,5H DESU)
WRITE(6,360) (FJ(N),N=1,7)
360 FORMAT(////140,7E15,6)
 0137
 6139
 9140
                     WR1TE (6,370) (FNEU(N),N=1,7)
 6141
               370 FORMAT (1H0, 7E15.6//)
 0142
                    LEC
```

6143	10	R9-L-1
9144	17	FLaL
0145		FREEK
6146		PHAIGS=20/FKK
A140		PHATOCETT, DEPHATOSEPHATOST 480.5
W147		
9148		IF(K)1.2.3
0149		GD TO 1090
A) an	ž	WRITE(6,400)
0150 0151	ARA	FORMAT(1HO,10H OKASHIIYO)
6121	400	60 70 9999
0152		GO 10 9999
5153	,	PRATOC=-PHATOC
0152 0153 0154	1050	PHAILE (EMERGY-Z1-PHAIDC) /11-0-2-0-FKK-PHAIDC)
0155		PHAIZIEZ, DEPHAI EPHAIOSA (1.0-PKK APHAIL) -Z2
6122		PHAIZEZ, OR (1, O.FKKEPHAIOC)
0154 Q157		Mista Mista: Bist
0157		PHAIZEPHAIZI/PHAIZ
Q150		PMAI3122.0aPHAI2aPHAI05#(1.0-2.0aFkKaPHA11)+Z3 PHAI3222.0aPHAI1aPHAI1aPHA10C#(1.0-2.0aFkKaPHAI1/3.0)
Q159		PRATIZE 2 BaPHATIAPHAILAPHAIOCA(1.0-2.04FKK4PHAI1/3.0)
4,24		DMATTER A. 2 DAFKKEPHAIDC
9160 9161		PHAI3#3,0=2,0#FKK#PHAI0C PHAI3# PHAI3# PHAI3#7 PHAI3
6393		Print 3 transferrance 3
6142		PHAIO#ARSIN(PHAIOS)
8163		TF (PHATA) 4.4.4
4103		PHAIGES, 141592654-PHAIO PHAIDPHAIGE, 3-RADE PHAIL-RADE (PHAIZ-RADEPHAIS)
0164		PRICE MITTEL & BIRE (BUST) . BAR-(BUST) . BAR-BUST 311
0145	•	PRESENTATION TO A PROPERTY OF THE PROPERTY OF
0166		CALL DIRAC (PHAI, FKK L. ENERGY, PAI, PAZ, PA3, PB1, PB2, PB3, RADIUS, PHAIL,
		H.SGM.FRUU.FNUU.RADI.RADIU.RADIUU)
2	•	TANPHL TAN (PHAIL)
Q167		THE PART OF THE PA
0167 0168		TANDLI=(ENERGY+1.0) *TANPHL+(1.0+FL+FKK) /RADIUS
6198		L10L+1
6170		L2=L+2
		TANDLUEFKEFJ(L2)=FJ(L1) RTANDL1
9171		TANDEDERREDICES - FICE I WINDE
0171 0172		TANDLE =FK-FNEU(L2) -FNEU(L1) +TANDL1
0173		1F(K)9,11,12
	_	
0174	9	TANDL(L1:1)=TANDL(DYLANDL: MRITE(6,1022)LK, PHAI, PHAIL, TANDL: FORMAT(1M, 3H L=,15,3%,3H K=,15,3%,6H PHAI=,E15,6,10X,7H PHAIL=,E1 15,6,10X,7H TANDL=,E15,3%,3H K=,15,3%,6H PHAI=,E15,6,10X,7H PHAIL=,E1 FORMAT(1H0,3H L=,15,3%,3H K=,15,3%,6H PHAI=,E15,6,10X,7H PHAIL=,E1
9175		MK11610-1005) P-K-Lust Shuwer Stauper (F191)
0176	1051	FORMAT(1H .3H L=,15,3X,3H K=,15,3X,6H PHA1=,015,6+10X,FH PHA1C=,01
		15.6.10x.7H TANDL#.E15.6)
6177	··· CAPA	EMPRATITUM SU I TE TE SE
0177	1032	TURNEY STORY CASE STORY
	1	15.6,10X,7H TANDL#,E15.6)
Õ178		1F(L)13,14,15
0179		WRITE (6,600)
	4.7	Manual Control of the
Grec	600	FORMAT (1HO-16H OKASHIIYO PARTZ)
	600	GO TO 9999
9101		GO TO 9999
0181 0182	600	GO TO 9999 TARDL(L1,2)#0,0
0181 0182 0183		GO TO 9999 TARDL((1,2)≠0,0 L±L+1
0181 0182 0183 0184	14	GO TO 9999 ↑ARD[:(1,2)≠0,0 L=L+1 GO TO 19
0181 0182 0183	14	GO TO 9999 TARDL((1,2)≠0,0 L±L+1
0181 0182 0183 0184 0185	14 15	GO TO 9999 TAMDL(11,2)≠0,0 L=L+1 GO TO 19 K#L
0181 0182 0183 0184	14 15	GO TO 9999 TARDL (11,2)#0,0 Let.1 CO TO 19 Kel Kel
0101 0102 0103 0104 0105	14 15	GO TO 9999 TARDL (11,2)#0,0 Let.1 CO TO 19 Kel Kel
0181 0182 0183 0184 0185 0187 0188	14 15	GO TO 9999 TARDE (11,2)=0,0 L=L+1 GO TO 19 WRITE(6,500) FORMAT(1,10-)6+ OKASHIIYO PARY3)
0181 0182 0183 0184 0185 0187 0188 0189	14 15 11 500	GO TO 9999 TARDE (11.2) # 0.0 Let. Ket. Ket.
0181 0182 0183 0184 0185 0187 0188 0189	14 15 11 500	GO TO 9999 TARDIL(1,2)=0,0 Let.+1 GO TO 19 WRITE(0,500) FORMAT(1,90-)6+ OKASHIIYO PART3) GO TO 9999 TARDIL(1,2)=TANDLU/TANDLL
0181 0182 0183 0184 0185 0187 0188 0189 0190 0191	14 15 11 500	GO TO 9999 TARDL (11,2)#0,0 Let.1 K#L K#L MRITE(0,500) FORMAT(1)M0,16H OKASHIIYO PARY3) GO TO 9999 TARDL (11,2)#5TANDLU/TANDLL MRITE(0,500) TARDL (11,2)#5TANDLU/TANDLL
0181 0182 0183 0184 0185 0187 0188 0189 0190 0191	14 15 11 500	GO TO 9999 TARDIL(1,2)=0,0 Let.+1 GO TO 19 WRITE(0,500) FORMAT(1,90-)6+ OKASHIIYO PART3) GO TO 9999 TARDIL(1,2)=TANDLU/TANDLL
0181 0182 0183 0184 0185 0187 0188 0189 0190 0191 0192	14 15 11 500	GO TO 9999 TARDL(11,2)=0,0 L=L+1 GO TO 19 WRITE(6,500) FORMAT(1)M0,16H OXASHIIYO PART3) GO TO 999 TARDL(11,2)=TANDLU,TANDLL WRITE(6,103)1L,K,PHAI,PHAIL,TANDL(L1,2) DEL:MATANTANDL(L1,1)
0191 0182 0183 0184 0187 0188 0189 0190 0191 0192 0192	14 15 11 500	GO TO 9999 TARDL (11,2) # 0,0 Let. K#L K#L K#L K#L K#L K#L K#L K#
0181 0182 0183 0184 0185 0187 0188 0189 0190 0191 0192 0193 0194	14 15 11 500	GO TO 9999 TARDL(11,2)=0,0 L=L+1 GO TO 19 KEL MRITE(6,500) FORMAT(1M0,16H OKASHIIYO PART3) GO TO 999 TARDL(11,2)=TANDLU,TANDLL MRITE(6,103)1L,K,PHAI,PHAIL,TANDL(L1,2) DEL:AATAN(TANDL(L1,1)) DEL:AATAN(TANDL(L1,2)) DEL:AATAN(TANDL(L1,2)) DEL:AATAN(TANDL(L1,2))
0181 0182 0183 0184 0185 0187 0188 0189 0190 0191 0192 0193 0194	14 15 11 500	GO TO 9999 TARDL (11,2)=0,0 Let-1 Ket MRITE(0,500) FORMAT(1)M0,16H OKASHIIYO PART3) GO TO 0999 TARDL (11,2)=TANDLU/TANDLL MRITE(0,500) FLETATAN(TANDL (11,1)) DELI=ATAN(TANDL (11,1)) DELI=ATAN(TANDL (11,1)) DELI=ATS(DELI) DELI=ASS(DELI) DELI=ASS(DELI)
0181 0182 0183 0184 0185 0187 0188 0189 0190 0191 0192 0193 0194	14 15 11 500	GO TO 9999 TARDL (11,2)=0,0 Let-1 Ket MRITE(0,500) FORMAT(1)M0,16H OKASHIIYO PART3) GO TO 0999 TARDL (11,2)=TANDLU/TANDLL MRITE(0,500) FLETATAN(TANDL (11,1)) DELI=ATAN(TANDL (11,1)) DELI=ATAN(TANDL (11,1)) DELI=ATS(DELI) DELI=ASS(DELI) DELI=ASS(DELI)
0181 0182 0183 0184 0185 0187 0188 0189 0191 0192 0193 0194 0193	14 15 11 500	GO TO 9999 TARDL (11,2)=0,0 L=L+1 GO TO 19 K=L MRITE(6,500) FORMAT(1M0,16H OKASHIIYO PART3) GO TO 999 TARDL (11,2)=TANDLU/TAMDLL MRITE(6,103)1L sK,PHAI;PHAIL,TANDL (L1,2) DELI=ATAN (TANDL (L1,1)) DELI=ATAN (TANDL (L1,2)) DELI=ATS (DELI) DELI=ATS (DELI) DELI=ABS (DELI) DELI=ABS (DELI)
0181 0182 0183 0184 0187 0188 0189 0190 0191 0192 0193 0194 0195 0196	14 15 11 500	GO TO 9999 TARDL (11,2)=0,0 L=L+1 EX
9181 0182 0183 0184 0185 0187 0188 0189 0191 0191 0193 0194 0193 0195 0197 0197	14 15 11 500	GO TO 9999 TARDL (11,200,0) Lete1 Ext. WRITE(0,300) FORMAT(1M0,10) OKASHIIYO PART3) GO TO 9999 TARDL (11,210,TAMDLL) FORMAT(1M0,10) OKASHIIYO PART3) GO TO 9999 TARDL (11,210,TAMDLL) FOR 1F (0,010,11,1,7,MAI,PHAIL,TAMDL(11,2)) DEL 1-AAS(TAM(TAMDL(11,2)) DEL 1-AAS(TAM(TAMDL(11,2)) DEL 1-AAS(TAM,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1
9181 0182 0183 0184 0185 0187 0188 0189 0191 0191 0193 0194 0193 0195 0197 0197	14 15 11 500	GO TO 9999 TARDL (11,200,0) Lete1 Ext. WRITE(0,300) FORMAT(1M0,10) OKASHIIYO PART3) GO TO 9999 TARDL (11,210,TAMDLL) FORMAT(1M0,10) OKASHIIYO PART3) GO TO 9999 TARDL (11,210,TAMDLL) FOR 1F (0,010,11,1,7,MAI,PHAIL,TAMDL(11,2)) DEL 1-AAS(TAM(TAMDL(11,2)) DEL 1-AAS(TAM(TAMDL(11,2)) DEL 1-AAS(TAM,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1
9181 9182 9183 9183 9185 9187 9188 9190 9191 9192 9193 9194 9195 9197 9197 9197	14 15 11 500	GO TO 9999 TARDL (11,2)=0,0 L=L+1 RITE(0,500) FDEMST(1)M0,00 NCASHIIYO PART3) GO TO 0999 TARDL (11,2)=TANDLU/TARDLL MRITE(0,500) FLOWAT(1)M0,10 NCASHIIYO PART3) GO TO 0999 TARDL (11,2)=TANDLU/TARDLL MRITE(0,1051)+, K,PPHAIL, TANDL (11,2) DEL1=ATAN(TANDL (11,2)) DEL1=ATAN(TANDL (11,2)) DEL1=ASS(DEL1) DEL1=ASS(DEL1) FDEL2=ASS(DEL2) IF(DEL2,GT,0,001)GO TO 16 IF(DEL2,GT,0,001)GO
9181 9182 9183 9183 9183 9185 9187 9189 9199 9199 9199 9199 9199 9199	14 15 11 500	GO TO 9999 TARDL (11,21=0,0) Let.1 Kel WRITE(0,300) FORMAT(1M0,16+ OKASHIIYO PART3) GO TO 9999 TARDL (11,21=TANDLU/TAMDLL MRITE(0,101)Li, K,PHAI,PHAIL,TANDL (11,2) DEL 1=ATAW(TANDL (11,1)) DEL 1=ATAW(TANDL (11,1)) DEL 1=ASS (DEL) FOR EL 2=ATAW(TANDL (11,2)) FOR EL 2=ATAW(TANDL (1
9181 9182 9183 9183 9184 9189 9190 9191 9192 9193 9194 9195 9196 9197 9198 9199 9200	14 15 11 500 12	GO TO 9999 TARDL (11,2)=0,0 L=L+1 REITE(=,500) FDEMST(1)MO; BH OKASHIIYD PART3) GO TO 0999 TARDL (11,2)=TANDLU/TARDLL MRITE(=,500) TARDL (11,2)=TANDLU/TARDLL MRITE(=,500) FLOELS-ATAN(TANDL (11,1)) DEL:ASTAN(TANDL (11,1)) DEL:ASTAN(TANDL (11,2)) DEL:ASTAN(TANDL (11,2)) DEL:ASS(DEL:) IF(DEL:,GT,0,001)GO TO 16 IF(DEL:,GT,0,001)GO TO 16 GO TO 18 L=L+1 IF(L,GT,300)GO TO 18 GO TO 19
9181 9182 9183 9183 9184 9185 9185 9185 9190 9191 9193 9194 9195 9196 9197 9196 9196 9196 9196 9196 9196	14 15 11 500 12	GO TO 9999 TARDL (11,21=0,0) Let-1 K#L MRITE(0,500) FORMAT(1M0,16+ OKASHIIYO PART3) GO TO 999 TARDL (LI,21=TANDLU/TANDLL MRITE(0,501)L, K,PHAI,PHAIL,TANDL (L1,2) DELI=ATAN(TANDL (L1,11) DELI=ATAN(TANDL (L1,21) DELI=ASS(DELI) COL2-ASS(DELI) COL2-ASS(DELI) GO TO 9999 TRODL (1,01) GO TO 16 GO TO 19
9181 9182 9183 9183 9184 9188 9188 9190 9191 9191 9193 9193 9195 8196 9193 9194 9195 8196 9196 9197 9197 9198 9199 9199 9199 9199 9199	14 15 11 500 12	GO TO 9999 TARDL (11,21=0,0) L=L+1 RITE(=,500) FORMAT(1)M0;16M OKASHIIYO PART3) OKASHIIYO PART3) TARDL (11,21=TANDLU/TARDLL MRITE(=,500) TARDL (11,21=TANDLU/TARDLL MRITE(=,500) DEL 1=ATAN(TANDL (11,11) DEL 1=ATAN(TANDL (11,11) DEL 1=ASIONEL1) DEL 1=ASIONEL1) DEL 1=ASIONEL1) DEL 1=ASIONEL1) DEL 1=ASIONEL1 IF(DEL,GT,0,001)GO TO 16 GO TO 18 L=L+1 IF(L,GT,300)GO TO 18 GO TO 19 CONTINUE MRITE(=,GT,750)L
9181 9182 9183 9183 9184 9188 9188 9190 9191 9191 9193 9193 9195 8196 9193 9194 9195 8196 9196 9197 9197 9198 9199 9199 9199 9199 9199	14 15 11 500 12	GO TO 9999 TARDL (11,21=0,0) L=L+1 RITE(=,500) FORMAT(1)M0;16M OKASHIIYO PART3) OKASHIIYO PART3) TARDL (11,21=TANDLU/TARDLL MRITE(=,500) TARDL (11,21=TANDLU/TARDLL MRITE(=,500) DEL 1=ATAN(TANDL (11,11) DEL 1=ATAN(TANDL (11,11) DEL 1=ASIONEL1) DEL 1=ASIONEL1) DEL 1=ASIONEL1) DEL 1=ASIONEL1) DEL 1=ASIONEL1 IF(DEL,GT,0,001)GO TO 16 GO TO 18 L=L+1 IF(L,GT,300)GO TO 18 GO TO 19 CONTINUE MRITE(=,GT,750)L
9181 9182 9183 9184 9185 9188 9189 9190 9191 9193 9193 9194 9195 9199 9200 9201 9202 9203 9204	14 15 11 500 12	GO TO 9999 TARDL (11,21=0,0) Let.1 GO TO 19 KML MRITE(0,500) FORMAT(1)M0:16H OKASHIIYO PARY3) GO TO 9999 TARDL (11,21=TANDLU/TANDLL MRITE(0,1051)L, K,PMAI,PMAIL,TANDL (11,2) DEL:1aTAN (TANDL (11,11) DEL:2aTAN (TANDL (11,12))
9 in 2 9 in 2 9 in 3 9	14 15 11 500 12	GO TO 9999 TARDL (11,2)=0,0 Let-1 KEL WRITE(6,500) FORMATI(1M0)16H OKASHIIYO PART3) GARROL (12,2)=TANDLU/TARROLL WRITE(6,1050) DEL 10-A12=TANDLU/TARROLL WRITE(6,1050)+L, FPHAIL, TANDL (11,2) DEL 10-ATAN (TANDL (11,2)) DEL 10-ATAN (TANDL (11,2)) DEL 10-ASIONEL (1) DEL 10-ASIONEL
9181 9182 9183 9184 9185 9188 9189 9190 9191 9193 9193 9194 9195 9199 9200 9201 9202 9203 9204	14 15 11 500 12	GO TO 9999 TARDL (11,21=0,0) Let-1 GO TO 19 KM MRITE(6,500) FDRMAT(1)M0:16+ OKASHIIYO PARY3) GO TO 9999 TARDL (L1,21=TANDLU/TANDLL MRITE(6,1051)L, K,PMAI,PMAIL,TANDL (L1,2) DELI=ATAN (TANDL (L1,11) DELI=ATAN (TANDL (L1,11) DELI=ATAN (TANDL (L1,2)) DELI=ASSIDELI) GO TO 9999 TARDL (L1,21=TANDL (L1,2)) DELI=ASTAN (TANDL (L1,2)) DELI=ASSIDELI) GO TO 18 GO TO 19 FILE(41,300)GO TO 18 GO TO 19 FORMAT(1)GIO,10X,26H KEISANSARETA PHASE SHIFT=,14,5H DESU) MRITE(6,770) FORMAT(1)GIO,10X,26H KEISANSARETA PHASE SHIFT=,14,5H DESU) MRITE(6,770) FORMAT(1)GIN ====================================
9 in 2 9 in 2 9 in 3 9	14 15 11 500 12	GO TO 9999 TARDL (11,2)=0,0 Let-1 KEL WRITE(6,500) FORMATI(1M0)16H OKASHIIYO PART3) GARROL (12,2)=TANDLU/TARROLL WRITE(6,1050) DEL 10-A12=TANDLU/TARROLL WRITE(6,1050)+L, FPHAIL, TANDL (11,2) DEL 10-ATAN (TANDL (11,2)) DEL 10-ATAN (TANDL (11,2)) DEL 10-ASIONEL (1) DEL 10-ASIONEL
9161 0162 0163 0164 0165 0165 0167 0167 0167 0167 0167 0167 0167 0167	14 15 11 500 12	GO TO 9999 TARDL (11,21=0,0) Lete1 GO TO 19 Kel WRITE(0,300) FORMAT(1 Mo,16) OKASHIIYO PART3) GO TO 9999 TARDL (11,21=TANDLU/TAMDLL MRITE(0,301)LI, K,PMAI,PMAIL,TANDL (11,2) DELISATAM(TANDL (11,1)) TEOREL, GT,0,001)GO TO 16 GO TO 18 GO TO 18 GO TO 18 GO TO 18 GO TO 19 GOMINUE GOMINUE TOPMAT(1 MO,10A,20H KEISANSARETA PHASE SHIFT=,14,5H DESU) WRITE(4,720) FORMAT(7,91H
9161 0162 0163 0164 0164 0165 0167 0160 0160 0160 0160 0160 0160 0160	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Let.+1 GO TO 19 K#L MRITE(0,500) FORMAT(1M0,16H OKASHIIYO PART3) GO TO 0999 TARDL (LI,21=TANDLU/TARDLL MRITE(0,1051)LK, PMAIL, PMAIL, TANDL (L1,2) DEL:ATAN (TANDL (L1,11) DEL:ATAN (TANDL (L1,11) DEL:ABS(DEL1) GEL:ABS(DEL1) GEL:ABS(DEL1) IF(DEL,GT,0,001)GO TO 16 IF(DEL,GT,0,001)GO TO 16 GO TO 18 Let.+1 IF(LS,T,300)GO TO 18 GO TO 18 CONTROL (LT,0) GO TO 18 GO TO 18 GO TO 18 GO TO 18 GO TO 19 GO T
9161 0162 0163 0164 0165 0165 0167 0167 0167 0167 0167 0167 0167 0167	14 15 11 500 12	GO TO 9999 TARDL (11,21=0,0) Let-1 TARDL (11,21=0,0) Let-1 RITE (6,300) FORMATI(1M0,16) OKASHIIYO PART3) GO TO 9999 TARDL (11,21=TANDL U,TANDLU,TANDL (11,2) DEL 10,000 DEL 10,0
9161 0162 0163 0164 0164 0165 0167 0167 0169 0169 0169 0169 0169 0169 0169 0169	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Let.+1 GO TO 19 K#L MRITE(0,500) FORMAT(1,M0,16) OKASHIIYO PART3) GO TO 0999 TARDL (LI,21)=TANDLU/TARDLL MRITE(0,101)L,K,PMAIL,TANDL(LI,2) DEL:ATAN(TANDL(LI,11) DEL:ATAN(TANDL(LI,11) DEL:ATAN(TANDL(LI,11) DEL:ABS(DEL) GO TO 0999 TARDL (LI,21) DEL:ABS(DEL) IF(DEL),GT,0,001)GO TO 16 IF(DEL),GT,0,001)GO TO 16 GO TO 18 Let.+1 IF(LE,GT,300)GO TO 18 GO TO 18 CONTINUE 750)L FORMAT(1,M1,DAX,26H KEISANSARETA PHASE SHIFT=,I4,5H DESU) WRITE(6,T70) FORMAT(1,M1,DAX,26H KEISANSARETA PHASE SHIFT=,I4,5H DESU) WRITE(16,T70) FORMAT(1,M1,DAX,26H KEISANSARETA PHASE SHIFT=,I4,5H DESU) WRITE(10,DAX,26H KEISANSARETA PHASE SHIFT=,I4,5H DESU)
9161 0162 0163 0164 0164 0165 0167 0160 0160 0160 0160 0160 0160 0160	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Let.+1 GO TO 19 K#L MRITE(0,500) FORMAT(1,M0,16) OKASHIIYO PART3) GO TO 0999 TARDL (LI,21)=TANDLU/TARDLL MRITE(0,101)L,K,PMAIL,TANDL(LI,2) DEL:ATAN(TANDL(LI,11) DEL:ATAN(TANDL(LI,11) DEL:ATAN(TANDL(LI,11) DEL:ABS(DEL) GO TO 0999 TARDL (LI,21) DEL:ABS(DEL) IF(DEL),GT,0,001)GO TO 16 IF(DEL),GT,0,001)GO TO 16 GO TO 18 Let.+1 IF(LE,GT,300)GO TO 18 GO TO 18 CONTINUE 750)L FORMAT(1,M1,DAX,26H KEISANSARETA PHASE SHIFT=,I4,5H DESU) WRITE(6,T70) FORMAT(1,M1,DAX,26H KEISANSARETA PHASE SHIFT=,I4,5H DESU) WRITE(16,T70) FORMAT(1,M1,DAX,26H KEISANSARETA PHASE SHIFT=,I4,5H DESU) WRITE(10,DAX,26H KEISANSARETA PHASE SHIFT=,I4,5H DESU)
9181 0182 0183 0189 0189 0189 0189 0190 0192 0192 0192 0192 0192 0202 020	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Let-1 TARDL (11,21=0,0) Let-1 RET TE (0,300) FORMAT (110,16) OKASHIIYO PART3) GO TO 999 TARDL (11,21=TANDLU/TAMDLL MRITE (0,1051) LK,PHAIPHAIL,TANDL (11,2) DEL 1=ATAN(TANDL (11,11) DEL 1=ATAN(TANDL (11,11) DEL 1=ASSIDELI) OCL2-ASSIDELI) OCL2-ASSIDELI) OCL2-ASSIDELI) OCL2-ASSIDELI) OCL3-ASSIDELI) OCL3-ASSIDELI OCL3-A
9161 0162 0163 0164 0164 0165 0166 0166 0166 0166 0166 0166 0166	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Let.+1 GO TO 19 Ket MRITE(0,500) FORMAT(1M0.16) OKASHIIYO PART3) GO TO 999 TARDL (11,21=TANDLU/TARDLL MRITE(0,1051)+, F.PHAIL, FANDL (11,2) DEL 1=ATAN(TANDL (11,1)) DEL 1=ATAN(TANDL (11,1)) DEL 1=ASIOEL1) DEL 1=ASIOEL1) DEL 1=ASIOEL1) DEL 1=ASIOEL1) IF(DEL, GT.0,001) GO TO 16 IF(DEL, GT.0,001) GO TO 16 GO TO 18 Let.+1 IF(L, GT.300) GO TO 18 GO TO 19 Let.+1 IF(L, GT.300) GO TO 18 HITE(0,1750)L FORMAT(1M0,10X,26H KEISANSARETA PHASE SHIFT=,14,5H DESU) WRITE(0,1750)L SHIP (10,10X,26H KEISANSARETA PHASE SHIFT=,14,5H DESU) WRITE(1,1750)L SHIP (10,10X,26H KEISANSARETA PHASE SHIFT=,14,5H DESU) WRITE(1,10X,1750)L SHIP (10,10X,26H KEISANSARETA PHASE SHIP (10,10X,
9181 9182 9183 9184 9187 9187 9187 9187 9187 9187 9187 9187	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Let-1 TARDL (11,21=0,0) Let-1 RET TE (0,500) FORMAT (110-16+0 OKASHIIYO PART3) GO TO 999 TARDL (L1,21)=TANDL U,TANDLL MRITE (0,1051)L K,PHAI,PHAIL,TANDL (L1,2) DEL 1=ATAN (TANDL (L1,11) DEL 1=ATAN (TANDL (L1,11) DEL 1=ASS (DEL 1) OCL2=ASS (DEL 1) OCL2-ASS (DEL 1) OC
9161 9162 9163 9164 9165 9166 9166 9166 9167 9169 9169 9169 9169	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Let.+1 GO TO 19 Ket MRITE(0,500) FORMAT(1)MO:100 OKASHIIYO PART3) GO TO 0999 TARDL (11,21=TANDLU/TARDLL MRITE(0,1001): K, PMAIL, PHAIL, TANDL (11,2) DEL:100 DEL:
9161 9162 9163 9165 9165 9166 9167 9169 9169 9169 9169 9169 9169	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Let-1 GO TO 19 KM MRITE(6,500) FORMAT(1)M0:166 OKASHIIYO PART3) GO TO 999 TARDL (L1,21)=TANDLU/TANDLL MRITE(6,1051)L, K,PMAI,PMAIL,TANDL(L1,2) DEL1=ATAN (TANDL (L1,11) DEL1=ATAN (TANDL (L1,11) DEL1=ATAN (TANDL (L1,21) DEL1=ASSIDELI) GO TO 9999 TARDL (L1,21)=TANDLU/TANDLL MRITE(6,10,001)GO TO 16 IF (DEL2,67,0,001)GO TO 16 GO TO 18 FORMAT(1,41,300)GO TO 18 GO TO 19 FORMAT(1,41,002,64 KEISANSARETA PHASE SHIFT=,14,5H DESU) MRITE(6,770) FORMAT(1,91,002,64 KEISANSARETA PHASE SHIFT=,14,5H DESU) MRITE(6,770) FORMAT(1,91,002,64 KEISANSARETA PHASE SHIFT=,14,5H DESU) MRITE(6,700) FORMAT(1,91,002,64 KEISANSARETA PHASE SHIFT=,14,5H DESU) MRITE(6,002,002,002,002,002,002,002,002,002,00
9161 9162 9163 9165 9165 9166 9167 9169 9169 9169 9169 9169 9169	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Let-1 GO TO 19 KM MRITE(6,500) FORMAT(1)M0:166 OKASHIIYO PART3) GO TO 999 TARDL (L1,21)=TANDLU/TANDLL MRITE(6,1051)L, K,PMAI,PMAIL,TANDL(L1,2) DEL1=ATAN (TANDL (L1,11) DEL1=ATAN (TANDL (L1,11) DEL1=ATAN (TANDL (L1,21) DEL1=ASSIDELI) GO TO 9999 TARDL (L1,21)=TANDLU/TANDLL MRITE(6,10,001)GO TO 16 IF (DEL2,67,0,001)GO TO 16 GO TO 18 FORMAT(1,41,300)GO TO 18 GO TO 19 FORMAT(1,41,002,64 KEISANSARETA PHASE SHIFT=,14,5H DESU) MRITE(6,770) FORMAT(1,91,002,64 KEISANSARETA PHASE SHIFT=,14,5H DESU) MRITE(6,770) FORMAT(1,91,002,64 KEISANSARETA PHASE SHIFT=,14,5H DESU) MRITE(6,700) FORMAT(1,91,002,64 KEISANSARETA PHASE SHIFT=,14,5H DESU) MRITE(6,002,002,002,002,002,002,002,002,002,00
9182 9182 9183 9183 9183 9189 9189 9189 9189 9189	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Lete1 GO TO 19 Kel MRITE(0,300) FORMAT(19M0,16) OKASHIIYO PART3) GO TO 9999 TARDL (11,21=TANDLU,TANDLL) MRITE(0,300) FORMAT(3MD1,1,1) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) FICIEL,07,0,001)GO TO 16 IF(0EL,2,GT,0,001)GO TO 16 IF(0EL,2,GT,0,001)GO TO 16 GO TO 18 HEI F(0,70) MRITE(0,70) FORMAT(3MT) FORMAT(3MT) MRITE(0,700) FORMAT(3MT) MRITE(0,700) MRITE(0,700) FORMAT(3MT) SAMPANDA 0,3X,6MT THETA,0X,10M CROSS SEC,6X,10M NORM C S,6X,10M 1 SMT) 1 SME FUN,10X,2M F,7X,10M MOD ASYM,3M e) 1 SME FUN,10X,2M F,7X,10M MOD ASYM,3M e) 1 SME(M) PO.0
9161 9162 9163 9163 9184 9185 9185 9186 9187 9189 9189 9189 9189 9201 9201 9202 9203 9203 9204 9203 9204 9203 9204 9203 9204 9205 9206 9207 9208 9209 9210 9211 9211 9211 9211 9211 9211	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Let-1 GO TO 19 KM MRITE(6,500) FORMAT(1)M0:166 OKASHIIYO PARY3) GO TO 9999 TARDL (L1,21)=TANDLU/TANDLL MRITE(6,1051)L, K,PMAI,PMAIL,TANDL(L1,2) DECLEATAN (TANDL (L1,2)) DECLEATAN (TANDL (L1,2)) DECLEATAN (TANDL (L1,2)) DECLEASSIDELI) GOLZ-ABSIDELI) GO TO 9999 TARDL (L1,21)=TANDL (MIL) DECLEATAN (TANDL (L1,2)) DECLEASSIDELI) GOLZ-ABSIDELI) GO TO 16 GO TO 18 GO TO 18 GO TO 18 GO TO 19 GO TO 19 GO TO 19 MRITE(6,7501) FORMAT(19H.10A,26H KEISANSARETA PHASE SHIFT=,14,9H DESU) MRITE(6,7701) FORMAT(19H.10A,26H KEISANSARETA PHASE SHIFT=,14,9H DESU) MRITE(6,7701) FORMAT(19H.10A,26H KEISANSARETA PHASE SHIFT=,14,9H DESU) MRITE(6,701) SHER FUNDAL SHIPPEN SHIPPE
9182 9182 9183 9183 9183 9189 9189 9189 9189 9189	14 15 11 500 12 16 18 750 720	GO TO 9999 TARDL (11,21=0,0) Lete1 GO TO 19 Kel MRITE(0,300) FORMAT(19M0,16) OKASHIIYO PART3) GO TO 9999 TARDL (11,21=TANDLU,TANDLL) MRITE(0,300) FORMAT(3MD1,1,1) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) DELJATAM(TANDL(1,1)) FICIEL,07,0,001)GO TO 16 IF(0EL,2,GT,0,001)GO TO 16 IF(0EL,2,GT,0,001)GO TO 16 GO TO 18 HEI F(0,70) MRITE(0,70) FORMAT(3MT) FORMAT(3MT) MRITE(0,700) FORMAT(3MT) MRITE(0,700) MRITE(0,700) FORMAT(3MT) SAMPANDA 0,3X,6MT THETA,0X,10M CROSS SEC,6X,10M NORM C S,6X,10M 1 SMT) 1 SME FUN,10X,2M F,7X,10M MOD ASYM,3M e) 1 SME FUN,10X,2M F,7X,10M MOD ASYM,3M e) 1 SME(M) PO.0

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DO 50 NX=1,10
NX1=50+10#NX
                                                                                                                                                                                                                                                                     NX1=50-10#0A

FNX1=NX1

FNX=FNX1/2,0

FNX=FNX+1,7453292E-2

FNX1=FNX1+1,7453292E-2
                                                                                                                                                                                                                                                          FRX1=FRX1=1.7453292E=2

ER=0.0

ER=0.0

HI=0.0

OD 60 Mi=1.L1

N2=M1=1

A1=TANDL [M1:1]=TAMDL [M1:1]=1.0

A2=TANDL [M2:2]=TAMDL [M2:2]=1.0

A2=TANDL [M3:2]=TAMDL [M3:2]=1.0

HI=(1.0/A1=1.0/A2)=FLJ(NX,M2)

EI=(TAMDL (M1:1)=TAMDL (M2:2)=TAMDL (M3:2)=TAMDL (M3:2)=TAMD
0222
0224
0225
0226
0227
0228
0230
0230
0231
           0233
0234
                                                                                                                                                                                                                                                                           ER#ER#ER1
EI#EI#EII
HR#HR#HRI
                0235
                0236
                                                                                                                                                                                                        He-He-He!

HEMPINTI

OCONTINUE

EREFOO, 5

EI-ELAO, 5

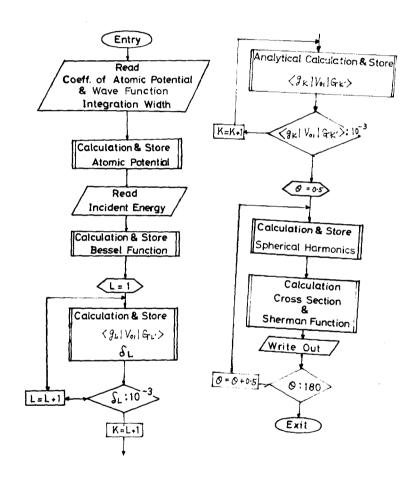
HIS-HROO, 6

HI
           0237
0238
0239
           0241
           0244
                0246
           0247
0248
           0249
0250
0251
           0253
           0255
0256
0257
0258
0259
0260
0261
0262
0263
0264
                                                                                                                                                                                                                                                                                NaMOD (N. 3)+1
SHIGIN) & SHIGMA
S(N) & SHERM
                                                                                                                                                      SHIG(N) #5H/GMA
S(N) #5H/FMA
ASYMODAS(1) #5H/G(1) *5(2) #5H/G(2) *5(3) #5H/G(3)
ASY #5H/G(1) #5H/G(2) *5H/G(3)
ASY #5H/G(1) #5H/G(2) *5H/G(3)
ASY #5H/G(1) #5H/G(2) *5H/G(3)
ASY #5H/G(1) #5H/G(3)
ASY #5H/G(1) #5H/G(3)
ASY #5H/G(1) #5H/G(3)
ASY #5H/G(1) #5H/G(3)
ASY #5H/G(1) #6H/G(3)
ASY #5H/G(1) #6H/G(1)
ASY #5H/G(1)
           0265
0266
0267
0268
0269
0270
           9271
0272
0273
                9275
6276
```

```
ōōō1
 0002
                 INN
Y1=2.=PHAI
 0003
                  NN1=NN-2
DD 3100 N=1.NN1.2
0004
                 N1=N-1
N2=R+2
RK1=FKK#SIN(Y1)+ZZ(N)+RR(N)*(ENERGY=COS(Y1))
0006
0007
0008
0009
0010
0012
0015
0016
0016
0017
0018
0020
0022
0023
0027
0027
                 RK1=H1=RK1
RK2=FKK#5IN(Y1=RK1)=ZZ(N1)=RK(N1)#(ENERGY=CO5(Y1=RK1))
                 RK2=H1+RK2
                  RK3#FKK#5IN(Y1+RK2)+ZZ(N1)+RR(N1)+(ENERGY=COS(Y1+RK2))
                 RK3=H[aPK3
RK4=FKK+5IN(Y1+2,*RK3)+ZZ(N2)+RR(N2)*(ENERGY-CO5(Y1+2,*RK3))
                  RK4sHIeRK4
                  Y1#Y1+(RK1+2,#(RK2+RK3)+RK4)/3.
          3100 CONTINUE
NNN1=NNN=2
R1=ERADI
                  R2=R1+H2
                  R3=R2+H2
                  DO 3200 N=1,NNN1,2
                  N1=N+1
                  N2EN+2
                  RK1=(FKK+SIN(Y11+2ZZ(N))/R1+ENERGY-COS(Y1)
                 RK!=M=RK1
RK2=(FKK+5IN(Y1+RK1)+ZZZ(N1))/R2+ENERGY+C05(Y1+RK1)
                 RK2=H=RK2
RK3=(FKK+5[N(Y1+RK2)+ZZZ(N1))/RZ+ENERGY+COS(Y1+RK2)
0030
0031
0032
0033
                 DK 3 mHe DK 3
                 RK4#(FKK#51N(Y1+2.#RK3)+ZZZ(N2))/R3+ENERGY+COS(Y1+2.#RK3)
                  Y1=Y1+(RK1+2.*(RK2+RK3)+RK4)/3.
0034
0035
0036
0037
0038
0039
0040
0041
0042
0043
0044
0045
                 R1=R1+H
R2=R2+H
           3200 CONTINUE
                  MNNN1=NNNN-1
                 R2=R1+H3#.5
                 R3#R1+H3
D0 3300 N=1,NNNH1
RRA1#R1-PADIUS
                 RRAZERZ-RADIUS
RRAZERZ-RADIUS
RRAZERRAZ/RADIUU
                 RRA2=RRA2/RADIUU
RPA3=RRA3/RADIUU
0047
                 Z1=RRA1=RRA1= (SGM+RRA1= (FMUU+RRA1=FNUU))
Z2=RRA2=RRA2= (SGM+RRA2= (FMUU+RRA2=FNUU))
Z3=RRA3=RRA3=(SGM+RRA3= (FMUU+RRA3=FNUU))
0048
0049
0050
0051
0052
0053
0054
0055
0056
0057
0058
                 RK1=(FKK=SIN(Y1)+Z1)/R1+ENERGY=COS(Y1)
                 RK!=H3#RK1
RK2=(FKK#SIN(Y1+RK1)+Z2)/R2+ENFRGY-CC5(Y1+RK1)
                 PK2=H3+PK2
                 RK3=(FKK+5IN(Y1+RK2)+Z2)/R2+ENFRGY-CC5(Y1+RK2)
                 RK3±H3BRK3
RK4±(FKK+5[N(Y1+2**RK3)+Z3)/R3+ENERGY-C05(Y1+2**RK3)
                  RK4#H3#RK4
                  Y1=Y1+(PK1+2.*(RK2+RK3)+RK4)/3.
0061
0061
                 R1=R3
R2=R2+H3
                  R3=R3+H3
$063
9064
           3300 CONTINUE
                 PHAILEY1/2.
4065
                  RETURN
                  END
```

SUBROUTINE BESSEL COMMON/BES/FJ(300),FNEU(300),RK,KR 5001 0002 5003 0004 0005 0006 0007 0008 5009 FJOBSTN(RK)/RK FNEU0=_COS(RK)/RK FNEU1=_(COS(RK)/RK+SIN(RK))/RK FJ(1)=FJ6 FJ(2)=FJ1 FJ(2)=FJ1 FNEU(1)=FNEU0 FNEU(2)=FNEU1 KR=INT(RK)+50 KROMINO (KR. 300) 0012 KR2=KR-1 k#2=kF=1 00 2100 kR1=3+kR2 fkR[i=kR1 fJ(kR1)==FJ0+(2_0=FKR1=3_0)=FJ1/Rk fMEU(kR1)==FMEU0+(2_0=FKR1=3_0)=FMEU1/Rk 0014 0015 0016 0017 0016 0019 FJ0=FJ1 FJ1=FJ(KR1) FNEUD#FNEU1 FNEUI#FNEU(KR1) 0020 0021 0022 0023 2100 CONTINUE DO 2200 KR1=KR,300 FJ(KR1)=0,0 FNEU(KR1)=0,0 0024 0026 0027 2200 CONTINUE RETURN 0028 END

b) Inelastic scattering case



```
INCLASTIC SCATTERING CROSS SECTION FOR MERCURY
                                                                                                                      വാവര്ട
                                                                                                                                        DO 600 I=1.NEN
 00001
                   DIMENSION GRAPH (121)
                                                                                                                      00066
                                                                                                                                            READ(5.5100) ENERG
                  DIMENSION ABTAN (2,2)
DIMENSION FUNC(2,2,2)
COMMON/SCOL/SINDL(300,2,2),COSDL(300,2,2),SCSQ(300,2,2)
COMMON/RADAL/RADIUS(6),RADIAL(10000)
 00002
                                                                                                                      00067
                                                                                                                                 5100 FORMAT (F10.3)
  00003
                                                                                                                      00068
                                                                                                                                        DO 50 N=1,2
                                                                                                                                       DO 50 J=1,2
DO 50 K=1,NSEK
 000004
                                                                                                                      00069
 00005
                                                                                                                      00070
                   COMMON/FKF/FK(2)
 00006
                                                                                                                      00071
                                                                                                                                        AMP1(M,J,K)=0.
                   COMMON/HHABA/HABA(4)
 00007
                                                                                                                      00072
                                                                                                                                    50 CONTINUE
 00008
                   COMMON/KKAISU/KAISU(4)
                                                                                                                      00073
                                                                                                                                        DO 61 J=1,2
 00009
                  COMMON/WAVPOT/POTE(2,3), WAVEFU(3,2,2)
COMMON/VVPOT/VPOT(10000,2), VPOTEI(10000)
                                                                                                                      00074
                                                                                                                                        DO 61 K=1,4
 00010
                                                                                                                      00075
                                                                                                                                        DO 61 Mm1,2
                   COMMON/AASSLG/ASSLEG(2000,3)
 00011
                                                                                                                      00076
                                                                                                                                       AMPL(J,K,M)=0.
PHAI(J,K,M)=0.
                  COMMON/BES/FJ(300,2), FNEU(300,2), RK(2), KR(2)
 00012
                                                                                                                      00077
                  COMMON/ZZB/ZBE(4,2)
 00013
                                                                                                                      00078
                                                                                                                                    61 CONTINUE
                  COMMON/PPHAI/PHAI(2,4,2),AMPL(2,4,2)
 00014
                                                                                                                      00079
 00015
                  CCMMON/PPHAIO/PHAIO(2,2),AMPO(2,2)
                                                                                                                      00080
                                                                                                                                        DO 60 J=1,NPN
 00016
                  COMMON/MATRIX/FMATRX(2000,2,2,2)
                                                                                                                      18000
                                                                                                                                       ASSLEG(J,M)=0.
 00017
                  COMMON/L1L/L(2,2)/EENERG/ENERGY(2)
                                                                                                                      00082
                                                                                                                                    60 CONTINUE
  00018
                  COMMON/PPHAI1/AMP1(2,2,10000)
                                                                                                                      00083
                                                                                                                                       DO 810 JJ=1,2
 00019
                   COMMON/TANDEL/TANDL(300,2,2)
                                                                                                                      AROON
                                                                                                                                        DO 810 J=1,2
                   COMMON /AAAAMP/AAMP(2000,2,3,2),BBMP(300,2,3,2),ABMP(300,2,3,2)
                                                                                                                      00085
                                                                                                                                        AMPO(J,JJ)=0.
  00020
                                                                                                                      00086
                                                                                                                                   810 CONTINUE
                  1,BAMP(300,2,3,2)
 00021
                  COMMON/SIG/SIGMA(4), SHERM(4,2)
                                                                                                                      00087
                                                                                                                                       FFF=0.
                                                                                                                      00088
                                                                                                                                       ENERGY(1)=ENERG
ENERGY(2)=ENERG-6.703
 00022
                   COMMON/FFSC/FSC(2.3.2)
                                                                                                                      00089
 00023
                  DIMENSION HI (360)
 00024
                                                                                                                      00090
                                                                                                                                       WRITE(6.800) ENERG
                  DIMENSION SIGMAA (360,6)
 00025
                                                                                                                                  800 FORMAT(1H1,//////20x.21H ***** NYUSHA ENERGY=,F10.1,6H *****)
DO 5150 J=1,NPP
                  DIMENSION SHERMM(360,4)
                DIMENSION FRE(2),FIM(2),GRE(2),GIM(2)
ABTAN(1,J) I,L OR -L-1,, J,ELASTIC OR INELASTIC
WAVEFU (1,J,K) I,STATE,,J,ATAMA OR KATA NOKEISU
                                                                                                                      00092
 00026
                                                                                                                      00093
                                                                                                                                       DO 5150 JJ=1.2
                                                                                                                      00094
                                                                                                                                       DO 5150 JJJ=1,2
               VPOT(I,J) J, ELASTIC OR INELASTIC
RK=RADIUS*(WAVE NUMBER), KR=PHYSE NUMBER
                                                                                                                     00095
                                                                                                                                       TANDL(J,JJ,JJJ)=0.
                                                                                                                      00096
                                                                                                                                       SINDL(J,JJ,JJJ)=0.
                                                                                                                      00097
              PHAT(I,J,K) I,L OR -L-1, J,KEISU, K, ELASTIC OR INELASTIC
PHAT(I,J,K,M) I,L,J,L OR -L-1 OF ELASTIC, K, PLUS OR MINUS SIGNS OF
INELASTIC, M, ABSOLUTE MAGRITUDE OF L OF INELASTIC
PHATIAT.
               VOTENTIAL NO TENKAIKEISU
                                                                                                                                       COSDL(J,JJ,JJJ)=1.
                                                                                                                      00098
                                                                                                                                       SCSQ(J,JJ,JJJ)=1.
                                                                                                                      00099
                                                                                                                                 5150 CONTINUE
                                                                                                                      00100
                                                                                                                                       DO 5200 Jal 2
              PHAII(I,J,K), AMPI(I,J,K) KIOKU SARETA INELATIC NO WAVE FUNCTION 1, -1, J,NNE OR OLD ONE
                                                                                                                      00101
                                                                                                                                       ENERGY(J)=ENERGY(J)/511008.+1.
                                                                                                                                       FK(J)=(ENERGY(J)*ENERGY(J)-1.)**.5
                                                                                                                      00102
              TAMDLD(1,3,K) JAL OR -L-1,1K, ELASTIC OR INELASTIC AAMP(1,3,K,L) J,(L,L+1) OR (L,L-1), K MAGNETIC UUANTUM NUMBER, ,L,R MAGNARY PART
                                                                                                                      00103
                                                                                                                                       RK(J)=FK(J)*RADIUS(5)
                                                                                                                                 5200 CONTÍNUE
                                                                                                                     00104
                                                                                                                     00105
                                                                                                                                       CALL BESSEL(NPP)
                                                                                                                      00106
                                                                                                                                  WRITE(6,900)RK
900 FORMAT(///13H HASU*RADIUS=2E15.5)
                                                                                                                      00107
 00027
                  NPN=2000
                                                                                                                      00108
                                                                                                                                  950 FORMAT (30H KEISANSARETA BESSEL NO JISU=,2115)
                                                                                                                                      WRITE(6,950)KR
WRITE(6,1000)((FJ(II,JJ),II=1,5),JJ=1,2)
WRITE(6,1000)((FNEU(II,JJ),II=1,5),JJ=1,2)
 00028
                                                                                                                      00109
                  NPP=300
 00029
                  NSEK=10000
                                                                                                                     00110
                  READ(5,100)RADIUS
                                                                                                                      00111
 00030
 00031
              100 FORMAT(6F10.2)
                                                                                                                     00112
                                                                                                                                 1000 FORMAT(/5E15.5)
                                                                                                                      00113
                                                                                                                                       DO 5250 LL=1.NPN
 00032
                  READ(5,200)HABA(2)
                                                                                                                     00114
                                                                                                                                       DO 5250 M=1.2
 00033
              200 FORMAT(F10.5)
                                                                                                                      00115
                                                                                                                                       DO 5250 J=1,2
 00034
                  READ(5,300)((POTE(I,J),I=1,2),J=1,3)
                                                                                                                     00116
 00035
              300 FORMAT (3E15,5)
                                                                                                                                       DO 5250 K=1.2
                                                                                                                     00117
                                                                                                                                       FMATRX(LL,M,J,K)=0.
 00036
                  READ(5,400)(((WAVEFU(1,J,K),J=1,2),K=1,2),T=1,3)
                                                                                                                     00118
 00037
              400 FORMAT(4E15.5)
                                                                                                                                 5250 CONTINUE
                                                                                                                                       READ(5,703)KLUNG,KTAE,KANKAK
 00038
                  READ(5,701)IP.DEL
                                                                                                                     00119
                                                                                                                     00120
              701 FORMAT(110,E10.1)
 00039
                                                                                                                                       FORMAT(3I1)
                                                                                                                     00121
 nnnhn
                  READ(5.500)NEN
                                                                                                                                       IF (KLUNG.EQ.1)GO TO 704
 00041
              500 FORMAT(110)
                                                                                                                     00122
                                                                                                                     00123
 00042
                                                                                                                                5300 CONTINUE
                  WRITE(6,102)
                                                                                                                     00124
              102 FORMAT(///////38H ***** YOMIKOMI DATA NOHAJIMARI *****)
 00043
                                                                                                                                       CALL DIRAC2(LL, FFF)
 00044
                                                                                                                     00125
                                                                                                                                       WRITE(6,1200)LL.1
                  WRITE(6,702) IP. DEL
 00045
                                                                                                                     00126
              702 FORMAT(1HO, 13H PHASE LIMIT=, 110, 19H PHASE SHIFT LIMIT=, E10.1)
                                                                                                                                       WRITE(6,1210)
                                                                                                                     00127
 00046
                  WRITE (6,101)RADIUS
                                                                                                                                       WRITE(6,6300)
 00047
                                                                                                                     00128
                                                                                                                                6300 FORMAT(22X,2H 0,13X,2H 1,11X,2H 2,11x,2H 3,19X,2H 0,11X,2H 1,11X,2
              101 FORMAT(1HO,8H RADIUS =,6F10.2)
                                                                                                                                1H 2,1(x,2H 3)

1210 FORMAT(//16x,9(2H *),7X,2H L,7X,9(2H *),9X,9(2H *),5X,5H -L-1,4X,
 00048
                  WRITE(6,201)HABA (2)
                                                                                                                     00129
 00049
              201 FORMAT(1H, 17H SEKIBUN HABA(2)=,F10.5)
 00050
                                                                                                                                     19(2H *))
DO 1150 II=1,2
                  WRITE(6,301)
                                                                                                                     00130
00051
              301 FORMAT(1HO, 33H YOMIKIMARETA POTENTIAL NO KEISU=)
                                                                                                                                      DO 1150 1151,2
IP(11.EQ.2)GO TO 6000
WRITE(6,1100)((PHAI(JJ,KK,II),KK=1,4),JJ=1,2)
                                                                                                                     00131
00052
                  WRITE(6,300)POTE
 00053
                  WRITE(6,401)
                                                                                                                     00133
00054
              401 FORMAT (1HO, 36H YOMIKOKARETA 6S 6P NO WAVE FUNCTION)
                                                                                                                                      WRITE(6,1160)((AMPL(JJ,KK,II),KK=1,4),JJ=1,2)
00055
                  WRITE(6,400)WAVEFU
                                                                                                                     00135
00056
                  CALL POTENT (NSEK)
                                                                                                                     00136
                                                                                                                                6000 CONTINUE
00057
                  WRITE(6,610)((VPOT(1,J),I=100.NSEK,1000),J=1,2)
                                                                                                                     00137
00058
                                                                                                                                     WRITE(6,1110)((PHAI(JJ,KK,II),KK=1,4),JJ=1,2)
             WRITE(6.610)(VPOTEI(I), I=100, NSEK, 1000)
610 FORMAT(1H, 10X, 10E10.)
                                                                                                                     00138
00059
                                                                                                                                GO TO 6100
6200 CONTINUE
                                                                                                                     00139
00060
                  CALL DIRACI
                                                                                                                     00140
00061
                                                                                                                                1100 FORMAT(1HO, 15H ELASTIC PHAI=, 4E13.4,8X,4E#3.4)
00062
              650 FORMAT(////27H POTENTIAL*R=Z(R) NO TENKAL)
                                                                                                                    00141
                                                                                                                               1110 FORMAT(1H ,15HINELASTIC PHAI=,4E13.4,8X,4E13.4)
00063
                 WRITE(6,700)((ZBE(I,J),I=1,4),J=1,2)
                                                                                                                    00142
00064
              700 FORMAT (4E15.5)
```

```
1160 FORMAT(10X,6H AMPL=,4E13.4,8X,4E13.4)
00143
                                                                                                                                                                        LL2=LL2+1
                      WRITE(6,8000)
                        FORMAT(///5x,2x,9(2H *),4x,6H PHAIO,5X,10(2H *),10X,11(2H *),4X,
                                                                                                                                                  00214
00144
                                                                                                                                                                 5620 CONTINUE
                                                                                                                                                  00215
00145
                    15H AMPO,5X,12(2H *))
                                                                                                                                                                         DO 5600 K=1,2
                                                                                                                                                  00216
                                                                                                                                                                         ABTAN(K,J)=ABS(TANDL(LLI,K,J))
                      WRITE(6,8100)
                                                                                                                                                  00217
00146
              8100 FORMAT(14x,8H ELASTIC,20x,10H INELASTIC,30x,8H ELASTIC,20x,10H INE
                                                                                                                                                                 5600 CONTINUE
                                                                                                                                                  00218
00147
                                                                                                                                                                         AMTAN=1.
                    ILASTIC)
                                                                                                                                                  00219
                                                                                                                                                                         IF(LL.LT.0)GO TO 7002
                      WRITE(6,8200)
                                                                                                                                                                          \begin{array}{l} \mathtt{AMTAN=AMAX1} \left( \mathtt{ABTAN} (1,1), \mathtt{ABTAN} (1,2), \mathtt{ABTAN} (2,1), \mathtt{ABTAN} (2,2) \right) \end{array} 
              8200 FORMAT(2(8x,2H L,12x,5H -L-1,3x),10x,2(8x,2H L,12x,5H +L-1,3x))
00148
                                                                                                                                                  00220
                                                                                                                                                  00221
00149
                                                                                                                                                                         WRITE(6,5376)
                      ARITE(6,8300)
                                                                                                                                                  00222
00150
                                                                                                                                                                         WRITE(6,5375)
              8300 FORMAT (5H R=.1)
                      WRITE(6,1220)((PHAIO(K,J),K=1,2),J=1,2),((AMPO(K,J),K=1,2),J=1,2)
                                                                                                                                                  00223
00151
                                                                                                                                                                 5376 FORMAT(180)
00152
                                                                                                                                                  00224
                                                                                                                                                                 5375 FORMAT(15X,8H (L,L+1),6X,11H (-L-1,L+1),4X,9H (L,-1-2),4X,12H (-L-
              1220 FORMAT(4E15.5,10X,4E15.5)
1200 FORMAT(1H1,////15(2H__),5X,4H LL=[10,20X,4]6,5X,15(2H__))
00153
                                                                                                                                                  00225
                                                                                                                                                                       11,-1-2), 9x,8H (L,L-1),5x,11H (-L-1,L-1),7x,7H (L,-L),8x,10H (-L-1
0015
                      CALL LUNGE(LL, NPN, NSEK)
00155
                                                                                                                                                                         WRITE(6,5370)(((FMATRX(LL+1,K,M,N),K=1,2),M=1,2),N=1,2)
                      LL2=LL+2
00156
                                                                                                                                                  00226
                                                                                                                                                                 5370 FORMAT(1H ,8H FMATRX=,4E15.5,5X,4E15.5)
                      LL1=LL+1
0015.7
                                                                                                                                                  00227
00158
                      JJJ=1
                                                                                                                                                                         LL11=LL+1
                                                                                                                                                  00228
                                                                                                                                                                LL22=LL2
WRITE(6,5381)(SINDL(LL11,K,1),K=1,2),(SINDL(LL22,K,2),K=1,2)
WRITE(6,5382)(COSDL(LL11,K,1),K=1,2),(COSDL(LL22,K,2),K=1,2)
WRITE(6,5380)(TANSL(LL11,K,1),K=1,2),(TANDL(LL22,K,2),K=1,2)
WRITE(6,5386)(SCSQ(LL11,K,1),K=1,2),(SCSQ(LL22,K,2),K=1,2)
5380 FORMAT(1H0,8H TANDL= ,10H (ELASTIC),2E15,5,12H (INELASTIC),2E15,5)
5381 FORMAT(1H0,8H SINDL= ,10H (ELASTIC),2E15,5,12H (INELASTIC),2E15,5)
5386 FORMAT(1H0,8H COSDL= ,10H (ELASTIC),2E15,5,12H (INELASTIC),2E15,5)
5386 FORMAT(1H0,8H COSDL= ,10H (ELASTIC),2E15,5,12H (INELASTIC),2E15,5)
60 TO 7003
00159
                                                                                                                                                                         1122=11+3
                                                                                                                                                  00229
                      1F(LL)5450,5320,5310
00160
                                                                                                                                                  00230
00161
              5450 CONTINUE
                                                                                                                                                  00231
00162
                      JJJJ=2
                                                                                                                                                  00232
00163
                      KKK = 2
                                                                                                                                                  00233
                      GO TO 5310
00164
                                                                                                                                                  00234
               5320 CONTINUE
00165
                                                                                                                                                  00235
00166
                      JJJJ=2
                                                                                                                                                  00236
00167
                      J = 1
                                                                                                                                                  00237
                      K=2
00168
                      \underset{\mathsf{TANU}=\mathsf{FK}(\mathtt{J})*\mathsf{FJ}(\mathtt{LL}^2,\mathtt{J})-\mathsf{FJ}(\mathtt{LL}^1,\mathtt{J})*((\mathtt{ENERGY}(\mathtt{J})+1,)*\mathsf{TAN}(\mathtt{PHALO}(\mathtt{K},\mathtt{J}))+
                                                                                                                                                                         GO TO 7003
                                                                                                                                                  00238
00169
                    1(1.+FLDAT(L(1,J)+L(K,J)))/RADIUS(5))
TANL=FK(J)*FNEU(LL2,J)-FNEU(LL1,J)*((ENERGY(J)+1.)*TAN(PHAIO(K,J))
                                                                                                                                                                 7002 CONTINUE
                                                                                                                                                  00239
                                                                                                                                                                         WRITE(6,7004)(SINDL(LL+2,K,2),K=1,2)
WRITE(6,7005)(COSDL(LL+2,K,2),K=1,2)
                                                                                                                                                  00240
00170
                                                                                                                                                  00241
                     1+(1.+FLOAT(L(1,J)+L(K,J)))/RADIUS(5))
                                                                                                                                                                 WRITE(0,700) (COSDL(LL+*,N,2),=1,2)
WRITE(0,700) (TAMDL(LL+2,K,2),K=1,2)
WRITE(0,7007) (SCSQ(LL+2,K,2),K=1,2)
WRITE(0,7007) (SCSQ(LL+2,K,2),K=1,2)
7004 FORMAT(1H0,RH COSDL= ,12H (INELASTIC),2E15.5)
7005 FORMAT(1H0,RH COSDL= ,12H (INELASTIC),2E15.5)
7007 FORMAT(1H0,RH SCSQ= ,12H (INELASTIC),2E15.5)
                                                                                                                                                  00242
                       \begin{array}{l} \texttt{TANDL}\{ \underbrace{\texttt{LL1}, \texttt{K}, \texttt{J}} \} = \texttt{TANU}/\texttt{TANL} \\ \texttt{SINDL}\{ \underbrace{\texttt{LL1}, \texttt{K}, \texttt{J}} \} = \texttt{TANU} + \texttt{EXP}(\texttt{AMPO}(\texttt{K}, \texttt{J})) \\ *\texttt{COS}(\texttt{PHAIO}(\texttt{K}, \texttt{J}))/\texttt{RADIUS}(5) \end{array} 
00171
                                                                                                                                                  00243
00172
                      SINDL(LL ,K,J)=SINDL(LL1,K,J)/(FJ(LL2,J)*FNEU(LL1,J)-FJ(LL1,J)
                                                                                                                                                  00244
00173
                                                                                                                                                  00245
                     I*FNEU(LL2,J))/FK(J)
                    \label{eq:cost} $$ \frac{(LL,K,J)+TANL+EXP(AMPO(K,J))+COS(PHAIO(K,J))}{COSDL(LLL,K,J)+COSL(LLL,K,J)+COSL(LLL,J)+FNEU(LLL,J)-FJ(LLL,J)}{L+FNEU(LL_2,J))+FK(J)} $$
                                                                                                                                                  00246
00174
                                                                                                                                                  00257
00175
                                                                                                                                                  00248
                                                                                                                                                                 7003 CONTINUE
                                                                                                                                                                          IF(LL.LT.0)GO TO 7001
                      SINDL(LILK, J)=-SINDL(LILK, J)
COSDL(LLL, K, J)=-COSDL(LILK, J)
                                                                                                                                                  00 249
00176
                                                                                                                                                                         LL11=LL+1
                                                                                                                                                  00250
00177
                                                                                                                                                                         DO 5383 J=1,2
                                                                                                                                                  00251
                       SCSQ(LL1,K,J)=(SINDL(LL1,K,J)**2 +COSDL(LL1,K,J)**2 )**.5
00178
                                                                                                                                                                         IF(J.EQ.2)LL11=LL+2
                                                                                                                                                  00252
                      IF(SCSQ(LL1,K,J),EQ..O)SCSQ(LL1,K,J)=1.
COSDL(LL1,K,J)=COSDL(LL1,K,J)/SCSQ(LL1,K,J)
SINDL(LL1,K,J)=SINDL(LL1,K,J)/SCSQ(LL1,K,J)
                                                                                                                                                                         no 5383 K=1.2
00180
                                                                                                                                                  00253
                                                                                                                                                                         FUNC(K,J,1)=EXP(AMPO(K,J))*COS(PHAIO(K,J))/RADIUS(5)/SCSQ(LL11,K,J
00181
                                                                                                                                                  00254
00182
                      GO TO 5310
00183
              5310 CONTINUE
                                                                                                                                                                         FUNC(K,J,2)= KJ(LL11,J)*COSDL(LL11,K,J)-FNEU(LL11,J)*SINDL(LL11,K.
                                                                                                                                                  00255
00184
                       DO 5500 J=JJJ,2
                                                                                                                                                                        1.1)
00185
                       IF(J.EQ.2)GO TO 5410
                                                                                                                                                  00256
                                                                                                                                                                 5383 CONTINUE
00186
                       GO TO 5420
                                                                                                                                                                         WRITE(6,5385)
                                                                                                                                                  00257
00187
               5410 CONTINUE
                                                                                                                                                  00258
                                                                                                                                                                 5385 FORMAT(1HO, 32H WAVE FUNCTION NO TSUNAGARI GUAL)
00188
                       LL1=LL2
                                                                                                                                                                         WRITE(6,5384)(((FUNC(K,J,JJJ),JJJ=1,2),K=1,2),J=1,2)
                                                                                                                                                  00259
00189
                       LL2=LL2+1
                                                                                                                                                                 5384 FORMAT(//8E15.5)
                                                                                                                                                  00260
               5420 CONTINUE
00190
                                                                                                                                                  00261
                                                                                                                                                                  7001 CONTINUE
                       DO 5400 K=KKK,2
00191
                                                                                                                                                  00262
                                                                                                                                                                         IF(LL.GE.IP)GO TO 7000
                       TANU=FK(J)*FJ(LL2,J)-FJ(LL1,J)*((ENERGY(J)+1.)*TAN(PHAIO(K,J))+
00192
                                                                                                                                                  00263
                                                                                                                                                                         LL=LL+1
                      1(1.+FLOAT(L(1,J)+L(K,J))/RADIUS(5))
                                                                                                                                                  00264
                                                                                                                                                                         IF(AMTAN,GE,DEL )GO TO 5300
                    Al-TROWLEL, JFELLA J JFARULUSES; J

TANL=FK(J) *PRUE(LL; J) *FREU(LL; J) *(ENERGY (J)+1.)*TAN(PHAIO(K,J))

1+(1.*FLOAT(L(1,J)+L(K,J)))/KADIUS(5))

TANDL(LL1, K, J)=TANU*EXP(AMPO(K,J))*COS(PHAIO(K,J))/RADIUS(5)

SINDL(LL1, K, J)=TANU*EXP(AMPO(K,J))*FO(LL2, J)*FREU(LL1, J)-FJ(LL1, J)
00193
                                                                                                                                                  00265
                                                                                                                                                                         GO TO 7100
                                                                                                                                                  00266
                                                                                                                                                                 7000 CONTINUE
00194
                                                                                                                                                  00267
                                                                                                                                                                         1.1.=1.1.+1
00195
                                                                                                                                                  00268
                                                                                                                                                                         WRITE(6,7200)
00196
                                                                                                                                                  00269
                                                                                                                                                                  7200 FORMAT(////35H ***** CAUTION ***** PHAISE IS OVER)
                      1*FNEU(LL2,J))/FK(J)
                                                                                                                                                  00270
                                                                                                                                                                 7100 CONTINUE
00197
                      COSDL(LL1,K,J)=TANL*EXP(AMPO(K,J))*COS(PHAIO(K,J))/RADIUS(5)
                                                                                                                                                                         WRITE(6,7300)
                      COSDL(LL1,K,J)=COSDL(LL1,K,J)/(FJ(LL2,J)*FNEU(LL1,J)-FJ(LL1,J)
00198
                                                                                                                                                  00271
                                                                                                                                                                 7300 FORMAT(25(2H *),19H PHAISE SHIFT OWAR1,25(2H *))
                    COSDL(LLI,K,J)=COSDL(LLI,K,J)/(FJ(LL2,J)*FNEU(LLI,J)-FJ(LI

+FNEU(LLI,K,J)=CSINDL(LLI,K,J)

COSDL(LLI,K,J)=CSINDL(LLI,K,J)

SCSQ(LLI,K,J)=(SINDL(LLI,K,J)**2

F(SCSQ(LLI,K,J)=(SINDL(LLI,K,J)+*2

SINDL(LLI,K,J)=SINDL(LLI,K,J)/

SCSQ(LLI,K,J)=SINDL(LLI,K,J)/

SCSQ(LLI,K,J)=SINDL(LLI,K,J)/

SCSQ(LLI,K,J)
                                                                                                                                                  00272
                                                                                                                                                                         DO 5000 Jal, LL
00199
                                                                                                                                                  00274
00200
                                                                                                                                                  00275
                                                                                                                                                                        1F(J.EQ.1)NN=1
DO 5000 N=1,NN
00201
                                                                                                                                                  00276
00202
                                                                                                                                                  00277
                                                                                                                                                                          J1=J+1
00203
                                                                                                                                                  00278
                                                                                                                                                                         IF(N,EQ,1)JI=J-1
00204
                      COSDL(LL1,K,J)=COSDL(LL1,K,J)/ SCSQ(LL1,K,J)
                                                                                                                                                  00279
                                                                                                                                                                         DO 5000 M=1,2
00205
                5400 CONTINUE
                                                                                                                                                  00280
                                                                                                                                                                         DO 5000 K=1,2
00206
                                                                                                                                                  00281
                5500 CONTINUE
                                                                                                                                                                         FMATRX(J,K,M,N) = FMATRX(J,K,M,N)/SCSQ(J,K,I)/SCSQ(JI,M,2)
00207
                                                                                                                                                  00282
                                                                                                                                                                  5000 CONTINUE
                      DO 5600 J=1,2
                                                                                                                                                  00283
00208
                                                                                                                                                                         WRITE(6,5371) RADIUS(5)
                      LL1=LL+1
                                                                                                                                                                 5371 FORMAT(1H1,///10x,3H R=,F10.1,10x,25H DE NORMALIZE SARETA ATAI)
00209
                                                                                                                                                  00285
                      LL2=LL+2
00210
                                                                                                                                                  00285
                                                                                                                                                                         WRITE(6,5375)
                      IF(J.EQ.2)GO TO 5610
00211
                                                                                                                                                  00286
                                                                                                                                                                         \begin{array}{l} \text{KHITE}(6,5373) \\ \text{WRITE}(6,5372) (J,(((\text{FMATRX}(J,K,M,X)K=1,2),M=1,2),X=1,2),J=1,LL) \end{array} 
                      GO TO 5620
                                                                                                                                                  00287
00212
                5610 CONTINUE
                                                                                                                                                  00288
                                                                                                                                                                 5373 FORMAT(III ,8H FMATRX=)
5372 FORMAT(IH ,18,4E15.5,5x,4E15.5)
00213
                      1.11 \pm 112
                                                                                                                                                  00289
                                                                                                                                                  00230
                                                                                                                                                                         1F(KATE, EQ. 1)GO TO 707
                                                                                                                                                  00291
```

00369

IL(J,1,JJ)-SINDL(J,2,JJ)*COSDL(J,2,JJ)*ASSLEG(J,2)

```
GTM(JJ)=GTM(JJ)+2.*((AL+1.)*AL/(2.*AL+1.))**.5*(SINDL(J,1,JJ)**2-S
IINDL(J,2,JJ)**2)*ASSLEG(J,2)
                   CALL TAE(LL, NPN, NPP)
00292
                                                                                                                          00370
                   GO TO 707
00293
             704 CONTINUE
                                                                                                                                            CONTINUE
SIGMAN(K,JJ+h)=FRE[JJ)**2+FIM(JJ)**2+GRE(JJ)**2+GIM(JJ)**2
SHERMM(K,JJ+h)=2.*(FRE[JJ)*CIM(JJ)-FIM(JJ)*GRE[JJ))/SIGMAA(K,JJ+h)
SIGMAA(K,JJ+h)=SIGMAA(K,JJ+h)*3,14159265h/FK(JJ)**2
SIGMAA(K,JJ+h)=SIGMAA(K,JJ+h)*5,3249E-05
00294
                                                                                                                                      4000 CONTINUE
                                                                                                                          00371
             READ(5,705)LL,LK
705 FORMAT(2110)
00295
                                                                                                                          00372
                 5 FORMAT(2110)

READ(5.5366) ((((FMATRX(J,K,M,N),K=1,2),M=1,2),N=1,2),J=1,LK)

READ(5.5366) ((FMATRX(J,1,1,N),N=1,2),J=1,KL,LL)

READ(5.5366) ((TMATRX(J,1,1,N),N=1,2),J=1,Z),J=1,LK)

READ(5.5366) (((COSDL(J,K,M),K=1,2),M=1,2),J=1,LK)

READ(5.5366) (((STKDL(J,K,M),K=1,2),M=1,2),J=1,LK)

DO 706 J=LK+1,LL
00296
                                                                                                                          00373
00297
                                                                                                                          00374
00298
                                                                                                                          00375
00299
                                                                                                                          00376
                                                                                                                                      WRITE(6,9/00)AK,(((FSC(II,JJ,KK),II=1,2),KK=1,2),JJ=1,3)
9100 FORMAT(1H,F10,1,3(2E10,2,2X,2E10,2))
00300
                                                                                                                          00377
00301
                                                                                                                          00378
00302
                                                                                                                                      9200 CONTINUE
                                                                                                                          00379
                  DO 708 K=1,2
                                                                                                                                             WRITE(6,4450)
00303
                                                                                                                          00380
                   DO 707 M=1,2
00304
                                                                                                                                      4450 FORMAT(1H1)
                                                                                                                          00381
                   DO 708 N=1.2
00305
                                                                                                                                             WRITE(6,4400)
                                                                                                                          00382
                                                                                                                                      4400 FORMAT(2X,5H KAKU, 3X, 18(2H *),6H SIGMA,17(2H *),5X,8(2H *),7H SHER
                   FMATRX(J,K,M,N)=FMATRX(J,1,1,N)
00306
                                                                                                                          00383
             708 CONTINUE
00307
                                                                                                                                           1MA,7(2H *))
A1A=8,7266463E-03*FLOAT(KANKAK)
                   FMATRX(LK+1,1,1,2)=-FMATRX(LK+1,1,1,2)
00308
                                                                                                                          00384
                   FMATRX(LK+1,2,1,2)=-FMATRX(LK+1,2,1,2)
FMATRX(LK+2,1,1,2)=-FMATRX(LK+2,1,1,2)
00309
                                                                                                                          00385
                                                                                                                                             S1GT01=0.
00310
                                                                                                                          00386
                                                                                                                                             SIGTO2=0.
                   FMATRX(LL+2,2,1,2)=-FMATRX(LK+2,2,1,2)
00311
                                                                                                                          00387
                                                                                                                                             sigto3=0.
00312
                   GO TO 706
                                                                                                                                             SIGTO4=0.
              707 CONTINUE
00313
                                                                                                                          00389
                                                                                                                                             DO 4300 K=KANKAK, 360, KANKAK
00314
                   T111=1
                                                                                                                          00390
                                                                                                                                             AK=F1.OAT(K)*.5
AK1=AK*1.745329252E=02
                   I222=0
00315
                                                                                                                          00391
                   WRITE(7,5362)ENERG
00316
                                                                                                                                             AK1=SIN(AK1)
                                                                                                                          00392
00317
            5362 FORMAT(F10,1)
                                                                                                                                             KIK=MOD(K,10)
                                                                                                                          00393
00318
                   WRITE(7,5363)1111,1222
                                                                                                                                            IF(KIK.EQ.1)GO TO 4401
GO TO 4402
                                                                                                                          00394
00319
            5363 FORMAT(211)
                                                                                                                          00395
00320
                   WRITE(7,5361)LL,LK
                                                                                                                          00396
                                                                                                                                       4401 CONTINUE
           00321
                                                                                                                          00397
                                                                                                                                            WRITE(6,4403)
00322
                                                                                                                          00398
                                                                                                                                      4403 FORMAT(1HO,5(2H ~))
00323
                                                                                                                          00399
                                                                                                                                      4402 CONTINUE
00324
                                                                                                                          00500
                                                                                                                                      WRITE(6,4200)AK,(SIGMAA(K,J),J=1,6),(SHERMM(K,J),J=1,4)
4200 FORMAT(F6,1,6212.4,5X,4212.4)
00325
                                                                                                                          00401
                   WRITE(7,5360)(((SINDL(J,K,M),K=1,2),M=1,2),J=1,LK)
00326
                                                                                                                          00402
                                                                                                                                             SIGTO!=SIGTO!+SIGMAA(K.1)*AKI
00327
              204 CONTINUE
                                                                                                                          00463
                                                                                                                                             SIGTO2=SIGTO2+SIGMAA(K,2)*AK1
00328
                   WRITE(6,5371)RADIUS(6)
                                                                                                                                             SIGTO3=SIGTO3+SIGMAA(K,3)*AK1
                                                                                                                          00404
00329
                   WRITE(6,5375)
                                                                                                                                      1300 CONTINUE
SIGTO1=SIGTO1*A1A*6.283185307
                                                                                                                          00405
                   WRITE(6,5372)U,(((FMATRX(J,K,M,N),K=1,2),M=1,2),N=1,2),J=1,LK)
WRITE(6,5374)U, (FMATRX(J,1,1,N),N=1,2)J=LK+1,LL)
00330
                                                                                                                          00406
                                                                                                                                            SIGT02=SIGT02*A1A*6.283185307
SIGT03=SIGT03*A1A*6.283185307
00331
                                                                                                                          00407
00332
            5374 FORMAT(1H 3(14,2E15,5.6x))
                                                                                                                          00/08
                   WRITE(6.5364)
                                                                                                                          00409
                                                                                                                                             SIGTO4=SIGTO1+SIGTO2+SIGTO3
00333
                                                                                                                                      4404 FORMAT(1HO, 20H TOTAL CROSS SECTION, 4E20.3)
             5364 FORMAT(7H TANDL=)
00334
                                                                                                                          00410
                   WRITE(6,5365)(J,((TANDL(J,K,M),K=1,2),M=1,2),J=1,LK+2)
                                                                                                                                            WRITE(6,4404)SIGTO1,SIGTO2,SIGTO3,SIGTO4
DATA BLANK,SIG,HI1,KYO,ZERO/1H,1H,1H*,1H0,1HI/
00335
                                                                                                                          00411
00336
                   WRITE(6,5366
                                                                                                                          00512
                   WRITE(6,5365)(J,((COSDL(J,K,M),K=1,2),M=1,2),J=1,LK+2)
                                                                                                                                            WRITE(6,4450)
00337
                                                                                                                          00413
00338
                   WRITE (6,5367
                                                                                                                                            DO 4410 K=10,180,2
                                                                                                                          00444
 00339
                   WRITE (6,5365) (J, ((SINDL(J,K,M),K=1,2),M=1,2),J=1,LK+2)
                                                                                                                                            K1=2*K
                                                                                                                          00415
00340
             5366 FORMAT(7H COSDL≈)
                                                                                                                          00416
                                                                                                                                            SIG1=SIGMAA(K1.5)/(SIGMAA(360.5)*20.
00341
             5367 FORMAT (7H SINDL=)
5365 FORMAT (2(15,4E15.5))
                                                                                                                          00417
                                                                                                                                             NSIGI=TNT(SIGI)
                                                                                                                                             IF(NSIG1.GT,120)NSIG1=120
 00342
                                                                                                                          00418
00343
             5360 FORMAT(4E15.9)
                                                                                                                          00419
                                                                                                                                            HI2=SIGMAA(K1,4)/SIGMAA(360,4)*20.
SHI2=INT(SHERMM(K1,4)*25,+101.)
 00344
                   CALL NAO(LL, LK, NPN, NPP)
                                                                                                                          00420
00345
                   WRITE(6,8900)
                                                                                                                          00421
                                                                                                                                             NHII=INT(HI2)
             8900 FORMAT(1H1)
                                                                                                                                             IF(NHI1.GT.120)NHJ1=120
00346
                                                                                                                          00422
00347
                                                                                                                          00423
                                                                                                                                            NSHE1=INT(SHERMM(K1,2)*25.+101.)
NSHE1=INT(SHERMM(K1,2)*25.+101.)
                   DO 9200 K=KANKAK, 360, KANKAK
 00348
                                                                                                                          00424
                   AK=FLOAT(K)*.5
00349
                                                                                                                          00325
                                                                                                                                            DO 3411 Jel.121
                   CALL SPHERI (K, LL, NPN)
 00350
                   CALL RET(LL, LK, NPN, NPP)
                                                                                                                          00426
                                                                                                                                            GRAPH(J)=BLANK
                   DO 9201 J=1.4
                                                                                                                                      4411 CONTINUE
 00351
 00352
                   SIGMAA(K,J)=SIGMA(J)
                                                                                                                          00428
                                                                                                                                            GRAPH(1)=ZERO
 00353
             9201 CONTINUE
                                                                                                                          00429
                                                                                                                                             GRAPH(81)=KYO
 00354
                   SHERMM(K.1)=SHERM(4.2)
                                                                                                                          00430
                                                                                                                                             GRAPH (101) = ZERO
 00355
                   SHERMM(K,4)=SHERM(4,1)
                                                                                                                          notation.
                                                                                                                                             WRITE (6,4412)K, GRAPH, K
00356
                   FRE(1)=.0
                                                                                                                          000100
                                                                                                                                            GRAPH(NSIGN)=SIG
                                                                                                                          00533
 00357
                   FRE(2)=.0
                                                                                                                                            GRAPH(NHII)=HII
 00358
                                                                                                                          00434
                   FIM(1)=.0
                                                                                                                                             GRAPH(NH12)=KVO
 00359
                   F1M(2)≈.0
GRE(1)≈.0
                                                                                                                          00435
                                                                                                                                            WRITE(6,3513)GRAPH
 00360
                                                                                                                          00436
                                                                                                                                            GRAPH(NSHFT)=SIG
00361
                   GRE(2)=.0
                                                                                                                          00537
                                                                                                                                            GRADU(NSHF2)=HL1
 00362
                   GIM(1)=0.
                                                                                                                          00538
                                                                                                                                            WRITE(6,4413)GHADH
00363
                                                                                                                          00139
                   GIM(2)=.0
                                                                                                                                      4513 FORMAT(1H*,6X,121A1)
00364
                   DO 4100 JJ=1.2
                                                                                                                          00440
                                                                                                                                      4412 FORMAT(IH ,14,2x,121a1,74)
00365
                   DO 4000 J=1,1X
                                                                                                                          00441
                                                                                                                                      1410 CONTINUE
 00366
                   AL=FLOAT(J -1)
                                                                                                                          00442
                                                                                                                                       600 CONTINUE
                   FRE(JJ)=FRE(JJ)+(2.*AL+1.)**(-.5)*2.*(AL*SINDL(J,1,JJ)*COSDL(J,1,J
00367
                                                                                                                         00443
                                                                                                                                            STOP
                  1J)+(AL+1.)*SINDL(J,2,JJ)*COSDL(J,2,JJ))*ASSLEG(J,1)
FIM(JJ)=FIM(JJ)+(2.*AL+1.)**(-.5)*2.*(AL*SINDL(J,1,JJ)**2
                                                                                                                         00444
                                                                                                                                            EXD
00368
                  1+(AL+1.)*SINDL(J,2,J)**2}**ASSLEG(J,1)
GRE(JJ)=GRE(JJ)+2.*((AL+1.)*AL/(2.*AL+1.))**.5*(SINDL(J,1,JJ)*COSD
```

00518

```
DO 400 I JJ, NSFK
                  SUBROUTINE SPHERI (K, LL, NPN)
                                                                                                                                   RADIAL(I)=RADIUS(5)+HABA(4)*FLOAT(I-JJ)
                                                                                                                 00519
00445
                                                                                                                 00520
                  COMMON/AASSLG/ASSLEG(2000,3)
00446
                                                                                                                 00521
                                                                                                                              400 CONTINUE
                                                                                                                                   RADIAL NO KETSAN OWARI GOKUROSAN
                  DIMENSION F(3.2)
00447
                  FK=FT.OAT(K)+,01745329252+.5
00448
                                                                                                                                    JJ=JJ-1
                                                                                                                 0052
                  CFK=COS(FK)
00449
                                                                                                                                    WRITE(6,1000)HABA
                                                                                                                 00523
                                                                                                                             1000 FORMAT(1HO.14H SEKIBUN HABA=,4F15.5)
                  SFK=SIN(FK)
00450
                                 ±0.2820947918
=0.4886025119*CFK
                                                                                                                 00524
                  ASSLEG(1.1)
00451
                                                                                                                                   WRITE(6,1100)KAISU
                                                                                                                             1100 FORMAT(1H ,15H SEKTBUN KAISU=,4115)
WRITE(6,1200)(RADTAL(1),1=100,NSEK,1000)
                                                                                                                 00525
                                 =0.3454941495*SFK
                                                                                                                 00526
                  ASSLEG(2,2)
00453
                  ASSLEG(3,1) =0.3153915653*(3,*CFK*CFK-1.)
                                                                                                                 00527
00454
                                                                                                                             1200 FORMAT(1HO, 3H R=,7x,12E10.2)
                  F(1,1)=4SSLEG(3,1)
                                                                                                                 00528
                                                                                                                                    DO 500 NN=1, NSEK
00455
                  ASSLEG(3.2) =0.772548404*SFK*CFK
                                                                                                                 00529
00456
                 ASSLEG(3,2) =0.772548404*SFK*CFK
F(2,1)=ASSLEG(3,2)
ASSLEG(3,3) =0.386274202*SFK*SFK
F(3,1)=ASSLEG(3,3)
                                                                                                                                    R=RADIAL(NN)
                                                                                                                 00530
                                                                                                                                   VPOT(NN,1)=0.
VPOT(NN,2)=0.
00457
00458
                                                                                                                 00532
00459
                                                                                                                                    VPOTEI(NN)=0.
                                                                                                                  00533
                  ASSLEG(4.1) =0.3731763326*CFK*(5.*CFK*CFK-3.)
00460
                                                                                                                                    DO 600 I=1,3
                                                                                                                 00534
                                                                                                                                    VPOT(NN,1)=VPOT(NN,1)-POTE(1,1)*EXP(-POTE(2,1)*R)
                  F(1,2)=ASSLEG(4,1)
00461
                                                                                                                 00535
                  ASSLEG(4,2) =.3231801841*SFK*(5.*CFK*CFK-1.)
00462
                                                                                                                  00536
                                                                                                                                    VPOT(NN.1)=VPOT(NN.1)/R
                  F(2,2)=ASSLEG(4,2)
00463
                                                                                                                 00537
                  ASSLEG(4,3) =1.021985476*CFK*SFK*SFK
00464
                                                                                                                                    no 700 I=1,2
                                                                                                                 00538
                  F(3,2)=ASSLEG(4,3)
DO 200 I=5,LL+2
00465
                                                                                                                                    DO 700 J=1,2
                                                                                                                 00539
                                                                                                                                    A1=WAVEFU(1,1,1)*WAVEFU(1,1,J)
                                                                                                                                    A2=WAVFU(1,2,I)=WAVFFU(1,2,J)

A2=WAVFU(1,2,I)=WAVFU(1,2,J)

VPOT(NN,2)=WPOT(NN,2)=A1/A2/A2*(2,/A2/B*(1,-EXF(-A2*R))-EXP(-A2*R)
00466
                                                                                                                  00540
                  FI=FLOAT(1)-2.
00467
                                                                                                                 00541
00468
                  DO 300 J=1,3
                                                                                                                 00542
                  FJ=-(FLOAT(J)-1.)
00469
                  ASSLEG(I.J) =((2.*FI+1.)*(2.*FI+3.)/(FI+FJ+1.)/(FT-FJ+1.))**.5*CF
00470
                                                                                                                  00543
                                                                                                                               700 CONTINUE
                                                                                                                                    VPOT(NN,2)=2.*VPOT(NN,2)
IZYO KITEIZYOTAI KARANO POTENTIAL
                 1K*F(J,2)-((2.*FI+3.)*(FI+FJ)*(FI-FJ)/(2.*FI-1.)/(FI+FJ+1.)/(FI+FJ+
                                                                                                                  00544
                21.))**0.5*F(J,1)
             300 CONTINUE
00471
                                                                                                                                    A1=WAVEFU(2,1,1)**2
                                                                                                                  00545
                                                                                                                                    42=WAVEFU(2,2,1)*2.
                                                                                                                  00546
                                                                                                                                    VPOT(NN,2)=VPOT(NN,2)-A1/A2/A2*(24./A2**3,*(1.-EXP(-A2*R))/R-EXP(-
00473
                  F(J,1)=F(J,2)
                                                                                                                  00547
00474
                  F(J,2)=ASSLEG(I,J)
                                                                                                                                   1A2*R)*(18./A2/A2+6./A2*H+R*R))
00475
             200 CONTINUE
                                                                                                                                    DO 800 T=1,2
                                                                                                                  00548
00476
                  RETURN
                                                                                                                                    Do 800 J=1,2
                                                                                                                  00549
                                                                                                                                    Al=WAVEFU(3,1,1)*WAVEFU(3,1,J)
00477
                  END
                                                                                                                  00550
                                                                                                                                    A2=WAVEFU(3,2,1)+WAVFU(3,2,3)
VPOT(NN,2)=VPOT(NN,2)-A1/A2/A2*(24./A2**3.*(1.-EXP(-A2*R))/R-EXP(-
                                                                                                                  00551
                                                                                                                  00552
                                                                                                                                   1A2*R)*(18./A2/A2+6./A2*R+R*R))
                                                                                                                  0055.3
                                                                                                                               800 CONTINUE
                                                                                                                                    Al=WAVEFU(2,1,1)*WAVEFU(2,1,2)
A2=WAVEFU(2,2,1)*WAVEFU(2,2,2)
                                                                                                                  00554
                                                                                                                 00555
                                                                                                                                    \begin{array}{l} {\tt VPOT(NN,2)=VPOT(NN,2)=2.*A1/42/42*(6./A2/A2*(1.-EXP(-A2*R))/R-EXP(1-A2*R)*(4./A2+R))} \\ \end{array} 
00478
                  SUBROUTINE POTENT(NSEK)
                 COMMON/WAVPOT/POTE(2,3), WAVEFII(3,2,2)
COMMON/RRADAL/RADTUS(6), RADIAT.(10000)/HHARA/HABA(4)
00479
                                                                                                                                    Al=WAVEFU(2,1,2)*WAVFFU(2,1,2)
A2=WAVEFU(2,2,2)*2
VPOT(NN,2)=VPOT(NN,2)-A1/A2/A2*(2./A2*(1.-EXP(-A2*R))/R-EXP(-A2*R)
                                                                                                                  00557
                 COMMON/KKAISU/K4ISU(4)
                                                                                                                 00558
00481
                 COMMON' VYPOTYPOT(10000,2), VPOTEI(10000)
HABA(1)=HABA(2)/WADIUS(2)
HABA(1)=HABA(2)/WADIUS(2))/HABA(1)
HABA(1)=ALOG(10, *RADIUS(2))/FLOAT(KAISU(1))
HABA(1)=ALOG(10, *RADIUS(2))/FLOAT(KAISU(1))
KAISU(1)=INTY((RADIUS(2))/FLOAT(KAISU(1))
00482
00483
                                                                                                                  00560
                                                                                                                                    VPOT(NN,2)=VPOT(NN,1)-VPOT(NN,2)
0048
                                                                                                                                                                     MATAMATA GOKUROSAN
                                                                                                                                    POT OF INELA
                                                                                                                                                       OWARI
00485
                                                                                                                  00561
                                                                                                                                    DO 900 I±1,2
00486
                                                                                                                  00562
                                                                                                                                    no 900 J=1,2
                 HABA(2)=(RADIUS(3)-RADIUS(2))/FLOAT(KAISU(2))
00487
                                                                                                                  00563
                                                                                                                                    A1=WAVEFU(1,1,1)*WAVEFU(3,1,J)
                 HABA(3)=2.*HABA(2)
00488
                                                                                                                  00564
                                                                                                                                    A2=WAVEFU(1,2,1)*WAVEFU(3,2,J)
                  KAISU(3)=INT(RADIUS(4)-RADIUS(3))/HABA(3))
00489
                                                                                                                  00565
                                                                                                                                   VPOTEI(NN)=VPOTEI(NN)+3.*A1/A2/A2*(8./A2**3.*(1.-EXP(-A2*R))/R/R-(18./A2/A2/R+4./A2 +R)*EXP(-A2*R))
00490
                  HABA(3)=(RADIUS(4)-RADIUS(3))/FLOAT(KAISU(3))
00491
                  HABA(4)=2.5*HABA(3)
KAISU(4)=INT((RADIUS(5)-RADIUS(4))/HABA(4))
                                                                                                                  00566
00492
                                                                                                                               900 CONTINUE
00493
00494
00495
                  HABA(4)=(RADIUS(5)-RADIUS(4))/FLOAT(KAISU(4))
DO 100 I=1,KAISU(1)
RADIAL(I)=0.1*EXP(HABA(1)*FLOAT(I))
                                                                                                                  00567
                                                                                                                                    VPOTEI (NN) = VPOTEI (NN) *1.5437488
                                                                                                                  00568
                                                                                                                                500 CONTINUE
                                                                                                                  00569
                                                                                                                                    WRITE(6,5000)((1,RADTAL(1),VPOTEI(1)),T=1,NSEK,10)
00496
             LOD CONTENTE
                                                                                                                                    FORMAT((4(17,2E13.4))
                                                                                                                  00570
00497
                  J=1+KAISU(1)
                                                                                                                  00571
                  JJ=KAISU(1)+KAISU(2)
                                                                                                                                    RETURN
00498
                                                                                                                  00572
                                                                                                                                    END
00499
                  DO 200 K=2.4
00500
                  DO 300 [=J.JJ
00501
                  RADIAL(I)=RADIUS(K)+HABA(K)*FLOAT(I-J+1)
             300 CONTINUE
00502
00503
                  J=JJ+1
00504
                  KK=K+1
00505
                  IF(KK,GE.5)GO TO 210
                                                                                                                  00573
                                                                                                                                    SUBROUTINE BESSEL(NPP)
00506
                  JJ=JJ+K4ISU(KK)
                                                                                                                  00574
00507
             200 CONTINUE
                                                                                                                                    COMMON/BES/FJ(300,2), FNEU(300,2), RK(2), KR(2)
                                                                                                                  00575
                                                                                                                                    DO 100 J=1,2
00508
             210 CONTINUE
                                                                                                                  00576
                                                                                                                                    R=RK(J)
00509
                  JJ=JJ+1
                                                                                                                                    FJO=SIN(R)/R
00510
                  IF(JJ.GE.NSFK)GO TO 2000
                                                                                                                  00577
                                                                                                                  00578
00511
                  GO TO 2100
                                                                                                                                    FJI=(SIN(R)/(R)-COS(R))/R
                                                                                                                  00579
                                                                                                                                    FNEU0=-COS(R)/R
FNEU1=-(COS(R)/R+SIN(R))/R
00512
            2000 CONTINUE
00513
                                                                                                                  00580
                  WRITF(6,2300)
00514
                                                                                                                  00581
                                                                                                                                    FJ(1,J)=FJO
                  WRITE(6,2200)
                                                                                                                  00582
00515
                                                                                                                                    FJ(2,J)=FJ1
                  WRITE(6.2300)
00516
           2200 FORMAT (29H SEKIBUN KAISU DIMENSION OVER)
                                                                                                                  00583
                                                                                                                                    FNEU(1,J)=FNEUO
           2300 FORMAT(1H ,50(2H**))
                                                                                                                  00584
00517
                                                                                                                                    FNEU(2,J)=FNEUI
           2100 CONTINUE
```

```
1*WAVEFU(2,1,1)*WAVEFU(2,1,2)*(WAVEFU(2,2,1)*WAVEFU(2,2,2))**(-3,)+2.25*MAVEFU(2,1,2)*WAVEFU(2,1,2)*WAVEFU(2,2,2)**(-2,)+ZHE(2,2)
ZBE(4,2)=ZBE(4,2)-WAVEFU(2,1,2)*WAVEFU(2,1,2)/6.
                                      KR(J)=INT(R)+50
00585
                                      KR(J)=MINO(KR(J),NPP)
00586
                                      KR2=KR(J)-1
                                                                                                                                                                                                                                                                                  DO 300 1=1,2
00587
                                                                                                                                                                                                                                            00653
                                      DO 200 KR1=3,KR2
                                                                                                                                                                                                                                                                               DU JOU JELL (2)-E. **MAVEFU(3,1,1)**MAVEFU(3,1,1)** (NAVEFU(3,2,1)**AVEFU(2,2)-EBE(2,2)-EBE(2,2)-**(-1,)-2.**MAVEFU(1,1,1)**MAVEFU(1,1,1)**(MAVEFU(1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(-1,2,1)**(
00588
                                                                                                                                                                                                                                            00655
                                      FKR1=KR1
00589
                                      FJ(KR1,J)=-FJO+(2.*FKR1-3.)*FJ1/R
                                                                                                                                                                                                                                            011155
                                      FNEU(KR1, J)=-FNEU0+(2.*FKR1-3.)*FNEU1/R
00590
                                                                                                                                                                                                                                                                                2WAVEFU(1,2,J))**(-2.)
00591
                                                                                                                                                                                                                                                                                 ZBE(4,2)=ZBE(4,2)+WAVEFU(1,1,1)*WAVEFU(1,1,J)/3.
                                      FJO=FJ1
                                                                                                                                                                                                                                            00656
                                      FJ1=FJ(KR1,J)
00593
                                                                                                                                                                                                                                                                         300 CONTINUE
                                                                                                                                                                                                                                            00657
                                      FNEUO=FNEU1
 00594
                                                                                                                                                                                                                                                                                 RETURN
                                                                                                                                                                                                                                            00658
                                      FNEU1=FNEU(KR1,J)
 00595
                                                                                                                                                                                                                                                                                  END
                                                                                                                                                                                                                                            00659
 00596
                            200 CONTINUE
                                      DO 300 KR1=KR(J),NPP
 00597
                                      FJ(KR1,J)=1.
 00598
                                      FNEU(KR1, J)=1.
 00599
                              300 CONTINUE
00500
                                                                                                                                                                                                                                                                                  SUBROUTINE DIRAC2(LL, FFF)
                                                                                                                                                                                                                                            00660
                                                                                                                                                                                                                                                                                  COMMON/PPHAI/PHAI(2,4,2), AMPL(2,4,2)
                             100 CONTINUE
                                                                                                                                                                                                                                            00661
 00602
                                      RETURN
                                                                                                                                                                                                                                                                                  COMMON/ZZB/ZBE(4,2)
                                                                                                                                                                                                                                            00662
 00603
                                                                                                                                                                                                                                                                                  COMMON/PPHATO/PHATO(2,2),AMPO(2,2
                                                                                                                                                                                                                                            00663
                                                                                                                                                                                                                                                                                  COMMON/LIL/L(2,2)/EENERG/ENERGY(2)
                                                                                                                                                                                                                                            00664
                                                                                                                                                                                                                                                                                  COMMON/HHABA/HABA(4)
                                                                                                                                                                                                                                            00665
                                                                                                                                                                                                                                                                                   I.(1,1)=LL
                                                                                                                                                                                                                                            00666
                                                                                                                                                                                                                                                                                  L(1,2)=LL+1
                                                                                                                                                                                                                                            00667
                                                                                                                                                                                                                                            00661
                                                                                                                                                                                                                                                                                  L(2,1)=-LL-1
                                                                                                                                                                                                                                            00669
                                                                                                                                                                                                                                                                                   L(2,2)=-LL-2
                                       SUBROUTINE BESELI(LL,I,NPP)
 00604
                                                                                                                                                                                                                                                                                  IF(LL) 100,150,200
                                       COMMON/BES/FJ(300,2),FNEU(300,2),RK(2),KR(2)
                                                                                                                                                                                                                                            00670
 00605
                                                                                                                                                                                                                                            00671
                                                                                                                                                                                                                                                                         100 L(1,2)=1
                                       DO 100 J=1,2
 00606
                                                                                                                                                                                                                                            00672
                                                                                                                                                                                                                                                                                  1(2,1)=1
 00607
                                        R=RK(J)
                                                                                                                                                                                                                                                                                  GO TO 200
                                                                                                                                                                                                                                            00673
 00608
                                       FJO=SIN(R)/R
                                                                                                                                                                                                                                                                        150 L(1,1)=+1
                                       FJ1 = (SIN(R)/(R) - COS(R))/R
                                                                                                                                                                                                                                            00675
 00609
                                                                                                                                                                                                                                            00675
                                                                                                                                                                                                                                                                                 GO TO 200
                                      FNEU0=-COS(R)/R
FNEU1=-(COS(R)/R+SIN(R))/R
 00610
                                                                                                                                                                                                                                                                        200 CONTINUE
                                                                                                                                                                                                                                            00676
 00611
                                                                                                                                                                                                                                                                                   DO 300 T=1.2
                                      FJ(1,J)=FJ0
FJ(2,J)=FJ1
                                                                                                                                                                                                                                            00677
 00612
                                                                                                                                                                                                                                            00678
                                                                                                                                                                                                                                                                                   DO 400 J=1.2
 00613
                                                                                                                                                                                                                                                                                   PHAI(I,1,J)=-ZBE(1,J)/FLOAT(L(I,J))
                                                                                                                                                                                                                                            00679
                                       FNEU(1,J)=FNEUO
 00614
                                       FNEU(2,J)=FNEU1
                                                                                                                                                                                                                                            00680
                                                                                                                                                                                                                                                                         400 CONTINUE
 00615
                                                                                                                                                                                                                                            00681
                                                                                                                                                                                                                                                                                   DO 300 J=1,2
 00616
                                       KR(J)=LL+3
                                                                                                                                                                                                                                                                                    PHAI(I,1,J)=ARSIN(PHAI(I,1,J))
                                                                                                                                                                                                                                            00682
 00617
                                       KR(J)=MINO(KR(J),NPP)
                                                                                                                                                                                                                                             00683
                                                                                                                                                                                                                                                                                   TF(PHAI(1,1,J)) 501,502,502
                                       KR2=KR(J)-1
 00618
                                                                                                                                                                                                                                                                        501 PHAI(I,1,J)=3.141592654-PHAI(I,1,J)
 00619
                                       DO 200 KR1=3.KR2
                                                                                                                                                                                                                                            00689
                                        FKR1=KR1
                                                                                                                                                                                                                                            00685
                                                                                                                                                                                                                                                                         502 CONTINUE
   00620
                                        FJ(KR1,J)=-FJO+(2.*FKR1-3.)*FJ1/R
                                                                                                                                                                                                                                            00686
                                                                                                                                                                                                                                                                                  PH1=PHAL(I,1,J)
  00621
                                        FNEU(KR1,J)=-FNEUO+(2.*FKR1-3.)*FNEU1/R
                                                                                                                                                                                                                                                                               \begin{split} & \text{Fils=IOAT(1,(1,J))} \\ & \text{PHAI(1,2,J)} = & \text{PNEN(Y,J)} + \text{ZBE(2,J)} - \text{COS(PH1)} / (1,-2,*\text{Fil}*\text{COS(PH1)}) \\ & \text{PHAI(1,3,J)} = 2,*\text{PHAI(1,2,J)} + \text{SNI(PH1)} * (1,-\text{Fil}*\text{PHAI(1,2,J)}) + \text{ZBE(3,J)} \\ & \text{PHAI(1,3,J)} = 2,*\text{PHAI(1,3,J)} / 2,* (1,-\text{Fil}*\text{COS(PH1)}) \\ & \text{PHAI(1,4,J)} = 2,*\text{PHAI(1,3,J)} + \text{SNI(PH1)} * (1,-2,3,*\text{Fil}*\text{PHAI(1,2,J)}) * 2,*\text{PHAI(1,4,J)} + \text{PHAI(1,4,J)} + \text{COS(PH1)} \\ & \text{PHAI(1,4,J)} = \text{PHAI(1,4,J)} + \text{COS(PH1)} * (1,-2,J,*\text{Fil}*\text{PHAI(1,2,J)}) * + \text{ZBE(1,J)} * \text{COS(PH1)} \\ & \text{AMPL(1,1,J)} = \text{AMPL(1,1,J)} = \text{AMPC(1,J)} + \text{SNI(1,3,J)} = \text{NN(1,1,J)} + \text{SNI(1,3,J)} + \text{NN(1,1,J)} = \text{SNI(1,3,J)} + \text{NN(1,1,J)} + \text{SNI(1,3,J)} = \text{NN(1,1,J)} + \text{SNI(1,3,J)} = \text{NN(1,1,J)} + \text{SNI(1,3,J)} = \text{NN(1,1,J)} + \text{SNI(1,3,J)} = \text{NN(1,1,J)} = \text{SNI(1,1,J)} = \text{NN(1,1,J)} = \text{NN(1
   00622
                                                                                                                                                                                                                                            00687
                                                                                                                                                                                                                                                                                  FLL=FLOAT(L(I,J))
   00623
                                         FJO=FJ1
                                                                                                                                                                                                                                            00688
   00624
                                         FJ1=FJ(KR1,J)
                                                                                                                                                                                                                                            00689
  00625
                                         ENERIO-ENEUL
                                                                                                                                                                                                                                            00690
                                        FNEU1=FNEU(KR1,J)
                                                                                                                                                                                                                                            00691
   00627
                              200 CONTINUE
   00628
                                        IF( I.GE. 3)GO TO 150
                                                                                                                                                                                                                                            00692
   00629
                                         DO 300 KR1=KR(J), NPP
                                                                                                                                                                                                                                            00693
                                        FNEU(KR1, J)=0.
                                                                                                                                                                                                                                             00694
   00630
                                        FJ(KR1,J)=0.
                                                                                                                                                                                                                                            00695
   00631
                              300 CONTINUE
                                                                                                                                                                                                                                            00696
   00632
                              150 CONTINUE
                                                                                                                                                                                                                                                                                 1.J)*SIN(PH1)
   00633
   00634
                              100 CONTINUE
                                                                                                                                                                                                                                            00697
                                                                                                                                                                                                                                                                         300 CONTINUE
                                                                                                                                                                                                                                           00698
                                                                                                                                                                                                                                                                                 DO 500 I=1,2
DO 500 J=1,2
PHAI (I,1,J)=PHAI (I,1,J)/2
   00635
                                        RETURN
                                                                                                                                                                                                                                            00699
   00636
                                                                                                                                                                                                                                            00700
                                                                                                                                                                                                                                            00701
                                                                                                                                                                                                                                                                                  PHAIO((1,j)=0.
                                                                                                                                                                                                                                            00702
                                                                                                                                                                                                                                                                         500 CONTINUE
                                                                                                                                                                                                                                            00703
                                                                                                                                                                                                                                                                                  DO 600 T=1,2
                                                                                                                                                                                                                                            00704
                                                                                                                                                                                                                                                                                  DO 600 J=1,2
                                                                                                                                                                                                                                            00705
                                                                                                                                                                                                                                                                                  DO 650 K=1.4
                                                                                                                                                                                                                                            00706
                                         SUBROUTINE DIRAC1
                                                                                                                                                                                                                                                                                   FK=FLOAT(K)
   00637
                                                                                                                                                                                                                                            00707
                                                                                                                                                                                                                                                                                   PHAIO(I,J)=PHAIO(I,J)+(.1*EXP(HABA(1)))**(FK-1.)*PHAI(I,K,J)
  00638
                                        COMMON/WAVPOT/POTE(2,3), WAVEFU(3,2,2)
                                                                                                                                                                                                                                            00708
  00639
                                        COMMON/ZZB/ZBE(4,2)
                                        DO 100 (=1,4
                                                                                                                                                                                                                                            00709
                                                                                                                                                                                                                                                                                \begin{array}{l} \text{AMPO(1,J)=AMPL(1,1,3)+AMPL(1,2,3)*ALOG(.1*EXP(HABA(1)))+AMPL(1,3,J)*1.*EXP(HABA(1))+AMPL(1,4,0)*.01*EXP(2.*HABA(1))} \end{array}
   00640
   00641
                                        DO 100 J=1.2
                                                                                                                                                                                                                                            00710
                                                                                                                                                                                                                                                                        600 CONTINUE
   00642
                                        ZBE(1,J)=0.
                                                                                                                                                                                                                                            00711
                              100 CONTINUE
                                                                                                                                                                                                                                                                                 RETURN
                                                                                                                                                                                                                                            00712
   00644
                                        DO 200 1=1,3
                                                                                                                                                                                                                                                                                 END
   00645
                                        DO 200 J=1.2
   00646
                                        ZBE(1,J)=ZBE(1,J)+POTE(1,1)
   00647
                                        ZBE(2,J)=ZBE(2,J)-POTE(1,I)*POTE(2,I)
   00648
                                        2BE(3,J)=2BE(3,J)+POTE(1,1)*POTE(2,1)*POTE(2,1)/2.
   00649
                                        ZBE(4,J)=ZBE(4,J)-POTE(1,I)*POTE(2,I)**3./6.
   00650
                                                                                                                                                                                                                                            00713
                                                                                                                                                                                                                                                                                  SUBROUTINE LUNGE(LL, NPN, NSEK)
                                        ZBE(2,2)=3./8.*WAVEFU(2,1,1)*WAVEFU(2,1,1)*WAVEFU(2,2,1)**(-4.)+4.
                                                                                                                                                                                                                                            00714
                                                                                                                                                                                                                                                                                 DIMENSION DELTA(4), DELAMP(4)
                                                                                                                                                                                                                                            00715
                                                                                                                                                                                                                                                                                 COMMON/HHABA/HANA(4)/KKATSU/KATSU(4)
                                                                                                                                                                                                                                            00716
                                                                                                                                                                                                                                                                                  COMMON/RRADAL/RADIUS(6), RADIAL(10000)/EENERG/ENERGY(2)
```

```
COMMON/MATRIX/FMATRX(2000,2,2,2)/VVPOT/VPOT(10000,2),VPOTEI(10000)
COMMON/PPHAI1/AMP1(2,2,10000)
 00718
                              COMMON/L1L/ L(2,2)/PPHAIO/PHAIO(2,2),AMPO(2,2)
 00719
 00720
                              LL1=LL+1
                              KKK#1
 00721
                             KATel
 00722
                              KAIS=KAISU(1)
 00723
                              HAB=HABA(1)
 00724
                      100 CONTINUE
 00725
                              DO 200 I=KAI, KAIS
00726
                              DO 300 J=1,2
 00727
                              DO 300 K#1,2
00728
                              FL=FLOAT(L(K,J))
00729
                              PHA=PHAIO(K,J)
00730
                              DELTA(1)=FL*SIN(2.*PHA)+RADIAL(I)*(-VPOT(I,J)+ENERGY(J)-COS(2.*PHA
00731
00732
                           00733
00734
                             DELTA(2)=HAB*DELTA(2)
                           DELTA(3)=FL*SIN(2.*PHA+DELTA(2))+(RADIAL(I)+RADIAL(I+1))/2.*((-VPO 1f(1,J)-VPOT(1+1,J))/2.+ENPPOV(J)-COS(2.*PHA+DELTA(2)))
00735
                             DELTA(3)=HAP*DELTA(3)
00736
                             DELTA(4)=FL*SIN(2.*(PHA+DELTA(3)))+RADIAL(I+1)*(-VPOT(I+1,J)+ENERG
00737
                            1Y(J)-COS(2.*(PHA+DELTA(3))))
00738
                              DELTA(4)=HAB*DELTA(4)
00739
                             PHATO(K.J)=PHATO(K.J)+(DELTA(1)+2.*(DELTA(2)+DELTA(3))+DELTA(4))/6
                            DELAMP(1)=-FL*COS(2.*PHA)-RADIAL(1)*SIN(2.*PHA)
DELAMP(2)=-FL*COS(2.*PHA+DELTA(1))-(RADIAL(1)+RADIAL(1+1))/2.-SIN(
00741
                           1 2.#PHA+DELTA(1))
                             DELAMP(3) = -FL*COS(2.*PHA+DELTA(2)) - (RADIAL(1)+RADIAL(1+1))/2.*SIN(
00742
                            1(2.*PHA+DELTA(2)))
00743
                             DELAMP(4)=-FL*COS(2.*(PHA+DELTA(3)))-RADIAL(I+1)*SIN(2.*(PHA+DELTA
00744
                            AMPO(K,J)=AMPC(K,J)+HAB*(DELAMP(1)+2.*(DELAMP(2)+DELAMP(3))+DELAMP
                          1(4))/6.
                     300 CONTINUE
00745
00746
                             IF(LL.LT.0)GO TO 270
                             DO 250 J=1,2
00747
                             DO 250 K=1,2
00748
                             IF(AMPO(K.1).LE.-170.)GO TO 251
00749
                           00750
00751
00752
                           1* VPOTEI(I)*EXP(AMPO(J,2)*COS(PHATO(J,2))*HAB*RADIAL(I)
 00753
                      251 CONTINUE
                      250 CONTINUE
 00754
                      270 CONTINUE
 00756
                              AMP1(1,2,1)=AMPM(1,1,1)
 00757
                              AMP1(2,2,1)=AMP1(2,1,1)
 00758
                              AMP1(1,1,1)=EXP(AMPO(1,2))*COS(
                                                                                                 PHAIO(1,2))/RADIAL(I)
PHAIO(2,2))/RADIAL(I)
 00759
                              AMP1(2,1,1)=EXP(AMPO(2,2))*COS(
 00760
                      200 CONTINUE
 00761
                              WRITE(6,1100)
 00762
                    1100
                                   FORMAT(5H R=15)
 00763
                             WRITE(6,1000)((PHAIO(I,J),I=1,2),J=1,2),((AMPO(I,J),I=1,2),J=1,2)
FORMAT(4E15.5,10X,4E15.5)
 00764
                    1000
                      210 CONTINUE
 00766
                              KKK2=KKK
00767
                              KKK=KKK+1
 00768
                              KAI=KAI+KAISU(KKK2)
 00769
                             KAIS=KAIS +KAISU(KKK)
 00770
                             HAR=HARA(KKK)
 00771
                             DO 500 I=KAI KAIS
                              DO 400 J=1,2
 00773
                             DO 400 K=1,2
00774
                              FI=FLOAT(L(K,J))
 00775
                             PHA=PHAI(K,1)'
PELIA(|)=FLSIN(2.*PHA)/RADIAL(1)+ENERGY(.T)-VFOT(1,J)-COS(2.*PHA)
00776
                          DELTA() = 1*SIN(-**PHA)/RADIAL(1) + ENERGY(J) - VPOT(I, J) - COS(2.*PHA)
DELTA() = 1*HAP-DELTA(1)
DELTA(2) = F1*SIN(2.*PHA+DELTA(1))/(RADIAL(1) + RADIAL(1+1))*2. + ENERGY
[(J) - (VPOT(I, J) + VPOT(I+1, J))/2. - COS(2.*PHA+DELTA(1))
DELTA(2) = DELTA(2) **HAB
00778
00779
00780
                           DELTA(3)=E*SIA(2.*PHA+DELTA(2))/(RADIAI(1)+RADIAI(1+1))*2.+ENERGY
|| 1(J)=(VPOT(1,J)*VPOT(1+1,J))/2.-COS(2.*PHA+DELTA(2))
                             DELTA(3)=HAP*DFITA(3)
00782
                            DELIA() PERIAMPERIAL ()
DELIA(4) PERIAMPERIAL 
                           LJ)-COS(2.*(PHA+DELTA(3)))
0078
                            DELTA(4)=DELTA(4)*HAR
00784
                            PHALO(K,J)=PHALO(K,J)+(DELTA(1)+2.*(DELTA(2)+DELTA(3))+DELTA(4))/
00785
                            DFLAME(1)=-F1*COS(2.*PHA)/RADIAL(1)-SIN(2.*PHA)
00786
                            DFIAMP(2)=-FL*COS(2.*PHA+DFITA(1))/(RADIAL(1)+RADIAL(1+1))*2.-SIN(
```

```
12.*PHA+DELTA(1))
DELAMP(3)=-FL*COS(2.*PHA+DELTA(2)/(RADIAL(I)+RADIAL(I+1))*2.-SIN(
 00787
                                      12. *PHA+DELTA(2))
                                        DELAMP(4)=-FL*COS(2.*(PHA+DELTA(3)))/RADIAL(I+1)-SIN(2.*(PHA+DELTA
 00788
                                      \begin{array}{l} \text{AMPO}(K,J) = \text{AMPO}(K,J) + \text{HAB*}(\text{Delamp}(1) + 2.*(\text{Delamp}(2) + \text{Delamp}(3)) + \text{Delamp}(4))/6. \end{array} 
 00789
                              400 CONTINUE
 00790
                                        IF(LL.LT.0)GO TO 370
 00791
                                        DO 350 J=1,2
 00792
                                        DO 350 K=1,2
 00793
                                     \label{eq:final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_final_
 00794
                                     \label{eq:final_problem} \begin{split} & \texttt{FMATRX}(\texttt{LL1},\texttt{K},\texttt{J},\texttt{1}) = \texttt{FMATRX}(\texttt{LL1},\texttt{K},\texttt{J},\texttt{1}) + \texttt{EXP}(\texttt{AMPO}(\texttt{K},\texttt{1})) + \texttt{COS}(\texttt{PHAIO}(\texttt{K},\texttt{1})) \\ & \texttt{1} + \texttt{VPOTEI}(\texttt{1}) + \texttt{EXP}(\texttt{AMPO}(\texttt{J},\texttt{2})) + \texttt{COS}(\texttt{PHAIO}(\texttt{J},\texttt{2})) + \texttt{HAB} \end{split}
 00795
 00796
 00797
                             370 CONTINUE
                                       AMP1(1,2,1)=AMP1(1,1,1)
AMP1(2,2,1)=AMP1(2,1,1)
 00799
                                                                                                                              PHAIO(1,2))/RADIAL(I)
 00800
                                       AMP1(1,1,1)=EXP(AMPO(1,2))*COS(
AMP1(2,1,1)=EXP(AMPO(2,2))*COS(
                                                                                                                              PHAIO(2,2))/RADIAL(4)
 00801
 00802
                             500 CONTINUE
 00803
                                        KKK1=KKK+1
                                        A=RADTUS(KKK1)
 00804
                          A=MAUJUSIANA /
WHITE(6,1200), KAI, KAIS

1200 FORMAT(1H, 3H R=,F5,1,10(2H *),14H SEKIBUN KAISU,2110)
WRITE(6,1000)((PHAIO(K,J),K=1,2),J=1,2),((AMPO(K,J),K=1,2),J=1,2)
 00805
 00806
 00807
                                        IF(KKK, NE. 4)GO TO 210
 00809
                                        DO 3000 M=1,2
                                        FMATRX(1,2,M,2)=0.
 00810
 00811
                                        FMATRX(2,M,1,2)=0.
                                        DO 3000 N=1,2
 00812
 00813
                                        FMATRX(1,1,M,N)=0.
 00814
                           3000 CONTINUE
 00815
                                        RETURN
 00816
                                      SUBROUTINE REI(LL,LK,NPN,NPP)
DIMENS ON C1(2),C2(2),C3(2)
COMMON/SIC/SIGNA(4), SHERN(4,2)
COMMON/BES/FJ(300,2),FNEU(300,2),RK(2),KR(2)
 00817
 00818
 00819
 00820
 00821
                                        COMMON/AASSIG/ASSLEG(2000,3)
 00822
                                        COMMON/FFSC/FSC(2,3,2)/AAAAMP/AAMP(2000,2,3,2),BBMP(300,2,3,2),
                                     1ABMP(300,2,3,2),BAMP(300,2,3,2)
                               F(I.K,K) I,UP-UP ORUP-DOWN, J, MAFNETIC QUANTUM NUMBER, KREAL OR IMAG
 00823
                                        DO 50 N=1.4
 00824
                                        SIGMA(N)=.0
 00825
                                        DO 50 M=1,2
 00826
                                        SHERM(N.M)=O.
                               50 CONTINUE
 00827
 00828
                                       DO 60 N=1,3
 00829
                                        DO 60 M=1,2
 00830
                                       DO 60 L=1,2
 00831
                                       FSC(M,N,L)=0.
 00832
                               60 CONTINUE
 00833
                                       DO 100 M=1,3
 00834
                                       M1=M-2
 00835
                                       DO 200 LLL=0,LL
 00836
                                      LLL1=LLL+1
00837
                                      FLL=FLOAT(LLL)
 00838
                                      IF(M1)300,400,500
00839
                             300 CONTINUE
00840
                                      ALEG=ASSLEG(LIL1,2)
00851
                                     ALEG1=ASSLEG(LLL1,3)
C1(2)=(FLL/(2.*FLL+3.)/2.)**.5
00859
00843
                                      1F(LLI .EQ. 0)GO TO 350
00844
                                     C1(1)=((FLL+1.)/(2.*FLL-1)/2.)**5
C2(2)=((FLL+1.)*(FLL+2.)/FLL/(2.*FLL-1.)/2.)**.5
00845
00846
                                     C2(1)=(Fil*(Fil-1.)/(Fil+1.)/(2.*Fil+3.)/2.)**.5
00847
                                      GO TO 600
00848
                             350 CONTINUE
00849
                                     C1(1)=0.
00850
                                      C2(1)=0.
00851
                                     C2(2)=0.
00852
                                     GO TO 600
00853
                           400 CONTINUE
                                     Al EG=ASSLEG(LLL1,1)
```

F, BAMP(300, 2, 3, 2).

COMMON/TANDEL/TANDE (300,2,2)

00925

```
COMMON/SCDL/SINDL(300,2,2),COSDL(300,2,2),SCSQ(300,2,2)
                    ALBG1=ASSLEG(LLL1,2)
C1(2)=-((FLL+1.)/(2.*FLL+3.))**.5
C2(1)=-(FLL*(FLL+2.)/(2.*FLL+3.)/(FLL+1.))*4.5
                                                                                                                                            C SDL (I.J.K) I.J.L DR -L-1 OF ELASTIC OR INBLASTIC, K, SIN OR COS
00855
                                                                                                                                 00926
00856
                                                                                                                                                      LK=LK+2
                                                                                                                                 00927
00857
                                                                                                                                                      DO 1000 N=1,NPP
                     IF(LLL.LE.O)GO TO 450
                     C1(1)*(FLL/(2.*FLL-1.))**.5
                                                                                                                                 00928
                                                                                                                                                      DO 1000 NN=1,2
OORSE
                     C2(2)=((FLL+1.)*(FLL-1.)/FLL/(2.*FLL-1.))**.5
                                                                                                                                 00929
                                                                                                                                                      DO 1000 NNN=1,3
DO 1000 NNNN=1,2
00859
                                                                                                                                  00930
00860
                     GO TO 600
                                                                                                                                  00931
                                                                                                                                                      BBMP(N,NN,NNN,NNNN)=0.
ABMP(N,NN,NNN,NNNN)=0.
00861
                450 CONTINUE
                                                                                                                                  00932
00862
                     c1(1)#0.
                                                                                                                                 00933
00863
                                                                                                                                                       BAMP(N,NN,NNN,NNNN)=0.
                      c2{2}=0.
                                                                                                                                 00934
00864
                                                                                                                                                1000 CONTINUE
DO 1100 N=1,NPN
                      GO TO 600
                                                                                                                                  00935
 00865
                550 CONTINUE
                                                                                                                                  00936
                                                                                                                                                       DO 1100 NN=1,2
 00866
                      c1(1)=0.
                                                                                                                                  00937
 00867
                                                                                                                                                       DO 1100 NNN=1,3
                      C2(2)=0.
                                                                                                                                  00938
                                                                                                                                                        DO 1100 NNNN=1,2
 00868
                      GO TO 600
                                                                                                                                  00939
                                                                                                                                                       AAMP(N,NN,NNN,NNNN)=0.
00869
                                                                                                                                  00940
                500 CONTINUE
 00870
                      ALEG -- ASSLEG(LLL1,2)
                                                                                                                                                1100 CONTINUE
                     ALDRA-ASSLEG(LLL1,1)
c1(2)=(FLL/(2, FLL+3,1/2,1)**.5
c2(1)=(FLL+2,1/(2, FLL+3,1/2,1)**.5
c2(1)=(C(1)+(2,**.5)**.1+3,1/2,1)**.5
FIGURE (FLL+2,1/(2, FLL+1,1))**.5
c1(1)=(FLL+1,1/(2, FLL+1,1))**.5
                                                                                                                                  00941
 00871
                                                                                                                                                       DO 100 1=1,2
                                                                                                                                  00942
 00872
                                                                                                                                                        EXSe-1.
                                                                                                                                  00941
 00873
                                                                                                                                  00944
                                                                                                                                                        1.1 \pm 2
                                                                                                                                                       IF(1.EQ.2)GO TO 250
 00874
                                                                                                                                  00945
 00875
                                                                                                                                                        JJ=1
                                                                                                                                  00946
 00876
                                                                                                                                                        EXS#1.
                                                                                                                                  00947
 00877
                                                                                                                                  00948
                                                                                                                                                  250 CONTINUE
                      c1(1)=c1(1)/2,**.5
 00878
                                                                                                                                                        DO 200 J=JJ, LL
                      C2(2)=((FLL-1.)/(2.*FLL-1.)/2.)**.5
                                                                                                                                   00949
 00879
                                                                                                                                   00950
                                                                                                                                                        It all all
                     O PONTINUE

C1(2)=C1(2)=((FLL+L.)/(2.*FLL+L.))**.5

C2(1)=C2(1)=(FLL+L.)/(2.*FLL+L.))**.5

C2(2)=(C2(2)=(FLL/(2.*FLL+L.))**.5

C1(1)=C1(1)=(FLL/(2.*FLL+L.))**.5

IF(LLL.GT.LK+2)GO TO 610

PD 7200-1-1
                600 CONTINUE
 00880
                                                                                                                                                        AJ=FLOAT(J-1)
                                                                                                                                   00951
 00881
                                                                                                                                                        IF(I,EQ, 1)GO TO 350
                                                                                                                                   00952
 00992
                                                                                                                                   00953
                                                                                                                                                        J1=J-1
 00883
                                                                                                                                   00954
                                                                                                                                                   350 CONTINUE
  00884
                                                                                                                                   00955
                                                                                                                                                        AJI=FLOAT(J1-1)
                                                                                                                                                        AL=FLOAT(2*J-1)*(FLOAT(2*J1-1))**.5
 00885
                                                                                                                                   00956
                     \begin{array}{ll} & \text{FSC}(1,M,1) = \text{PSC}(1,M,1) + (\text{AAMP}(\text{LLL1},2,M,1) * \text{C1}(1) - \text{AAMP}(\text{LLL1},1,M,1) * \text{C1}(2) + \text{BBMP}(\text{LLL1},1,M,1) * \text{C2}(1) - \text{BBMP}(\text{LLL1},2,M,1) * \text{C2}(2)) * \text{ALES} \end{array}
                                                                                                                                   00957
                                                                                                                                                        IF(J.GT.LK+3)GO TO 310
 00886
 00887
                                                                                                                                   00958
                                                                                                                                                        DO 300 K±1,2
                     FSC(2,M,1)=PSC(2,M,1)+(BAMP(LLL1,2,M,1)*C(1())=HAMP(LL1,1,M,1)*
IC1(2)*ABMP(LL1,1,M,1)*C2(1)-ABMP(LLL1,2,M,1)*C2(2))*ALEGI
                                                                                                                                                        DO 300 M=1,2
                                                                                                                                   00959
                                                                                                                                                         \begin{array}{l} \operatorname{SbL}(K,M,1) = \operatorname{SINDL}(J1,M,1) * \operatorname{Cospl}(J,K,2) * \operatorname{SINDL}(J,K,2) * \operatorname{Cospl}(J1,M,1) \\ \operatorname{SbL}(K,M,2) = \operatorname{Cospl}(J1,M,1) * \operatorname{Cospl}(J,K,2) - \operatorname{SINDL}(J1,M,1) * \operatorname{SINDL}(J,K,2) \\ \end{array} 
                                                                                                                                   00960
  OORER
                                                                                                                                   00961
                                                                                                                                   00962
                                                                                                                                                   300 CONTINUE
                 700 CONTINUE
  00889
                                                                                                                                   00963
                                                                                                                                                        GO TO 320
                      40 TO 620
  00890
                                                                                                                                   00965
                                                                                                                                                   310 CONTINUE
                 610 CONTINUE
  00891
                                                                                                                                   00965
                                                                                                                                                        Do 330 K=1,2
                       po 710 I=1,2
                       FSC(1,M,I)=FSC(1,M,I)+(AAMP(LLL1,2,M,I)*C1(1)-AAMP(LLL1,1,M,I)*
  00892
  nower a
                                                                                                                                                         DO 330 M=1,2
                                                                                                                                  00966
                                                                                                                                                         SDL(K,M,1)=.0
                      1C1(2))*ALEG
                                                                                                                                  00967
                                                                                                                                  00968
                                                                                                                                                         SDL(K,M,2)=1.
  00894
                  710 CONTINUE
                                                                                                                                  00969
                                                                                                                                                    330 CONTINUE
                  620 CONTINUE
  00895
                                                                                                                                  00970
                                                                                                                                                    320 CONTINUE
                  200 CONTINUE
  00896
                                                                                                                                  00971
                       DO 800 I=1,2
  00897
                       FSC(1,M,I)=-FSC(1,M,I)*3.464101615
FSC(2,M,I)=-FSC(2,M,I)*3.464101615
                                                                                                                                  00972
                                                                                                                                                         MMM= 3
  00898
                                                                                                                                                        IF(J.EQ.1)GO TO 600
GO TO 700
                                                                                                                                  00973
  00899
                                                                                                                                  00974
                  800 CONTINUE
  00900
                                                                                                                                                   600 CONTINUE
                                                                                                                                  00975
                       po 900 L=1,2
  00901
                                                                                                                                  00976
                                                                                                                                                         MM= 2
                        DO 900 N=1,2
  00902
                        SIGMA(M)=SIGMA(M)+FSC(L,M,N)+FSC(L,M,N)
                                                                                                                                  00977
  00901
                                                                                                                                  00978
                                                                                                                                                    700 CONTINUE
  00904
                  900 CONTINUE
                       SIGMA(M)=SIGMA(M)=5.3294E-05
                                                                                                                                                         DO 400 M=MM, MMM
                                                                                                                                   00979
  00905
                                                                                                                                                         AM=FLOAT(M-2)
                                                                                                                                  00980
                  100 CONTINUE
   00906
                       FSC(2,2,1)=+FSC(2,2,1)
FSC(2,2,2)=-FSC(2,2,2)
                                                                                                                                   00981
                                                                                                                                                         no 400 K=1 2
                                                                                                                                                        DO 400 K=1,2

EEXS=EXS*FLOAT((-1)**K)

SF1=SDL(1,1,K)*FMATRX(J1,1,1,3-1)

SF2=SDL(1,2,K)*FMATRX(J1,2,1,3-1)
   00907
                                                                                                                                  00987
   ongov
                                                                                                                                   00983
                        DC 1000 M=1,3
  110190110
                                                                                                                                   00984
                        DO 1000 K=1,2
   00910
                                                                                                                                                        SF3-SDL(1,2,K)*PMATRX(J1,2,1,3-1)
SF3-SDL(2,1,K)*PMATRX(J1,1,2,3-1)
SF4-SDL(2,2,K)*PMATRX(J1,2,2,3-1)
AAMP(J,1,M,K)=EEXS/AL*((AJ+AM)*(AJ1*SF1+(AJ1+1.)*SF2)+(AJ-AM+1.)
1*(AJ1*SF3+(AJ1+1.)*SF4)
                        SHERM(4,2)=SHERM(4,2)+2.*FLOAT((-0**K)*FSC(1,M,K)*FSC(2,M,3-K)
                                                                                                                                   00985
  00911
                                                                                                                                   00986
                        SHERM(4,1)=SHERM(4,1)+2.*FLOAT((-1)**(M+K))*FSC(1,M,K)*FSC(2,4-M,
  00912
                                                                                                                                   00987
   ocsta
                 1000 CONTINUE
                                                                                                                                   00988
                                                                                                                                                         IF(J,GT,LK+3)GO TO 401
   00014
                        po 910 1=1,3
                                                                                                                                  00989
                                                                                                                                                         BBMP(J, I, M, K) = EEXS/AL*((AJ+AM)*(AJ-AM+1.)*AJ1*(AJ1+1.))**.5*(SF1-S
   00915
                        SIGMA(4)=SIGMA(4)+SIGMA(1)
                                                                                                                                                        1F2-SF3+SF4)
   00916
                  910 CONTINUE
                                                                                                                                                       171-3-3-3-3-1
BBMP(J, I, M, K) -- BBMP(J, I, M, K)
ABMP(J, I, M, K) -- BBMP(J, I, M, K)
ABMP(J, I, M, K) -- BEXS/AL* (AJI*(AJI+1.))**.5*(-(AJ-AM+1.)*(SFI-SF2)
-- (AJ-AM)*(SF3-SF4)
                        SHERM(4,2)=SHERM(4,2)/SIGMA(4)*5.3249E=05
                                                                                                                                   00990
  00917
                        SHERM(4,1)=SHERM(4,1)/SIGMA(4)*5.3249E-05
                                                                                                                                   16600
   DOOLS
  06919
                        RETURN
                                                                                                                                                         BAMP(J,1,M,K)=EEXS/AL*((AJ+AM)*(AJ-AM+1.))**.5*(-AJ1*(SF1-SF3)
                                                                                                                                   00992
   00920
                        END
                                                                                                                                                        1-(AJ1+1.)*(SF2-SF4))
                                                                                                                                   00993
                                                                                                                                                         BAMP(J,I,M,K) = -BAMP(J,I,M,K)
                                                                                                                                   00994
                                                                                                                                                    401 CONTINUE
                                                                                                                                   00995
                                                                                                                                                    400 CONTINUE
                                                                                                                                   00996
                                                                                                                                                    200 CONTINUE
                                                                                                                                   00997
                                                                                                                                                    100 CONTINUE
                                                                                                                                   00998
   00921
                        SUBROUTINE NAU(11,1K,NPN,NPP)
                                                                                                                                                         WRITE(6,3500)
                                                                                                                                   00999
   009322
                                                                                                                                                   3500 FORMAT(////29H AAMP NO ZERO DE ARUBEKI ATAI)
                        DIMENSION Spi (2,2,2)
                                                                                                                                   01000
   00923
                        COMMON/MATRIX/FMATRX(2000,2,2,2)
                                                                                                                                                         WRITE(6,3000)((AAMP(1,2,M,N),M*1,3)N=1,2)
   06025
                       COMMCN/AAAAMP/AAMP(2000,2,3,2),BHMP(300,2,3,2),ABMP(300,2,3,2)
```

01001

```
WRITE(6, 3100) ((BBMP(1,1,M,N),M=1,3),N=1,2)
WRITE(6, 3100) ((BBMP(1,2,M,N),M=1,3),N=1,2)
WRITE(6, 3100) ((BBMP(1,2,M,N),M=1,3),N=1,2)
WRITE(6, 3200) ((BAMP(1,1,M,N),M=1,3),N=1,2)
WRITE(6, 3200) ((BAMP(1,2,M,N),M=1,3),N=1,2)
WRITE(6, 3300) ((ABMP(2,2,M,N),M=1,3),N=1,2)
WRITE(6, 3500) ((ABMP(2,2,M,N),M=1,3),N=1,2)
WRITE(6, 3500) ((ABMP(1,2,M,N),M=1,3),N=1,2)
3100 FORMAT(1H,6H BBMP-,6E15.5)
3100 FORMAT(1H,6H BBMP-,6E15.5)
3500 FORMAT(1H,6H BBMP-,6E15.5)
3500 FORMAT(1H,6H BBMP-,6E15.5)
01002
01003
                                                                                                                                                              4200 FORMAT(10X, 32H CAUSION?? VPTEI DIMENSION OVER
01004
                                                                                                                                           01082
                                                                                                                                                                     GO TO 1200
01005
                                                                                                                                           01083
                                                                                                                                                             4100 CONTINUE
01006
                                                                                                                                           01084
                                                                                                                                                               400 CONTINUE
01007
                                                                                                                                           01085
                                                                                                                                                                     DO 50 I-1,N99
01008
                                                                                                                                           01086
                                                                                                                                                                     VPTEI (1)=0.
01009
                                                                                                                                           01087
01010
                                                                                                                                           01088
                                                                                                                                                                50 CONTINUE
01011
                                                                                                                                           01089
                                                                                                                                                                     DO 2000 I=1,NPP
                      DO 2000 M=1,3
                                                                                                                                                                     DO 2000 J=1,2
01012
                                                                                                                                           01090
                      DO 2000 N=1,2
01013
              DO 2000 N=1,2

AMMF(1,2,M,N)=0.

BAMF(1,1,M,N)=0.

BBMF(1,2,M,N)=0.

BBMF(1,2,M,N)=0.

ABMF(1,2,M,N)=0.

ABMF(1,2,M,N)=0.

ABMF(2,2,M,N)=0.

ABMF(2,2,M,N)=0.

ABMF(2,1,M,N)=0.
                                                                                                                                                                     DO 2000 K=1,2
                                                                                                                                           01091
01014
                                                                                                                                                                     DO 2000 M=1,2
                                                                                                                                           01092
01015
                                                                                                                                           01093
                                                                                                                                                                     FMTRX(I,J,L,M)=0.
                                                                                                                                                              2000 CONTINUE
01016
                                                                                                                                           01094
                                                                                                                                                                    DO 100 I-NN1.NN2
01017
                                                                                                                                           01095
01018
                                                                                                                                           01096
                                                                                                                                                                     FFI-FLOAT(I)
                                                                                                                                                                    R=RADI+HAB*FFI
01019
                                                                                                                                           01097
                                                                                                                                                                    RK(1)=R *FK(1)
01020
                                                                                                                                           01098
                                                                                                                                                                    RK(2)=R *FK(2)
01021
                                                                                                                                           01099
                                                                                                                                                                    CALL BESELI(LL,I,NPP)
01022
                                                                                                                                           01100
                3600 FORMAT(12E11.3)
                                                                                                                                                                    DO 300 J=1,2
01023
                                                                                                                                           01101
                                                                                                                                                                    DO 300 N=1,2
DO 300 K=1,2
Al=MAVEFU(1,1,2,J)*WAVEFU(3,1,K)
A2=MAVEFU(1,2,J)*WAVEFU(3,2,K)
VPTEI(1)*VPTEI(1)*S.*Al/AZ/AZ*(8./AZ**3.*(1.-EXP(-AZ*R))/R/R-(8.
01024
                       WRITE(6,3601)
                                                                                                                                           01102
               3601 FORMAT (6H AAMP=)
01025
                                                                                                                                           01103
                       WRITE(6,3600)((((AAMP(L,1,M,J),J=1,2),M=1,3),I=1,2),L*1,LK+2)
01026
                                                                                                                                           01104
01027
                       WRITE(6.3605)
                                                                                                                                           01105
01028
                3605 FORMAT (1HO
                                                                                                                                                                   1/A2/A2/R+4./A2+R)*EXP(-A2*R))
                        WRITE(6,3600)((AAMP(L,I,1,2),I=1,2),L=LK+3,LL)
01029
                                                                                                                                           01106
                                                                                                                                                               300 CONTINUE
01030
                       WRITE(6,3602)
                                                                                                                                                                    VPTEI(I)=VPTEI(I)*1.5437488
DO 200 K=1,2
                                                                                                                                           01107
01031
                3602 FORMAT(6H ABMP=)
                                                                                                                                           01108
                       WRITE(6,3600)((((ABMP(L,I,M,J),J=1,2),M=1,3),I=1,2),L=I,LK+2)
01032
                                                                                                                                           01109
01033
                        WRITE(6,3603)
                                                                                                                                           01110
                                                                                                                                                                    IF(K.EQ.2)JJ=2
                3603 FORMAT(6H BAMP*)
01034
                       WRITE(6,3600)((((BAMP(L,I,M,J),J=1;2),M=1,3),I=1,2),L=1,LK+2)WRITE(6.3604)
                                                                                                                                                                    DO 200 J=JJ, LL
01035
                                                                                                                                           01112
                                                                                                                                                                    .I1=.I+1
                                                                                                                                                                   JIFUX.EQ.2) JI-J1

|FKK.EQ.2) JI-J1

|FMTRK(J.1,1,K)=FMTRX(J.1,1,K)+EJ(J.1)*VPTEI(I)*FJ(JI,2)*R*R

|FMTRK(J.1,2,K)=FMTRX(J.1,2,K)+FJ(J,1)*VPTEI(I)*FMEU(JI,2)*R*R

|FMTRK(J.2,1,K)=FMTRX(J,2,1,K)=FMEU(J,1)*VPTEI(I)*FMEU(J).2)*R*R

|FMTRK(J,2,2,K)=FMTRX(J,2,2,K)=FMEU(J,1)*VPTEI(I)*FMEU(J).2)*R*R
01036
                                                                                                                                           01113
01037
                3604 FORMAT(6H BBMP="
                                                                                                                                           01114
                        WRITE(6,3600)((((BBMP(L,I,M,J),J=1,2),M=1,3),I=1,2),L=1,LK+2)
01038
                                                                                                                                           01115
01039
                        RETURN
                                                                                                                                           01116
01040
                                                                                                                                           01117
                                                                                                                                           01118
                                                                                                                                                               200 CONTINUE
                                                                                                                                                               100 CONTINUE
                                                                                                                                           01119
                                                                                                                                                                    DO 3000 J=1,LL
                                                                                                                                           01120
                                                                                                                                           01121
                                                                                                                                                                    DO 3000 I=1.2
                                                                                                                                            01122
                                                                                                                                                                    DO 3000 K=1,2
01041
                         SUBROUTINE TAE(LL, NPN, NPP)
                                                                                                                                            01123
                                                                                                                                                                    DO 3000 M=1.2
01042
                        DIMENSION VPTEI (20000)
                        DIMENSION VPTEI (20000)
DIMENSION FMTRX(300,2,2,2),FMTRX1(300,2,2,2)
COMMON/HABA/HABA(4)
COMMON/MAYPOT/POTE(2,3),WAVEFU(3,2,2)
COMMON/SES/FJ(300,2),FNEU(300,2),RK(2),KR(2)
COMMON/SED/L/SIDUL(300,2,2),CSD((300,2,2),SCSQ(300,2,2)
COMMON/MATRIX/FMATRX(2000,2,2,2)
                                                                                                                                            01124
                                                                                                                                                                    FMTRX1(J,I,K,M)=FMTRX1(J,I,K,M)+FMTRX(J,I,K,M)*HAB
01043
                                                                                                                                                            3000 CONTINUE
                                                                                                                                            01125
01044
                                                                                                                                            01126
                                                                                                                                                                    HAB=HAB*AA
01045
                                                                                                                                                                    RADI = RADI + RAD*AA**(JI-1)
                                                                                                                                            01127
01046
                                                                                                                                            01128
                                                                                                                                                                    WRITE(6,3100)R,RADI
01047
                                                                                                                                            01129
                                                                                                                                                             3100 FORMAT(1H , 3H R= , E15.5, 9H DE OWARI, 3H R= , E15.5, 12H DE HAJIMARU)
01048
                                                                                                                                            01130
                         COMMON RRADAL/RADIUS (6)
                                                                                                                                                                    JI=JI+1
01049
                                                                                                                                            01131
                                                                                                                                                                   IF(JI.NE.5)GO TO 400
WRITE(6,3300)
                         COMMON/FKF/FK(2)
01050
                                                                                                                                            01132
01051
                         N99-20000
                                                                                                                                            01133
                                                                                                                                                            3300 FORMAT(1HO,6H FMTRX1=)
WRITE(6,5200)((((FMTRX1(J,I,K,M),I=1,2),M=1,2,J=1,LL+2)
01052
                         LK=LL
                                                                                                                                            01134
                        DO 60 I=1,NPP
01053
                                                                                                                                                            3200 FORMAT(8E15.5)
                        DO 60 J=1,2
DO 60 K=1,2
                                                                                                                                            01135
01054
                                                                                                                                            01136
                                                                                                                                                                   DO 1000 N=1,2
 01055
                                                                                                                                            01137
                                                                                                                                                                   JJ=1
01056
                         DO 60 M=1,2
                                                                                                                                            01138
                                                                                                                                                                   IF(N.EQ.2) JJ=2
 01057
                         FMTRX1(I,J,K,M)=0.
                                                                                                                                            01139
                                                                                                                                                                   DO 1000 J=JJ, LL
 01058
                    60 CONTINUE
                                                                                                                                            01140
 01059
                                                                                                                                                                     . J-1
                                                                                                                                                                   iF(N.EQ.2)J1=J-1
DO 1000 I=1,2
                                                                                                                                            01141
 01060
                         HAB=1./FK(1)/41.958
                                                                                                                                            01142
                         IF(HAB.LT.HABA(4))GO TO 70
 01061
                                                                                                                                            01143
                                                                                                                                                                    DO 1000 K=1.2
 01062
                         GO TO 80
                                                                                                                                                                    FMATRX(J,I,K,N)=FMATRX(J,I,K,N)+COSDL(J,I,1)*COSDL(J1,K,2)*
 01063
                    70 CONTINUE
                                                                                                                                                                  THORIXI (J, 1, N) * SINDL(J, 1, 1) * SINDL(J1, K, 2) * FMTRX1 (J, 2, 2, N) 

2COSDL(J, 1, 1) * SINDL(J1, K, 2) * FMTRX1 (J, 1, 2, N) - SINDL(J, 1, 1) * COSDL(J1, 3, 2) * FMTRX1 (J, 2, 1, N)
 01064
                        WRITE(6,90)
FORMAT(//20(2H *),22H CAUTION TAE INCORRECT,20(2H *)
 01065
 01066
                         HAB*HABA(4)+.01
                                                                                                                                            01145
                                                                                                                                                           1000 CONTINUE
 01067
                                                                                                                                                                   FMATRX(1,1,1,1)=.0

FMATRX(1,1,2,1)=.0

FMATRX(2,1,1,2)=.0

FMATRX(2,2,1,2)=.0
                                                                                                                                           01146
 01068
                         AA = (HAB/HABA(4)) **(1./FLOAT(N))
RAD=(RADIUS(6)-RADIUS(5))/(AA*N-1.)*(AA-1.)
                                                                                                                                           01147
 01069
                                                                                                                                           01148
 01070
                         NN=INT(RAD/HABA(4)/AA)
                                                                                                                                           01149
 01071
                         HAB-RAD/FLOAT (NN)
                                                                                                                                           01150
                                                                                                                                                                    VP*.0
 01072
                                                                                                                                                                    DO 5400 J=1,2
 C1073
                                                                                                                                           01151
                         NN2=NN
                                                                                                                                                                   NO 5400 J=1,2

00-5400 I=1,2

A1=WAVEFU(1,1,1)*WAVEFU(3,1,J)

A2=WAVEFU(1,2,1)+WAVEFU(3,2,J)

VP=VP=6.*A1/A2**5
                                                                                                                                           01152
 01074
                         WRITE(6,110)NN
                                                                                                                                           01153
 61075
                   110 FORMAT (//18H TAE SEKIBUN KAISU, 110//)
 01076
                                                                                                                                           01154
                                                                                                                                           01155
 C1077
                         RADI=RADIUS(5)
                                                                                                                                           01156
 01078
                                                                                                                                                                   CONTINUE
                         IF(NN.GE.N99)GO TO 4000
 01079
                                                                                                                                           01157
                                                                                                                                                                   VP=VP*1.5437488
                         GO TO 4100
                4900 CONTINUE
 01080
 01081
                         WRITE(6,4200)
```

```
01158
                      5200 CONTINUE
 01159
                                 LL-LL+1
 01160
                                  AA=1.
 01161
                                 BB=1.
                                DO 5100 J=1,LL-2
FJ1=FLOAT(J)
AA=AA*FJ1/(FJ1-.5)
BB=BB*FJ1/(FJ1-1.5)
 01162
 01163
 01164
 01165
                      5100 CONTINUE
AA*AA/(FJ1+.5)/(FJ1+1.5)*(FJ1+1.)/(FJ1+2.5)
 01166
 01167
 01168
                                 BB=BB/(FJ1-.5)/(FJ1+.5)
01169
                                AA1=AA
                                BBI=BB
                                 LAL*LL*10
01171
                              LAL+LL*10
D0 5300 J-1,LAL+200
FJI=FLOAT(J)
AA-AAA(FJI-.5)/FJI*(FJI+FLOAT(LL-1))/(FJI+FLOAT(LL-1)+1.5)
1*(FK(2)/FK(1))*2
BB-BB*(FJI-1.5)/FJI*(FJI+FLOAT(LL-1)-1.)/(FJI+FLOAT(LL-1)-.5)
1*(FK(2)/FK(1))*2
 01172
 01174
01175
 01176
                                AAI=AAI+AA
BBI=BBI+BB
 01177
                     BB|*BB|*BB

5300 CONTINUE

AA1-AA1*VP*(FK(2)/FK(1))**(LL/FK(1)

BB|-*BB|*VP*(FK(2)/FK(1))**(LL-2)/FK(1)

DO 5500 1-1,

DO 5500 J-1,

PMATRX(LL,I,J,1)*AA1

FMATRX(LL,I,J,2)*BB

5500 CONTINE
 01178
 01179
01180
01181
01182
01183
 01185
                                CONTINUE
IF(LL.GE.NPN-5)GO TO 5600
AB1=AMAX1(AA1,BB1)
IF(AB1.GT.10E-4)GO TO 5200
 01186
 01187
 01188
                      5600 CONTINUE
01189
                               FMATRX (LK+1, 1, 1, 1, 2) *- FMATRX (LK+1, 1, 1, 2) 
FMATRX (LK+1, 2, 1, 2) *- FMATRX (LK+1, 1, 1, 2) 
FMATRX (LK+2, 1, 1, 2) *- FMATRX (LK+2, 1, 1, 2) 
FMATRX (LK+2, 2, 1, 2) *- FMATRX (LK+2, 1, 1, 2) 
FMATRX (LK+2, 2, 1, 2) *- FMATRX (LK+2, 2, 1, 2)
01190
01191
01192
01193
                      1200 CONTINUE
01194
01195
01196
                                RETURN
```

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