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Osaka University
100-KW Class Electron Beam Welding Technology (Report I) —Welding Apparatus and Some Aspects as A Heat Source—

Yoshiaki ARATA* and Michio TOMIE**

Abstract

A 100 KW-class electron beam welding apparatus was designed and assembled. Using this apparatus, characteristics of a powerful electron beam up to 120 KW as a heat source and of its bead penetration were both investigated. The possibility of both one-pass welding and cutting thick materials up to 10~20 cm was proposed.

1. Introduction

The heat source of the electron beam gives the deepest weld bead penetration compared with any others as it is well known. Characteristics of the electron beam heat source are that both the power and density become extremely high, moreover, these are controlled easily.

Such characteristics efficiently affect the thick materials as its power becomes much higher. The powerful electron beam of 100 KW-class or above, has the advantage over any other heat source, for the welding ultra high thick materials, 10~20 cm and/or over. From such a viewpoint, the 100 KW-class EB-welder was produced and its capability was tested; moreover, some properties of the powerful electron beam as a heat source were studied. It was then applied to welding and cutting.

2. Characteristics of 100 KW-EBwelder

Fig. 1 and Photo. 1 show the schematic diagram of the installation and its appearance respectively. Provided that \( V_b \text{(KV)} \), \( I_b \text{(mA)} \), and \( W_b \text{(KW)} \) are taken as beam accelerating voltage, beam current and beam power in the maximum value of a continuous respectively, its capability is as follows.

\[ V_b = 100, \ I_b = 1000, \ W_b = 100 \]

And it is also possible to utilize it as follows:

\[ V_b = 200, \ I_b = 500, \ W_b = 100 \]

And this welder was employed up to 120 KW to obtain experimental data although it was for a short interval. The volume of the vacuum work chamber is 1.3 m³ and the capacity of the exhaust system is 2,000/ min rotary pump, 10,000 l/min mechanical booster pump, 360,000 l/min diffusion and ejection booster pump respectively. The maximum welding speed is 5 m/min and the cathode material is 3 mmφ circular type Tungsten.

Fig. 1. Schematic diagram of EB-welder.

Photo 1. General view of 100 KW-EB welder which was developed by authors.

† Received on Nov. 25, 1972
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3. Some Results and Discussion

The welding bead test was performed using stainless steel SUS304, correspond to AISI304, whose chemical composition is shown in Table 1. The results obtained are shown in Figs. 2-4 and Photos 2-5. Photo 2 indicates the typical transverse section of the bead of 50 KW and 100 KW electron beam weldment. Figure 2 and Photo 3 show one example of distribution of the vickers hardness and the micro-structure of the bead cross-section respectively.

Figure 3 shows the effect of welding speed on penetration depth at 100 KW, and using this figure, the relation of $h_p$ against $1/\sqrt{v_b}$ ($h_p$: penetration depth, $v_b$: welding speed) is obtained as shown in Fig. 4. This is in agreement with formula, $h_p \propto I_b V_b^{1/2} / \sqrt{v_b}$, which is given by authors in another report of this JWR'.

Table 1. Chemical composition (Wt.%) of stainless steel used (SUS304 correspond to SUS27 or AISI304).

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<tr>
<th>Composition</th>
<th>C</th>
<th>Mn</th>
<th>Si</th>
<th>Ni</th>
<th>Cr</th>
<th>Cu</th>
<th>Mo</th>
<th>Al</th>
<th>S</th>
<th>P</th>
</tr>
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<tr>
<td>SUS 304</td>
<td>0.05</td>
<td>0.74</td>
<td>0.24</td>
<td>1.09</td>
<td>19.5</td>
<td>0.01</td>
<td>0.015</td>
<td>0.010</td>
<td>0.030</td>
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![Photo 2](image)

(a) Cross-sectional view of the bead, welded under conditions of $v_b = 60$ cm/min for SUS304
(b): $V_b = 100$ KV, $I_b = 500$ mA, $W_b = 50$ KW
(b): $V_b = 100$ KV, $I_b = 1000$ mA, $W_b = 100$ KW

![Fig. 2](image)

Fig. 2. Hardness distribution in cross-section of welds, ($V_b = 100$ KV, $I_b = 1000$ mA, $W_b = 100$ KW, $v_b = 60$ cm/min, SUS304).

![Fig. 3](image)

Fig. 3. Relations between $v_b$ and $h_p$.

![Fig. 4](image)

Fig. 4. Relations between $h_p$ and $1/ \sqrt{v_b}$. 
Photo 3. Microstructure at various positions in weld bead, \(V_b=100 \text{ KV}, \ i_b=1000 \text{ mA}, \ W_b=100 \text{ KW}, \ \nu_b=60 \text{ cm/min}, \text{ SUS304} \).

Photo 4 indicates one example of 100 KW electron beam cutting, which demonstrates the usefulness of the powerful beam for cutting ultra thick materials.

Photo 5 shows the profile of the very long molten pool over 10 cm waved strongly during 100 KW-class beam welding, and its aspect was that of molten metal poured into the long narrow beam cutting zone which was similar to a deep narrow gap. Such a powerful beam looks like it causes severe gaps compared with a relatively low power beam such as the 50 KW-class beam or below, especially the evaporation due to violent boiling during welding.

Such “welding vapor” emitted violently from the molten pool near the beam, heavily contaminates both space and wall surface of the beam channel and the beam accelerating chamber, and it leads to fluent arcing in the electron gun.

Consideration for its prevention is as follows.
1) To make each slit or nozzle of the beam channel as small or long as possible.
2) To make the beam axis shift with each other inside accelerating chamber, the beam channel and the work chamber.
3) To make a relative high pressure gas layer in a
4. Conclusion

The 100 KW-class EB-welder (120 KW in a short time) was designed and installed. The possibility of one-pass welding and cutting for the ultra thick material was proved. A scheme to decrease the damage due to the violent welding vapor was given.

Acknowledgment

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Reference