

Title	New Cathode Material for Air-Plasma Cutting (Report II): Effect of Sintering Temperature on Electrode Consumption(Physics, Process, Instrument & Measurement)							
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Citation	Transactions of JWRI. 1989, 18(2), p. 211-216							
Version Type	VoR							
URL	https://doi.org/10.18910/3929							
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## New Cathode Material for Air-Plasma Cutting (Report II)†

— Effect of Sintering Temperature on Electrode Consumption —

Fukuhisa MATSUDA\*, Masao USHIO\*\*, and Kazuomi KUSUMOTO\*\*\*

#### Abstract

This study has been carried out to explain the effect of sintering temperature on an electrode consumption of air plasma cutting.

 $Zr-Y_2O_3$ ,  $Hf-Y_2O_3$  and  $Ru-Y_2O_3$  systems were studied and compared. It was concluded that; in the case of  $Zr-Y_2O_3$  and  $Hf-Y_2O_3$  systems, the sintering temperature was a little effect on the electrode consumption. Also, the erosion resistance during arcing was not improved by adding  $Y_2O_3$ .

On the other hand, in Ru- $Y_2O_3$  system, the erosion resistance during arcing was remarkably improved by adding  $Y_2O_3$ . It is related to the high density of the electrode which is sintered at comparatively high temperature, 2373K.

KEY WORDS: (Air-Plasma Cutting) (Cathode) (Consumption) (Zirconium) (Hafnium) (Ruthenium) (Yttrium-Oxide)

#### 1. Introduction

In a previous study, it was shown that Ruthenium including  $Y_2O_3$  in  $10\sim35$  wt% have a superior erosion resistance in case of continuous and periodic arcing tests (max 65A), compared with that of Hafnium which is widely used<sup>1</sup>). It is considered that this good erosion resistance is due to the reduction of heat damage on the electrode that because,  $Y_2O_3$  acts as a good electron emitter and Ruthenium metal has higher thermal and electric conductivity than Hafnium. Generally, the heat conduction is severely influenced by the density ratio of material, which is defined by the ratio between the measured density and theoretical one. Sintered material has a little pores in it and the pore content is affected by the sintering condition, practically, by the sintering temperature and starting powder states.

Since the electrode is produced by the sintering

process, the effect of sintering temperature on the erosion resistance is an important factor to develop an endurable cathode for plasma cutting<sup>2)</sup>.

#### 2. Experimental Procedures

## 2.1 Preparation of specimens

In order to make a comparative study, various electrodes were fabricated by the following condition shown in **Table 1.** Powder Zirconium (98% including 2%Hf, mean particle diameter  $5 \mu$ ), Hafnium (99.9% including 2%Zr, mean particle diameter  $5 \mu$ ), Ruthenium (99.9% pure, mean particle diameter  $3 \mu$ ) and Yttria (99.9% pure, mean particle diameter  $2 \mu$ ) were used as starting materials.

These powders were weighed, mixed and pressed under 0.588MPa in a graphite die. After that, the pellets

Table 1 Experimental materials and sintering conditions

Metal	,		₃ CO wt%)	nten	t • •		ering eratur		Sintering time (ks)	Atmosphere
Zr	0,	5,	10,	20,	30	1373,	1573,	1773	3.6	Vacuum
Hf	0,	5,	10,	20,	30	1573,	1773,	1973	1.8	Vacuum
Ru	0,	5,	10,	20,	30	1573,	1773,	2373	1.8	Hydrogen

<sup>&</sup>lt;sup>†</sup> Recieved on November 6, 1989

Transaction of JWRI is published by Welding Research Institute of Osaka University, Ibaraki, Osaka 567, Japan

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(Tip) of Zr-Y<sub>2</sub>O<sub>3</sub> system was made by sintering in vacuum at 1373K, 1573K and 1773K for 3.6ks. Hf-Y<sub>2</sub>O<sub>3</sub> system was sintered in vacuum at 1573K, 1773K and 1973K for 1.8ks.

 $Ru-Y_2O_3$  system was made by sintering in hydrogen atmosphere at 1573K, 1773K and 2373K for 1.8ks. The sintered tips were mounted into copper-sheath as shown in **Fig.1.** 

The bulk density of sintered tip was measured from the weight and length of tips using an electric balance and a micro-meter.

## 2.2 Electrode consumption measurement

The consumption test was carried out by generating an arc discharge between electrode tip and water cooled

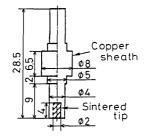


Fig.1 Shape of tentative electrode.

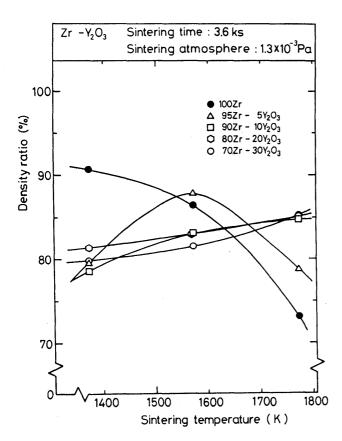


Fig.2 Relationship between sintering temperature and density ratio of Zr-Y<sub>2</sub>O<sub>3</sub> system.

copper anode for 0.3ks at 25A using compressed air as operating gas.

The electrode consumption was estimated by weighing an electrode before and after the test using an electric balance with sensitivity of  $10^{-5}$ g.

# 2.3 Observation of appearance and cross section of electrode

The observation of eroded appearance and cross section were carried out by low-powered microscope in order to confirm an eroding process of electrodes with different  $Y_2O_3$ -mixing ratio and sintering temperature.

#### 3. Experimental Results

## 3.1 Density ratio of sintered tip

## 3.1.1 $Zr-Y_2O_3$ system

The relationship between a sintering temperature (at 1373K, 1573K and 1773k) and density ratio of sintered  $Zr-Y_2O_3$  system is shown in **Fig.2.** In case of 100%Zr, the density ratio decreased with increasing a sintering temperature from 1373K to 1773K. On the other hand, density ratio of Zr including  $Y_2O_3$  increased slightly except of 95Zr-5 $Y_2O_3$ .

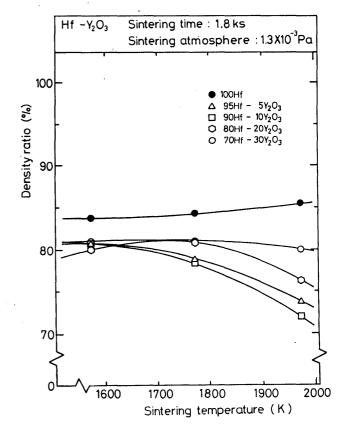


Fig.3 Relationship between sintering temperature density ratio of  $Hf-Y_2O_3$  system.

#### 3.1.2 $Hf-Y_2O_3$ system

The relationship between a sintering temperature (at 1573K, 1773K and 1973K) and density ratio of sintered  $Hf-Y_2O_3$  system is shown in **Fig.3**. In the case of 100%Hf, the density ratio slightly increased with increasing a sintering temperature from 1573K to 1973K and reached about 84% or over in all specimens. On the other hand, in case of  $Hf-Y_2O_3$  system, the density ratio decreased with raising the sintering temperature. Maximum density ratio of 82% was obtained with  $70Hf-30Y_2O_3$  at 1573K. In this system, the addition of  $Y_2O_3$  has no effect on increasing the density of sintering tip.

## $3.1.3 Ru-Y_2O_3$ system

The relationship between the sintering temperature and the bulk density of sintered Ru-Y<sub>2</sub>O<sub>3</sub> system is shown in **Fig.4.** The density ratio of all specimens increased with raising the sintering temperature from 1573k to 2373K. Densification rate  $\rho$  (%) is defined as following,

$$\rho \, (\%) = \frac{(D_{r2} - D_{r1})}{D_c} \times 100$$

where,  $D_{r2}$ : Density at 2373K,  $D_{r1}$ : Density at 1573K,  $D_c$ : Theoretical density.

Densification rate  $\rho$  (%) are 6.7% for 100%Ru, 19.4% for 90Ru-10Y<sub>2</sub>O<sub>3</sub>, and 28.7% for 70Ru-30Y<sub>2</sub>O<sub>3</sub>. The densification rate increased with Y<sub>2</sub>O<sub>3</sub> addition. 70Ru-

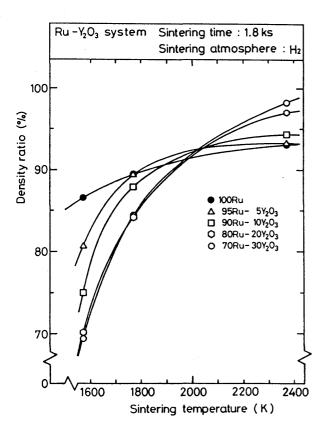


Fig.4 Relationship between sintering temperature and density ratio of Ru-Y<sub>2</sub>O<sub>3</sub> system.

 $30Y_2O_3$  sintered at 1573K showed the lowest density in this series, and the density ratio increased from 69.4% (at 1573K) to 98.2% (at 2373K), that was the maximum densification rate of all specimens.

#### 3.2 Characteristics of electrode consumption

## 3.2.1 $Zr-Y_2O_3$ electrode

The relationship between an electrode weight loss (consumption) and a sintering temperature of  $Zr-Y_2O_3$  system is shown in Fig.5. For both 100%Zr and Zr including  $Y_2O_3$  electrodes, the consumption increased with raising a sintering temperature. In the case of 100%Zr, the weight loss increased rapidly in the range between 1573K and 1773K of sintering temperature. It may be considered that the pore growth might take place because of high sintering temperature shown in Fig.2.

 $90Zr-10Y_2O_3$  sintered at 1373K showed a minimum weight loss of about 0.1mg in this series. The weight loss of  $90Zr-10Y_2O_3$  was nearly equal to that of  $80Ru-20Y_2O_3$ , which showed a good erosion resistance.

## 3.2.2 Hf-Y<sub>2</sub>O<sub>3</sub> electrode

The relationship between an electrode weight loss and a sintering temperature of  $Hf-Y_2O_3$  system is shown in **Fig.6.** In the case of 100%Hf, the minimum weight loss (0.4mg) was given by the electrode sintered at 1773K.

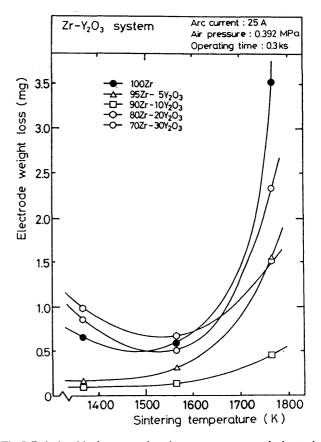


Fig.5 Relationship between sintering temperature and electrode weight loss of Zr-Y<sub>2</sub>O<sub>3</sub> system.

And in case of Hf- $Y_2O_3$  system, the weight loss increased with increasing a sintering temperature except of 90Hf- $10Y_2O_3$ .

The electrode with higher content of  $Y_2O_3$  (20 and 30wt%) showed an extreme consumption in the case of high sintering temperature (1973K). It may be attributed to the decrease of the thermal and electrical conductivity due to the increased volume fraction of  $Y_2O_3$ , and having a low conductivity rather than metals.

Hafnium oxide was formed tightly on the electrode surface after test. This formation of oxide has some influence on the measurement of an electrode weight loss. Hf including  $Y_2O_3$  was eroded severely rather than Zr including  $Y_2O_3$ .

The addition of Y<sub>2</sub>O<sub>3</sub> to Hf has no effect on the improvement of erosion resistance.

## 3.2.3 Ru-Y<sub>2</sub>O<sub>3</sub> electrode

The relationship between electrode weight loss and sintering temperature of Ru- $Y_2O_3$  electrode is shown in **Fig.7.** In case of Ru including  $Y_2O_3$  electrodes, the weight loss decreased rapidly by the use of higher sintering temperature ranging from 1573K to 2373K. In this study the best fabrication conditions to increase the erosion resistance is to mix about 20wt% $Y_2O_3$  and sintering at 2373K. This electrode has a dense structure such as

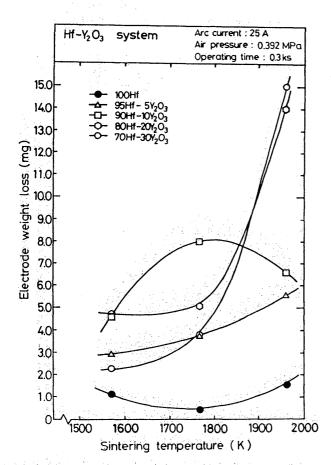


Fig. 6 Relationship between sintering temperature and eletrode weight loss of  $Hf-Y_2O_3$  system.

density ratio of about 90%. Even in case of low sintering temperature like 1573K, the consumption was lower than some others (100Zr or 100Hf). It may be considered that the combination of Ru and  $Y_2O_3$  is satisfactory for plasma cutting electrode using in air.

# 3.3 Observation of appearance and cross section of electrodes

## 3.3.1 $Zr-Y_2O_3$ electrode

Figure 8 shows the eroded appearance of 100%Zr and Zr-Y<sub>2</sub>O<sub>3</sub> electrodes surface at different sintering temperature, after operating in air at 25A for 0.3ks. It is clear that: (1) in case of 100%Zr, the eroded area limited in the central parts of the tip. (2) It might be due to the high operating temperature by lower heat conduction, which is attributable to generating pores by unsuitable sintering temperature.

## 3.3.2 Hf-Y<sub>2</sub>O<sub>3</sub> electrode

**Figure 9** shows the eroded appearances of 100%Hf and Hf-Y<sub>2</sub>O<sub>3</sub> electrode surface at different sintering temperature, after operating under same condition as in the case of Zr-Y<sub>2</sub>O<sub>3</sub>. Appearance of electrode were also very similar to that in case of Zr-Y<sub>2</sub>O<sub>3</sub> system. In case of 100%Hf, the erosion limited inside the sintered tip, showed a good erosion resistance rather than the other electrode in this system. In case of Hf including Y<sub>2</sub>O<sub>3</sub>, the erosion

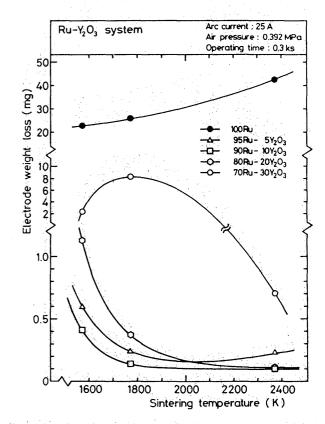


Fig.7 Relationship between sintering temperature and eletrode weight loss of Ru-Y<sub>2</sub>O<sub>3</sub> system.

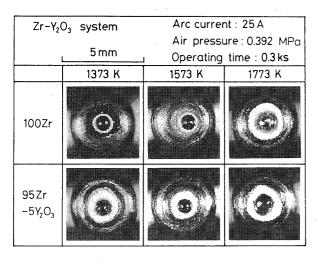


Fig.8 Appearance of  $Zr-Y_2O_3$  system electrodes after test (25A, 0.3ks).

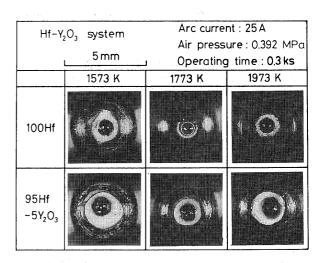


Fig.9 Appearance of Hf-Y<sub>2</sub>O<sub>3</sub> system electrodes after test (25A, 0.3ks).

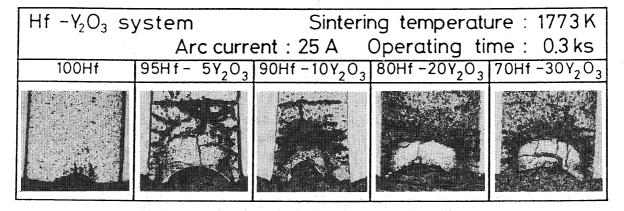


Fig.10 Cross section of Hf-Y<sub>2</sub>O<sub>3</sub> system electrodes after test (25A, 0.3ks).

Ru-Y	<sub>2</sub> O <sub>3</sub> system 5 mm	Arc current : 25 A Air pressure : 0.392 MPa Deperating time : 0.3 ks				
	1573 K	1773 K	2373 K			
100Ru						
95Ru -5Y <sub>2</sub> O <sub>3</sub>						

Fig.11 Appearance of Ru-Y<sub>2</sub>O<sub>3</sub> system electrodes after test (25A, 0.3ks).

extendend to copper sheath and Hafnium oxide was formed and covered on an eroded surface.

Figure 10 shows the electrode cross section of Hf-Y<sub>2</sub>O<sub>3</sub> electrodes sintered at 1773K. It may be said that the erosion or consumption of an electrode was progressed as

a semi-spherical wall which was formed at the center of the tip. The size of eroded wall was very small in 100% Hf, but in 95Hf-5Y<sub>2</sub>O<sub>3</sub> the size of eroded wall was large and its depth increased with increasing the content of Y<sub>2</sub>O<sub>3</sub>.

## 3.3.3 Ru- $Y_2O_3$ electrode

Figure 11 shows the eroded appearances of eroded surface in  $Ru-Y_2O_3$  electrode at several sintering temperatures. In case of 100%Ru, the electrode tip was completely damage and the erosion area extented to copper sheath. In case of Ru including  $Y_2O_3$ , the consumption was very low and the eroded wall was limited in the central parts of electrode tip. From the investigation of the electrode cross section sintered at 2373K, it is clearly observed the remarkable effect of  $Y_2O_3$  addition on decreasing electrode erosion contrary to the case of Hf and its additional effect of  $Y_2O_3$  as shown in Fig.12.

## 4. Conclusions

This study was made to explain the effect of sintering

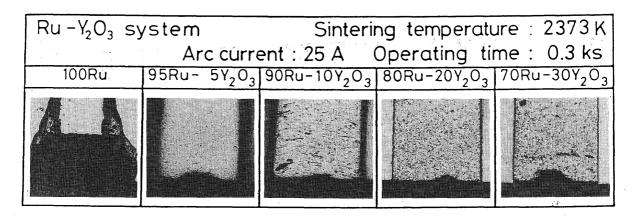


Fig.12 Cross section of Ru-Y<sub>2</sub>O<sub>3</sub> system electrodes after test (25A, 0.3ks).

temperatures on the electrode consumption in the case of  $Zr-Y_2O_3$ ,  $Hf-Y_2O_3$  and  $Ru-Y_2O_3$  systems for air plasma cathode.

The main conclusions drawn from this study are as follwos:

- (1) In 100%Zr, the electrode consumption increase with decreaseing a density by higher sintering temperature like at 1773K. In Zr including 5 ~ 30wt%Y₂O₃, the consumption is lower rather than in the case of 100%Zr. But in fact the oxide is formed on the eroded surface which is wide comparing with that of 100%Zr.
- (2) In 100%Hf, the electrode consumption is hardly affected by increasing the sintering temperature from 1573K to 1973K. In case of Hf including  $5 \sim 30 \text{wt}\% Y_2 O_3$ , the erosion resistance is not improved at any sintering temperatures.
- (3) In Ru including  $5 \sim 30 \text{wt} \% Y_2 O_3$ , the electrode consumption is extremely reduced comparing with

that in the case of 100%Ru under all sintering temperatures. And this effect is hardly affected by increasing the sintering temperature from 1573K to 2373K. Small addition of  $Y_2O_3$  in Ru improve remarkably the erosion resistance, contrary to the case of  $Y_2O_3$  addition to Hf and Zr.

## Acknowledgements

The authors would like to express their appreciation to TOHO KINZOKU CO., for the production of many kinds of electrodes.

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