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# Long-term Stability of Nickel-based Ohmic Contacts with n-type and p-type 4H-SiC in a High-temperature Environment

Masahiro Masunaga<sup>1,2\*</sup>, Viviana Crescitelli<sup>2</sup>, and Tsuyoshi Funaki<sup>1</sup>

<sup>1</sup>*Division of Electrical, Electronic and Information Engineering, Graduate School of Engineering, Funaki Laboratory, Osaka University, 2-1 Yamadaoka, Suita, Osaka 565-0871, Japan*

<sup>2</sup>*Center for Technology Innovation – Electronics, Research & Development Group, Hitachi, Ltd., 1-280 Higashi-koigakubo, Kokubunji-shi, Tokyo 185-8601, Japan*

\*E-mail: masahiro.masunaga.fw@hitachi.com

## Abstract

Long-term thermal stability of specific contact resistance ( $\rho_c$ ) in cross-bridge kelvin resistors (CBKR), with an Al/TiN/Ti/Ni<sub>2</sub>Si/4H-SiC layered structure was studied. In high-temperature-storage tests at 500°C,  $\rho_c$  of p-type SiC increased after it decreased to 1/100 from its initial value; however, in high-temperature-storage tests at 300°C, it was stable up to 1000 hr. The initial decline of  $\rho_c$  was due to formation of titanium-silicide alloy, whose barrier height is lower than that of Ni<sub>2</sub>Si phase. It was found that  $\rho_c$  increased when the aluminum electrode disappeared because aluminum displaced silicon in the silicon-dioxide layer. In thermal-shock tests (-40°C/300°C),  $\rho_c$  hardly changed up to 2000 cycles, and that trend was constant regardless of SiC carrier type. In both tests, almost no thermal deterioration of  $\rho_c$  around 300°C was observed even in air, so it is concluded that the CBKR structure is robust enough for installation in a high-temperature environment such as a nuclear power plant under decommissioning.

## 1. Introduction

Power devices and sensors are indispensable for operation, control, and safety of robots used in decommissioning nuclear power plants. Silicon (Si)-based devices are conventionally used for actuator drivers and sensors. However, they are susceptible to radiation and high temperature, so they require extra measures for normal operation (such as shielding or protection circuits).

Silicon-carbide (SiC) is a promising semiconductor material for devices operating in high-radiation<sup>1-7)</sup> and high-temperature<sup>8-13)</sup> environments. In a previous work, the authors fabricated a SiC operational amplifier (op-amp) based on 4H-SiC complementary MOS (CMOS) technology<sup>6)</sup>. The developed device showed superior radiation resistance (over 1 MGy), without use of a shield or an external process such as thermal annealing, due to significantly decreased interface state density of the 4H-SiC MOS with nitric-oxide (NO) passivation<sup>5)</sup>. The operation of SiC-CMOS integrated circuits in high-temperature environments has been demonstrated<sup>14-16)</sup>. The experimentally demonstrated long-term reliability of a gate-oxide film suggested a maximum operating electric field of 3.9 MV/cm for a 100-year lifetime at 375°C<sup>17)</sup>.

However, a contact metal and capping layer with high temperature resistance (at 300°C or more) suitable for SiC-CMOS has not been sufficiently studied. Nickel (Ni) has been frequently studied as a contact metal for n-type SiC<sup>18-21)</sup>, and its barrier height ( $\phi_B$ ) is known to decrease from 1.60 eV to 0.45 eV after annealing at over 900°C<sup>21,22)</sup>. This ohmic behavior can be mainly attributed to (i) formation of a silicide such as Ni<sub>2</sub>Si and/or (ii) redistribution of interfacial carbon after the silicide formation and its movement from the interface towards the contact surface at elevated temperature<sup>20)</sup>. Also, some researchers consider that carbon vacancies are generated from outdiffusion of carbon atoms at the interface during annealing, and those carbon vacancies act as donors that play a key role in reducing effective  $\phi_B$  and promoting formation of ohmic contacts<sup>19)</sup>. Stacked titanium and aluminum has been studied as contact metal for p-type SiC<sup>23-25)</sup>. Interface alloys such as Al<sub>3</sub>Ti and Ti<sub>3</sub>SiC<sub>2</sub> are produced at the interface between the titanium/aluminum metal stack and the p-type SiC during high-temperature annealing, and the Ti<sub>3</sub>SiC<sub>2</sub> divides the high  $\phi_B$  of the metal/p-type SiC contact interface into two low  $\phi_B$  to reduce  $\rho_c$ <sup>25,26)</sup>. Because of that fact, it is desirable to apply different contact metals to n-type and p-type SiC, although the CMOS manufacturing process becomes complicated.

Forming ohmic contacts to both n-type and p-type regions by the same process has been studied in the CMOS fabrication<sup>27-32)</sup>. Linear-transmission-line-model samples, which have

Ni-based ohmic contacts to implanted n-type and p-type SiC, showed  $\rho_c$  in the range of  $10^{-6} \Omega\text{cm}^2$  and  $10^{-3} \Omega\text{cm}^2$ , respectively at room temperature<sup>31)</sup>. Furthermore, the samples demonstrated high thermal stability in nitrogen atmosphere<sup>32)</sup>. However, in these studies, oxidation of the contacts in air was not considered. Contact resistance increased 10 times from the initial value in air at 300°C for a device with Ni-based ohmic contacts<sup>33)</sup>.

To address the oxidation issue, a conductive diffusion barrier that can prevent diffusion of oxygen into the contact metal has been suggested<sup>34-39)</sup>. A conductive diffusion barrier, such as TaRuN<sup>36,37)</sup> and TiN<sup>38,39)</sup>, is formed between the contact metal and the capping layer to slow the diffusion of oxygen and/or the reaction of oxygen with the contact metal and capping layer. The experimentally demonstrated performance of conductive diffusion barrier with TaRuN changed contact resistance only slightly from  $2 \times 10^{-5} \Omega\text{cm}^2$  to  $3 \times 10^{-5} \Omega\text{cm}^2$  for 2000 hr in air over 300°C<sup>36)</sup>. However, patterning the noble metals such as ruthenium in CMOS processing is not straightforward, and substitution to TiN is desired. In addition, although thermal stability of these stacked structures have been studied frequently, the influence of delamination caused by Kirkendall voids, which are formed at the interface between a Ni-based contact and the SiC substrate<sup>40)</sup>, has not been sufficiently verified.

This study subjects 4H-SiC cross-bridge kelvin resistors (CBKRs), with an Al/TiN/Ti/Ni silicide/4H-SiC layered structure, to a high-temperature-storage test in air and a specific environment. And this study subjects to a thermal-shock test to verify  $\rho_c$  fluctuation due to delamination of contact metals. To check deterioration of the interface,  $\rho_c$  in the case of implanted n-type and p-type SiC layer is periodically sampled.

## 2. Experimental methods

The CBKR samples (NN05 and PP10) investigated in this work were fabricated in-house as n-type and p-type semiconductors, respectively. Their detailed specifications are listed in Table I. Plan views and cross sections of NN05 and PP10 are shown in Figs. 1 and 2, respectively. The samples were monolithically fabricated on an n-type 4H-SiC epitaxial layer doped with nitrogen at  $7 \times 10^{14} \text{ cm}^{-3}$  and grown on a 4H-SiC substrate that was 4° off the silicon face. Acceptor concentration of a p-well in NN05 ( $3.6 \times 10^{17} \text{ cm}^{-3}$ ) was formed by aluminum implantation. An n+ layer in NN05 and a p+ layer in PP10 were formed by ion implantation. The ion species was nitrogen for n-type and aluminum for p-type. After the impurities were implanted, the samples were activated by annealing at 1700°C. Then, a silicon-dioxide (SiO<sub>2</sub>) interlayer was deposited on the SiC epitaxial surface by chemical vapor deposition, and the CKBR patterns were formed with a photoresist. After a part of the

SiO<sub>2</sub> interlayer was removed, the exposed surface of the 4H-SiC epitaxial layer was cleaned by buffered hydrofluoric acid. A 55-nm-thick nickel layer deposited on the exposed surface was annealed at 1000°C for silicidation. Titanium (10 nm), TiN (30 nm), and aluminum (300 nm) films were deposited on the nickel-silicide layer by sputtering as an adhesion-promoting layer, a conductive diffusion barrier and a capping layer, respectively. Finally, a SiO<sub>2</sub> layer was formed to passivate them, and  $\rho_c$  of the fabricated samples was measured with a precision semiconductor parameter analyzer (4156B, Keysight Technologies, Inc.). The basic experimental setup for the measurement is shown in Fig. 2(a), and  $\rho_c$  was measured by four-terminal Kelvin sensing with the current measured at “source-measurement unit 1” (SMU1) and the difference between voltages measured at “voltage-meter unit 1” (VMU1) and VMU2 as shown in Fig. 3.  $\rho_c$  was average of contact resistance from -1 V to 1 V except 0 V, and temperature dependence of  $\rho_c$  in the range 25–500°C was studied.

The high-temperature-storage-test samples were heated in specific environments (400°C and 500°C) in an electric furnace (DD-93000C, Kokusai Electric co., Ltd.) filled with nitrogen gas or at 300°C in a vacuum chamber (ZXVC-10150HT, Vector Semiconductor co., Ltd.). All the samples were tested in wafer state. Specific contact resistance ( $\rho_c$ ) of the samples heated at 400°C and 500°C test was periodically sampled at room temperature by taking the samples out of the electric furnace. In contrast,  $\rho_c$  of the sample heated at 300°C test was continuously measured by probe in the vacuum chamber for 1000 hr.

Long-term thermal stability of CBKR in air was evaluated using the samples, which were attached to a ceramic package, as shown in Fig. 4, with gold-germanium solder to withstand extreme temperature storage and temperature change of the thermal-shock test<sup>41)</sup>. The sample and terminals of the ceramic package were connected by aluminum wires. The samples subjected to thermal-shock tests at temperature difference ( $\Delta T$ ) of 340°C for 2000 cycles were set in a thermal-shock chamber (TSE-11, Espec corp.) with a temperature range of -40°C to 300°C. The temperature sequence—in which the temperature was transitioned at higher than 68°C per minute—is shown in Fig. 5.

Before the thermal-shock test, peel strength of the aluminum wires was tested by bond tester (Condor Sigma, XYZTEC, Inc.). The normal distribution of the wire's peel fracture strength before and after the thermal-shock test is shown in Fig. 6. It is clear from the figure that the wire's peel fracture strength is significantly decreased by metal fatigue. However, all tested wires (20 in total) keep contacts and their mechanical strengths were over 0.92 gf for 2000 cycles. The influence of wire-bond deterioration on  $\rho_c$  is negligible for 2000 cycles.

### 3. Results and discussion

#### 3.1 Temperature dependence of contact resistance

Before high-temperature storage tests, as temperature dependence of  $\rho_c$  for NN05 and PP10 are shown in Figs. 7(a) and 7(b). Specific contact resistance ( $\rho_c$ ) of NN05 stays in the range of  $10^{-6} \Omega\text{cm}^2$  up to  $500^\circ\text{C}$ . In contrast,  $\rho_c$  of PP10 fluctuates in the range from  $10^{-2} \Omega\text{cm}^2$  at  $25^\circ\text{C}$  to  $10^{-4} \Omega\text{cm}^2$  at  $500^\circ\text{C}$ . The difference in temperature dependences of  $\rho_c$  between NN05 and PP10 indicates different mechanism in carrier transport at the interface. The carrier-transport mechanism is related to the Padovani-Stratton parameter ( $E_{00}$ )<sup>26,34</sup> and depends on both temperature and doping level. Ratio  $E_{00}/kT$  (where  $k$  is the Boltzmann constant and  $T$  is temperature) indicates the carrier transport for which a specific current-flow mechanism plays the dominant role<sup>26,34</sup>.

According to ratio  $E_{00}/kT$ , carrier transport of NN05 is governed by a field-emission (FE) model. The extracted value of  $\phi_B$  is 0.5 eV, which agrees with its value of  $\text{Ni}_2\text{Si}$  contact to n-type SiC under a similar implantation and annealing condition<sup>32</sup>. On the other hand, carrier transport of PP10 is governed by a thermionic-field-emission (TFE) model, and the value of  $\phi_B$  is calculated as 1.1 eV, which is 0.35 eV higher than that of the reported  $\text{Ni}_2\text{Si}$  contact to p-type SiC<sup>32</sup>. For p-type material,  $\phi_B$  is often found to be independent of the metal work function and is related to the density of interface states ( $D_{it}$ )<sup>26,48,49</sup>.  $\phi_B$  for p-type material ( $\phi_{BP}$ ) can be derived approximately based on Bardeen model as<sup>26,48,49</sup>

$$\phi_{BP} = -\gamma(\phi_m - \chi) - (1 - \gamma)(E_g - \phi_0) + E_g \quad (1)$$

where  $\gamma$  is the pinning factor related to the  $D_{it}$ ,  $\phi_0$  is the charge-neutrality level,  $\phi_m$  is work function of metal,  $\chi$  is the electron affinity of SiC, and  $E_g$  is band gap.  $\gamma$  ranges from 0 to 1. Sufficiently high  $D_{it}$  ( $\gamma$  is close to 0) induces Fermi level pinned at the  $\phi_0$  in the band gap, and it reduces contact resistance<sup>26,42</sup>. On one hand, at low  $D_{it}$ , the  $\phi_{BP}$  subjects to Schottky-Mott model<sup>26</sup>. Thus,  $D_{it}$  is key factor for  $\phi_{BP}$ . However,  $D_{it}$  is known to be strongly influenced by surface treatments prior to SiC metalization<sup>26</sup>. It is considered that the difference of surface pretreatments made the difference in  $\phi_{BP}$  in this case.

The constitution of contact metal in the PP10 sample was analyzed by XRD (X-ray diffraction). The result of XRD is shown in Fig. 8. In the PP10 sample, the  $\text{Ni}_2\text{Si}$  phase was formed at the metal/SiC interface.

#### 3.2 High-temperature-storage test in specific environments

Specific contact resistance ( $\rho_c$ ) of NN05 and PP10 was investigated to evaluate the

deterioration of the interface between the contact metal and SiC layer in the high-temperature-storage test. The high-temperature-storage test was performed in vacuum or nitrogen atmosphere to exclude the influence of oxidation.  $\rho_c$  of NN05 and PP10 for storage time is plotted in Figs. 9(a) and 9(b), respectively. Note that  $\rho_c$  of NN05 stored at 300°C in the aging-time range of 450 to 600 hr was lost due to probing error. And  $\rho_c$  of NN05 stored at 500°C monotonically increases until 575 hr, even though it hardly changes in the 300°C and 400°C storage tests. On the contrary,  $\rho_c$  of PP10 shows a different thermal property from that of NN05 as in Fig. 9(b). That is,  $\rho_c$  of PP10 stored at 500°C increases after it decreased to 1/100 of its initial value.

The cross-section of PP10 was observed to investigate the cause of the large variation of  $\rho_c$ . TEM images before and after the 500°C storage test are shown in Figs. 10(a) and 10(b), respectively. Ni<sub>2</sub>Si, titanium, and TiN were present between the aluminum electrode and SiC layer in the initial state as shown in Fig 10(a). SiO<sub>2</sub> was present on the aluminum electrode as a passivation layer. Carbon clusters agglomerated in the Ni<sub>2</sub>Si layer far from interface. After the 500°C/575 hr storage test, the aluminum electrode disappeared or a part of it became discolored as shown in Fig. 10(b). In addition, the SiO<sub>2</sub> layer appeared to be deformed. The condition of the Ni<sub>2</sub>Si phase between the TiN and the SiC layers was also changed during the high-temperature storage test; that is, the carbon clusters disappeared.

The elemental analysis was performed at points 1, 2, and 3 in Fig. 10(b). Results of TEM-EDX at points 1, 2, and 3 are shown in Figs. 11, 12, and 13, respectively. It is noted for Ga peaks is caused by ion source of focused ion beam (FIB), and Cu peaks is caused by our sample holder. The predominant aluminum and oxygen peaks are found for point 1. Aluminum is known to displace silicon in the SiO<sub>2</sub> structure and form an Al-O compound with Al:O concentration ratio between 1:1 and 1.3:1 at temperature near 500°C<sup>43</sup>). Furthermore, this displacement reaction penetrates deeply into the SiO<sub>2</sub> structure without a noticeable change in the rate of penetration<sup>43</sup>). In other words, the aluminum electrode steadily disappeared via a solid-state chemical reaction with high-temperature-storage time, and  $\rho_c$  gradually increased simultaneously.

The predominant silicon and titanium peaks, as well as subordinate nitrogen, aluminum, and carbon peaks, are found (although nickel is not detected) for point 2. This result indicates a chemical reaction in silicide from Ni<sub>2</sub>Si phase to titanium-silicide alloy. It also shows aluminum atoms slightly penetrate into the silicide layer through TiN. From  $\rho_c$  in Fig. 9(b),  $\phi_B$  of the titanium-silicide alloy is estimated as 0.82 eV, which agrees with  $\phi_B$  of the titanium-alloy contact to p-type SiC<sup>44</sup>). In the same way, from  $\rho_c$  in Fig. 9(a),  $\phi_B$  of NN05 after the

high-temperature-storage test is estimated as 0.73 eV, which agrees with  $\phi_B$  of the titanium ohmic contact on n-type SiC, which was formed by low-temperature anneal<sup>45)</sup>. Titanium silicide formed below 600°C is mainly composed of  $\text{Ti}_5\text{Si}_4$ ,  $\text{Ti}_5\text{Si}_3$ , and  $\text{TiC}$ <sup>45)</sup>, and these alloys constitute for low ohmic contact to p-type SiC.

The nickel and silicon subordinate peaks are found for point 3 in addition to a predominant aluminum peak, as shown in Fig. 13. The nickel atoms penetrate into the aluminum-layer side (accompanied by silicon atoms) through TiN, and disappeared from the silicide layer during the high-temperature-storage test. An AlSiNi alloy is then formed in the aluminum region.

Thus, Fig. 9(b) can be interpreted as follows. From 0 to 200 hr,  $\text{Ni}_2\text{Si}$  phase transformed to titanium-silicide alloy and  $\rho_c$  was reduced due to reduction of  $\phi_B$ . After that,  $\rho_c$  was increased because the aluminum electrode diffused to  $\text{SiO}_2$  structure and vanished. Same phenomenon is expected to occur in  $\rho_c$  of NN05. In the period from 0 to 200 hr,  $\rho_c$  was increased due to elevation of  $\phi_B$  in n-type material of the titanium-silicide alloy. And then, disappearance of aluminum electrode further increased  $\rho_c$  of NN05.

### 3.3 Long-term thermal stability in air

To investigate deterioration of  $\rho_c$  of NN05 and PP10 by oxidation and delamination, the NN05 and PP10 samples were subjected to high-temperature-storage tests and thermal-shock tests in air. Storage temperature was set in 300°C to suppress  $\rho_c$  variation due to aluminum diffusion from the capping layer and change in the silicide composition. In Fig. 14,  $\rho_c$  of NN05 and PP10 against storage time is plotted. In addition,  $\rho_c$  of a reported device with Ni-based ohmic contact to n-type SiC without the diffusion barrier in Ref. 33 is also shown for comparison. NN05 shows  $\rho_c$  hardly changes up to 1000 hr because TiN prevents diffusion of oxygen into the metal/SiC interface<sup>37)</sup> although  $\rho_c$  of the reported device in Ref. 33 increases 10 times from the initial value. On the other hand,  $\rho_c$  of PP10 at 400 hr becomes 1.7 times larger than the initial value. After 400 hr,  $\rho_c$  saturates. This result agrees with that for  $\rho_c$  in vacuum condition, as shown in Fig. 9(b). It is considered that influence of oxidation in  $\text{Ni}_2\text{Si}$  is negligible because there is no difference in  $\rho_c$  between Fig. 9(b) and Fig. 14.

Increase of  $\rho_c$  in PP10 during the high-temperature-storage test has two main causes: (i) reduction of aluminum concentration at interface and (ii)  $\phi_B$  for p-type material increase due to silicide transformation. A thermally induced interaction between thin-film aluminum and Ni silicide is known to occur at 275°C, and the interaction forms NiAl silicide alloy<sup>46)</sup>.



If the similar phenomenon occurs at the interface, the NiAl silicide alloy is assumed to reduce  $\phi_B$  due to its high work function<sup>47)</sup>. Thus, increase of  $\rho_c$  is likely due to (i), and detailed investigation is our future work.

In Fig. 15,  $\rho_c$  of NN05 and PP10 is plotted for number of thermal-shock cycles. It is clear that  $\rho_c$  after the thermal-shock tests show the same tendency as that shown in Fig. 14. As for NN05,  $\rho_c$  hardly changes up to 2000 cycles, as for PP10,  $\rho_c$  slightly increases up to 1200 cycles and then saturates. The influence of the delamination caused by Kirkendall voids is supposed to be small regardless of carrier type at  $\Delta T = 340^\circ\text{C}$  because  $\rho_c$  variation of NN05 and PP10 is same or small in comparison with it in the high-temperature-storage tests. In other words, the effect of accumulated fatigue by large temperature change at the interface between the metal and SiC layers is negligible.

#### 4. Conclusions

Long-term thermal stability of specific contact resistance ( $\rho_c$ ) in cross-bridge kelvin resistors (composed of Al/TiN/Ti/Ni<sub>2</sub>Si/4H-SiC) at high temperature was studied. In high-temperature-storage tests,  $\rho_c$  for p-type SiC stored at  $500^\circ\text{C}$  increased after it decreased to 1/100 from the initial value, though that increase does not occur for  $300^\circ\text{C}$  storage up to 1000 hr. The initial decline of  $\rho_c$  was due to formation of titanium-silicide alloy, whose barrier height is lower than that of Ni<sub>2</sub>Si. Moreover,  $\rho_c$  increased with disappearance of the aluminum electrode, stemming from aluminum displacement into the silicon-dioxide layer. These results indicate that the aluminum electrode should be changed to a metal one with excellent heat resistance (such as molybdenum) or be covered with a barrier metal for operation at high temperature around  $500^\circ\text{C}$ . They also indicate that switching the silicide material from a nickel-based to a titanium-based one improves thermal stability of  $\rho_c$ . In thermal-shock tests ( $-40^\circ\text{C}/300^\circ\text{C}$ ),  $\rho_c$  hardly changed up to 2000 cycles regardless of SiC carrier type. In both tests, almost no thermal deterioration of  $\rho_c$  around  $300^\circ\text{C}$  was observed even in air, and stable operation of cross-bridge kelvin resistors can be expected up to  $300^\circ\text{C}$ .

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## Figure Captions

**Table I.** (black and white) Specification of contact in cross-bridge kelvin resistors.

**Fig. 1.** (black and white) (a) Plan view of NN05 and (b) cross section of a cross-bridge kelvin resistor.

**Fig. 2.** (black and white) (a) Plan view of PP10 and (b) cross section of a cross-bridge kelvin resistor. Plan view is shown together with basic experimental setup, which is the same for NN05.

**Fig. 3.** (black and white) SMU1 current ( $I_{\text{SMU1}}$ ) and specific contact resistance of NN05 for SMU1 voltage ( $V_{\text{SMU1}}$ ) with SMU2 voltage = 0 V at room temperature.  $\rho_c$  is average of contact resistance from -1 V to 1 V except 0 V.

**Fig. 4.** (black and white) Cross section of a packaged cross-bridge kelvin resistor used for long-term thermal-stability tests in air.

**Fig. 5.** (black and white) Temperature sequence of thermal-shock test.

**Fig. 6.** (black and white) Normal distribution of wire's peel-fracture strength before and after thermal-shock test.

**Fig. 7.** (black and white) Temperature dependence of specific contact resistance  $\rho_c$  for (a) NN05 and (b) PP10 before the high-temperature-storage test. The carrier transport is governed by a field-emission (FE) model in case (a) and by a thermionic-field-emission (TFE) model in case (b).

**Fig. 8.** (black and white) X-ray diffraction spectra of the nickel silicide metal in PP10.

**Fig. 9.** (black and white) Comparison of specific contact resistance  $\rho_c$  for (a) NN05 and (b) PP10 as function of thermal-storage aging time at 300°C in vacuum and 400°C and 500°C in nitrogen atmosphere.  $\rho_c$  of the samples heated at 400°C and 500°C test is periodically sampled at room temperature. In contrast,  $\rho_c$  of the sample heated at 300°C test is continuously measured by probe. Initial  $\rho_c$  of NN05 is  $2.8 \times 10^{-6} \Omega\text{cm}^2$  at room temperature and  $1.7 \times 10^{-6} \Omega\text{cm}^2$  at 300°C. On the other hand, initial  $\rho_c$  of PP10 is  $5.8 \times 10^{-2} \Omega\text{cm}^2$  at room temperature and  $2.1 \times 10^{-3} \Omega\text{cm}^2$  at 300°C.

**Fig. 10.** (color online) TEM images of PP10 (a) before and (b) after high-temperature-storage test at 500°C and aging time of 575 hr in nitrogen atmosphere.

**Fig. 11.** (black and white) (a) TEM-EDX result and (b) enlarged it. These results are at insulator layer after high-temperature-storage test (point 1 in Figure 10(b)).

**Fig. 12.** (black and white) (a) TEM-EDX result and (b) enlarged it. These results are at contact metal after high-temperature-storage test (point 2 in Figure 10(b)).

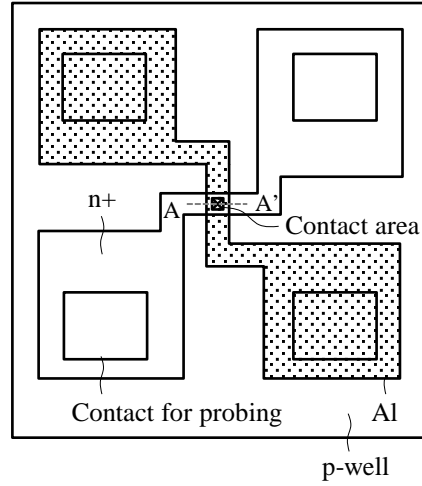
**Fig. 13.** (black and white) (a) TEM-EDX result and (b) enlarged it. These results are at aluminum layer near TiN after the high-temperature-storage test (point 3 in Figure 10(b)).

**Fig. 14.** (black and white) Specific contact resistance  $\rho_c$  of NN05 and PP10 as function of thermal-storage aging time at 300°C in air. Each  $\rho_c$  was measured at room temperature at 200-hr intervals. Reported  $\rho_c$  for a device with Ni-based ohmic contact to n-type SiC is also shown for comparison<sup>33)</sup>. Initial  $\rho_c$  of NN05, PP10 and the device in Ref. 33 are  $2 \times 10^{-5} \Omega\text{cm}^2$ ,  $6 \times 10^{-2} \Omega\text{cm}^2$ , and  $3 \times 10^{-4} \Omega\text{cm}^2$  respectively.

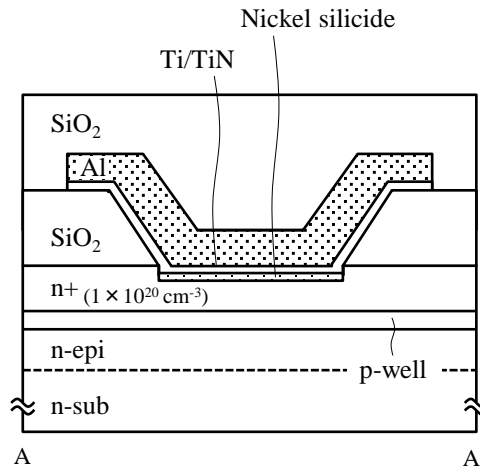
**Fig. 15.** (black and white) Specific contact resistance  $\rho_c$  versus number of thermal-shock cycles for NN05 and PP10 at  $\Delta T = 340^\circ\text{C}$  in air. Each  $\rho_c$  was measured at room temperature at almost-the-same time intervals. Initial  $\rho_c$  of NN05 and PP10 are  $2 \times 10^{-5} \Omega\text{cm}^2$  and  $6 \times 10^{-2} \Omega\text{cm}^2$  respectively.

Table I. (black and white) Specification of contact in cross-bridge kelvin resistors.

name	conduction type	concentration ( $\text{cm}^{-3}$ )	contact area ( $\mu\text{m}$ )
NN05	n-type	$1.0 \times 10^{20}$	$5 \times 5$
PP10	p-type	$0.7 \times 10^{20}$	$10 \times 10$

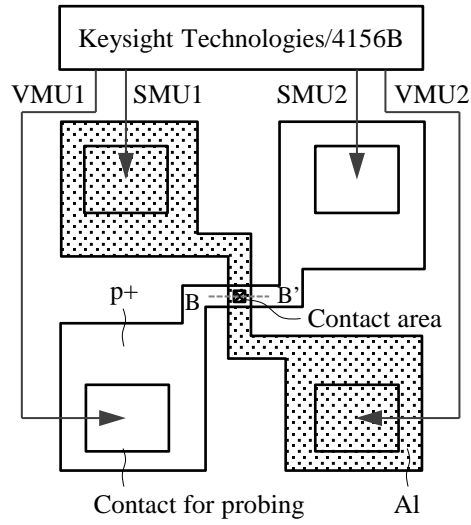


(a)

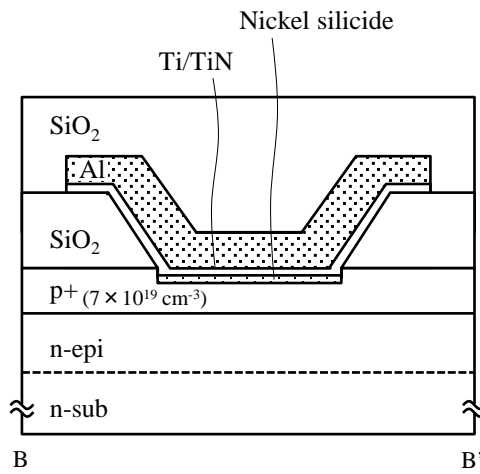


(b)

Fig. 1. (black and white) (a) Plan view of NN05 and (b) cross section of a cross-bridge kelvin resistor.



(a)



(b)

Fig. 2. (black and white) (a) Plan view of PP10 and (b) cross section of a cross-bridge kelvin resistor. Plan view is shown together with basic experimental setup, which is the same for NN05.



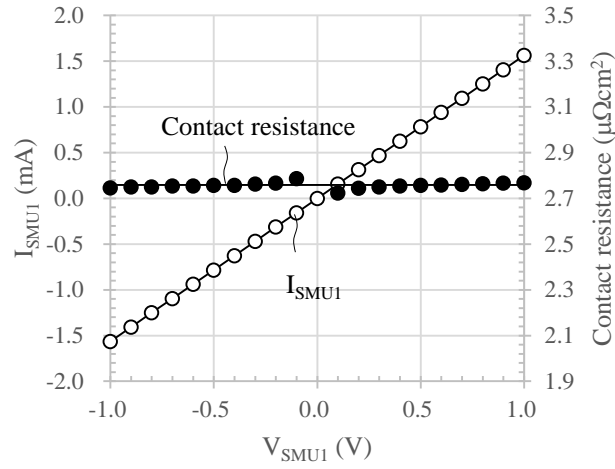


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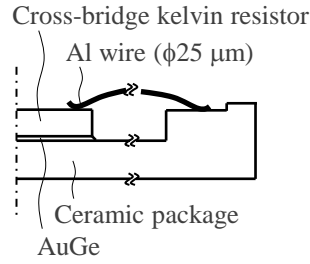


Fig. 4. (black and white) Cross section of a packaged cross-bridge kelvin resistor used for long-term thermal-stability tests in air.

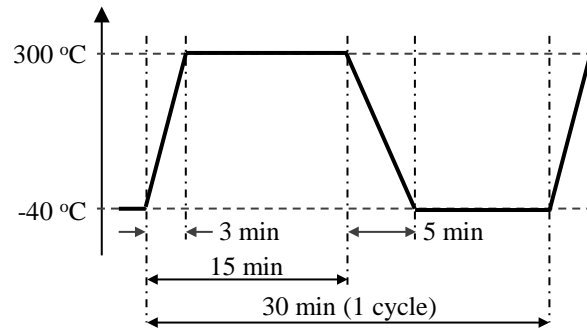


Fig. 5. (black and white) Temperature sequence of thermal-shock test.

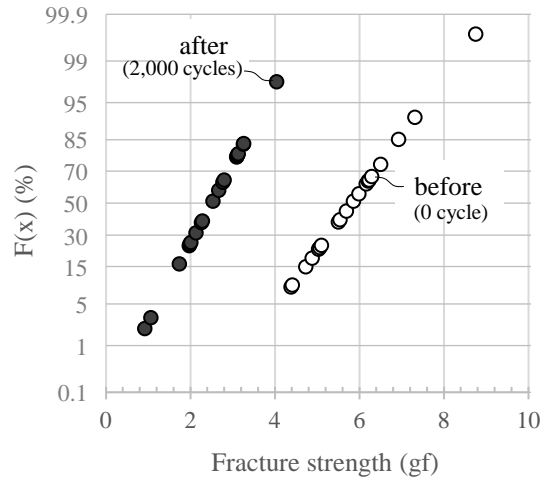


Fig. 6. (black and white) Normal distribution of wire's peel-fracture strength before and after thermal-shock test.

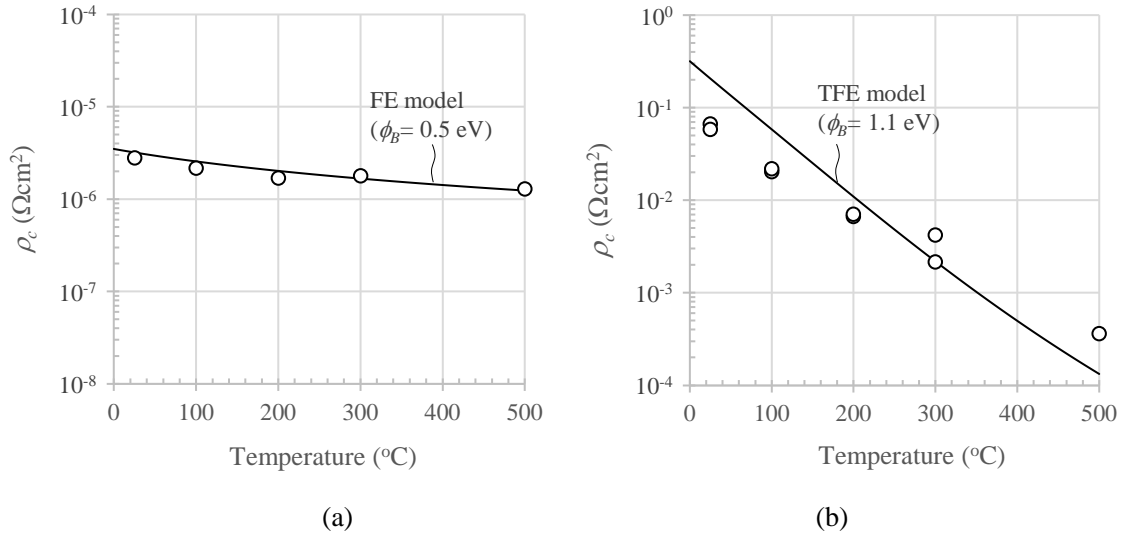


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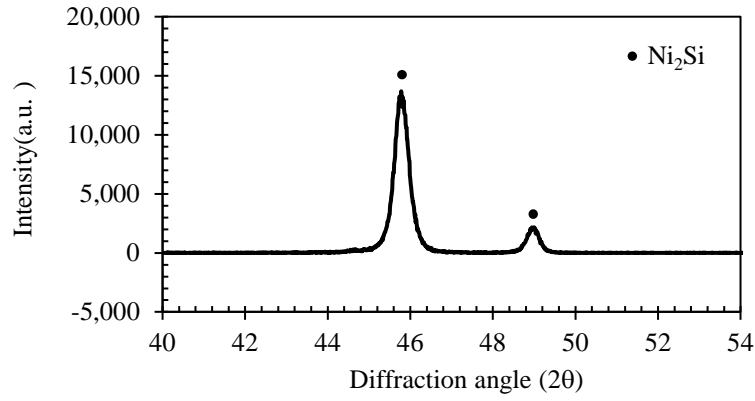


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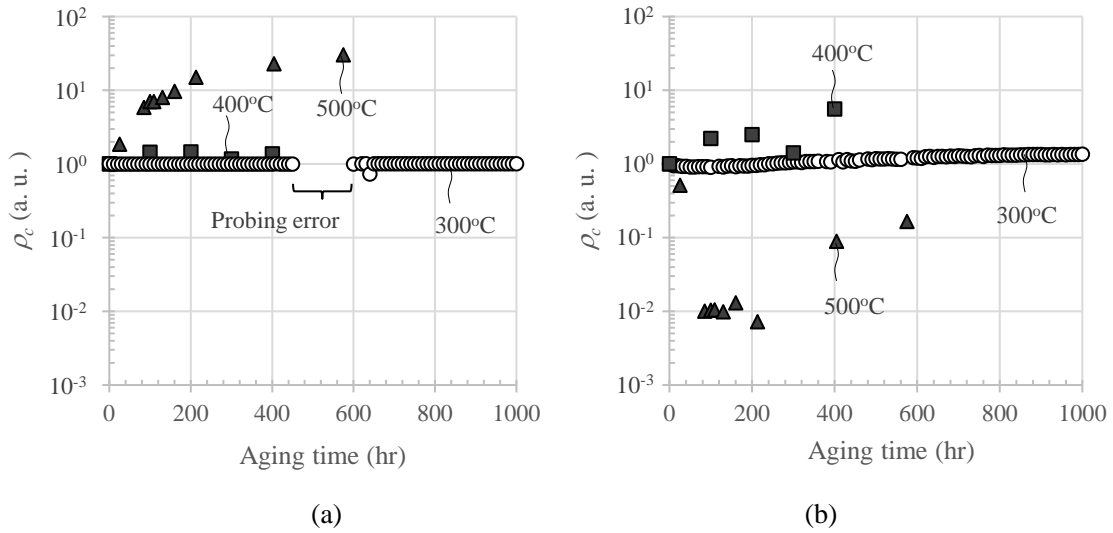


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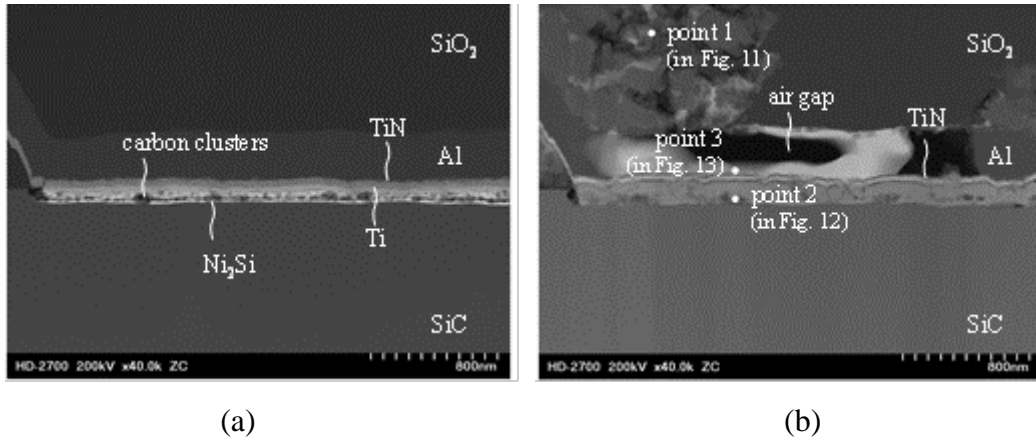


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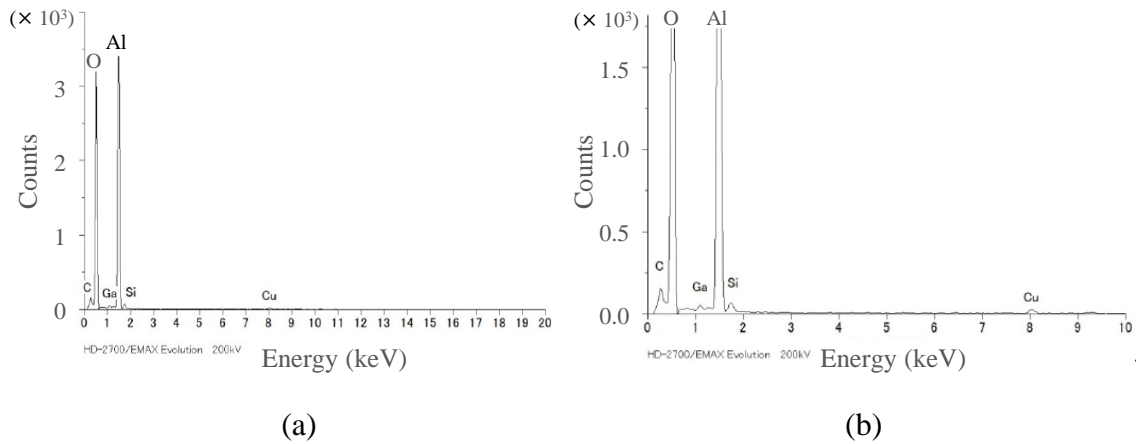


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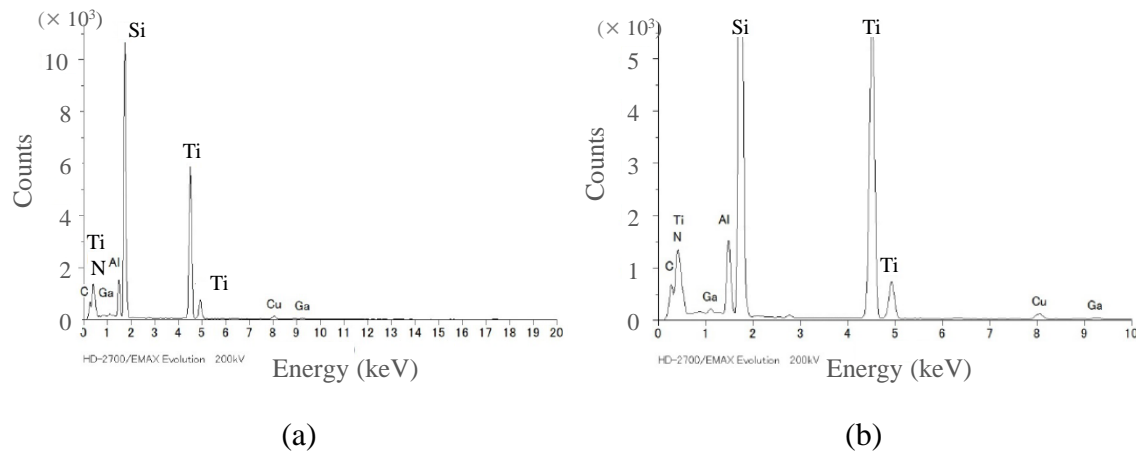


Fig. 12. (black and white) (a) TEM-EDX result and (b) enlarged it. These results are at contact metal after high-temperature-storage test (point 2 in Figure 10(b)).

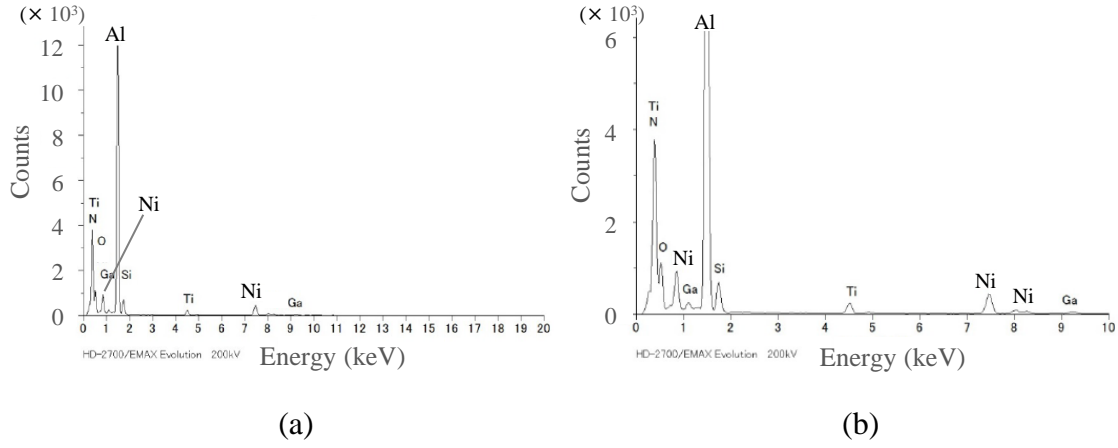


Fig. 13. (black and white) (a) TEM-EDX result and (b) enlarged it. These results are at aluminum layer near TiN after the high-temperature-storage test (point 3 in Figure 10(b)).

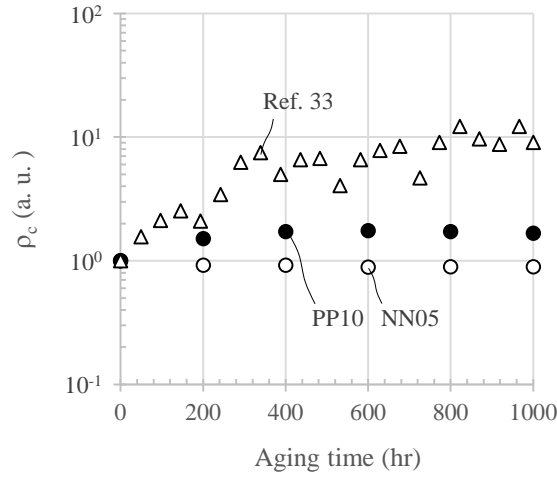
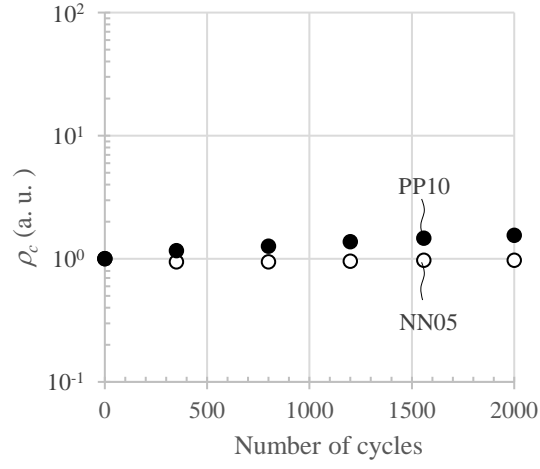


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