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Citation	Transactions of JWRI. 1983, 12(2), p. 327-328
Version Type	VoR
URL	<a href="https://doi.org/10.18910/7088">https://doi.org/10.18910/7088</a>
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# Pulsed CO<sub>2</sub> Arc Welding†

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KEY WORDS: (Pulsed Arc Welding) (Pulse Welding) (CO<sub>2</sub> Welding) (Arc Welding) (Spattering) (Metal Transfer)

CO<sub>2</sub> arc welding of solid wire has a great disadvantage, the spattering, under the condition of medium welding current. Various types of mechanism are considered to be attributable to the occurrence of spattering in CO<sub>2</sub> arc welding. Among them, the spattering occurring at the wire end or in the arc space can be ascribed to two categories of mechanism. They are excess heating of the droplet and magnetic effect due to the bending of current path. These spattering could be extremely reduced by

applying the pulsed current under the open arc condition.

The work described here verifies the existence of preferable condition of pulsed current for CO<sub>2</sub> arc welding, which enables to reduce the spattering loss extremely by using the transfer mode of one droplet transfer in one cycle of pulsed current.

Figure 1 shows an example of droplet transfer behavior in the pulsed CO<sub>2</sub> arc welding. The figures of arc and droplet are sampled from the high speed cinefilms. This

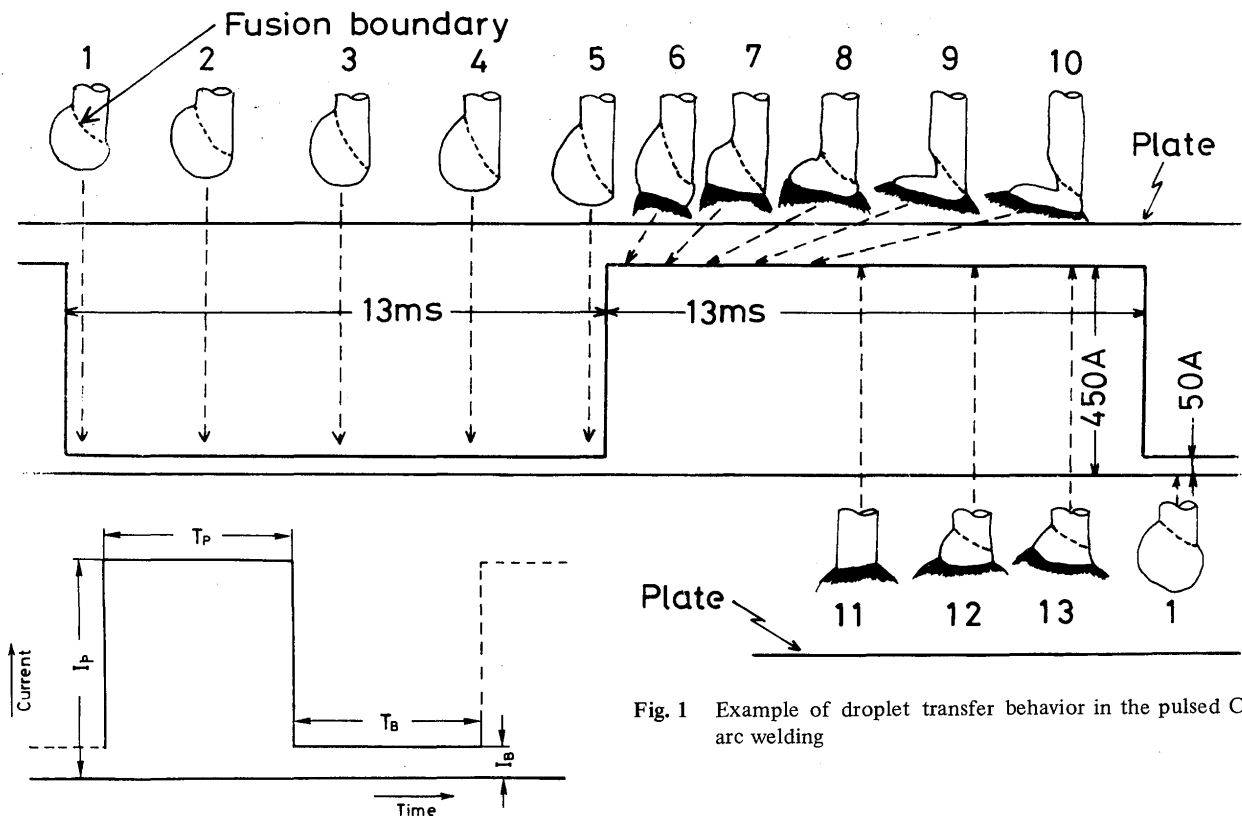


Fig. 1 Example of droplet transfer behavior in the pulsed CO<sub>2</sub> arc welding

† Received on October 31, 1983

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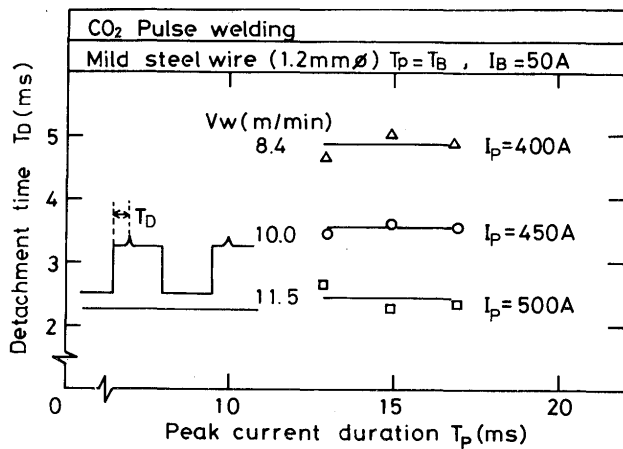


Fig. 2 Relation between  $T_p$  and detachment time  $T_D$  under condition of one droplet transfer per one pulse

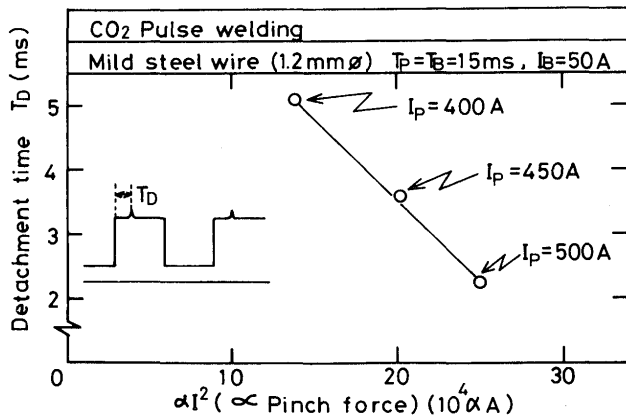


Fig. 3 Relation between pinch force ( $\propto I^2$ ) and detachment time  $T_D$

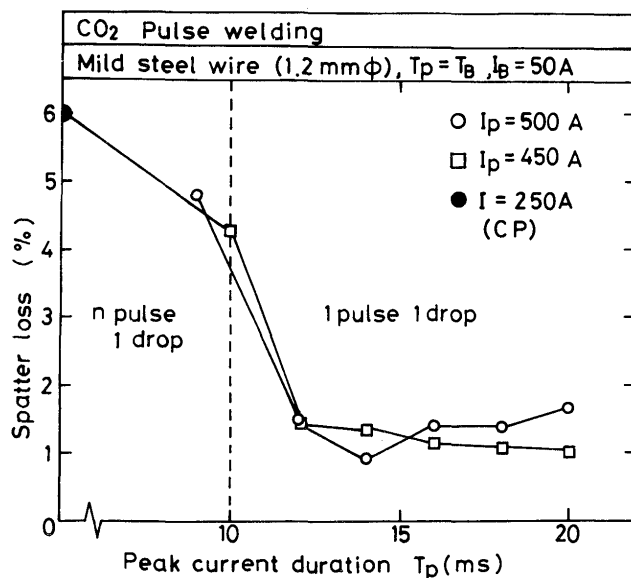


Fig. 4 Reduction of spatter loss by use of  $\text{CO}_2$  pulsed welding

metal transfer phenomena is different from the one of pulsed MAG or MIG welding. The droplet detaches regularly only in the early stage of higher current phase  $T_p$ . After detachment of droplet, the wire is melted continuously and large molten droplet is formed at the end of wire. This droplet is pushed up along the wire due to the strong arc force in  $T_p$  phase, but in  $T_B$  phase it begins to slide downward due to the decrease of arc force and it is hung on the wire end. As restarting the pulsed current, it rapidly detaches from the wire and is transferred to the puddle. This is the one droplet transfer in one cycle of pulsed current.

Figure 2 shows the relation between the  $T_p$  and the detachment time  $T_D$  under the condition of one droplet transfer per one pulse. The detachment time  $T_D$  means the time required for detaching from the beginning of pulsed current as shown in Fig. 1. This results show the time duration of pulsed current  $T_p$  has no effect on  $T_D$ . Even if long  $T_p$  should be applied for a  $I_p$  value, the detachment time  $T_D$  will be constant. It suggests the detaching has a strong dependence on  $I_p$  value and not on the volume of droplet.

Figure 3 shows the relation between the pinch force ( $\propto I^2$ ) and the detachment time  $T_D$ . This shows the detaching is mainly due to the pinch force.

Figure 4 shows the reduction of spatter loss by the use of  $\text{CO}_2$  pulsed welding. By adjusting the pulse condition to the one droplet transfer mode, the spattering losses are extremely reduced. The ratio of spattering loss of pulsed  $\text{CO}_2$  arc welding to the one of ordinarily used  $\text{CO}_2$  arc welding reaches to 1/5 in the optimum condition.