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Static Tensile and Brittle Fracture Strengths of Soft Welded Joints[†]

Kunihiko SATOH* and Masao TOYODA**

Abstract

Static tensile and brittle fracture behaviors of the welded joints having weld metal whose strength is lower than it of base metal, or soft welded joints, are investigated. The strength of the welded joints having soft weld metal is much elevated from it of the soft weld metal itself. It is effective to use soft weld metal in a part of weld metal from the viewpoint of efficiency of strength. The "Soft Ratio" Sr of weld metal required to guarantee the standard strength and the elongation of welded joints are considered. When $Sr (= \sigma_u^W / \sigma_u^B) \geq 0.93$, ultimate tensile strength and elongation of all kinds of soft welded joints become almost equal to those of base metal. The brittle fracture strength of welded joints is affected more considerably with fracture toughness than yield strength of weld metal. The soft welded joints whose fracture toughness is a little better than it of the ordinary weld metal guarantee the sufficiently brittle fracture strength.

1. Introduction

In the welded joints, it becomes a common idea that the strength of weld metal is equal to or higher than it of base metal from the viewpoints of efficiency of welded joints. Otherwise, it is effective to use the weld metal whose strength is lower it of base metal in order to prevent the initiation of weld cracking.¹⁾ If welded joints having lower grade weld metal have a larger strength than it required as the welded joints, it is one of the useful welding procedure to use the lower grade welding rod.

The investigations have been made by the static tensile test of model specimens including a soft interlayer whose strength is lower than it of base metals.^{2)~5)} The test results have revealed that the tensile strength approaches it of the base metal for sufficiently small values of the relative thickness of the soft interlayer.

In the future, as the welded structures become larger size and it becomes a larger demand to use the more thick plates of high tensile strength steel, the requirement to use the lower grade welding rods from a viewpoint of welding procedure will be arised. In this report, the static tensile and brittle fracture behaviors of the welded joints having weld metal whose strength is lower it of base metal —so called "Soft Welded Joints"— are investigated.

2. Static tensile behaviors of soft welded joints

2.1 Experiment

The following three kinds (four Series) of welded joints in each of which the size and the position of

soft weld metal were different as shown in **Table 1** were employed for experimental work.

- 1 ; All soft welded joint (Series ①): Welded joints in which all weld metal are soft metal.
- 2 ; Partial soft welded joint in which only weld metal in a root part is soft metal (Series ②, ③): From the viewpoints of prevention of root cracking in the welding of thick plates, lower grade electrodes are used only in a root part and ordinary grade electrodes are used in other parts of weld metal.
- 3 ; Partial soft welded joint in which only weld metal in a part of plate surface is soft metal (Series ④): In order to examine the possibility to use the lower grade electrodes in repair welding, this partial soft welded joints are made.

The details on experiments are found in another report.⁵⁾

2.2 Tensile strength of all soft welded joints

Let Sr denote the "Soft Ratio" defined by the following equation.

$$Sr = \sigma_u^W / \sigma_u^B$$

where σ_u^W is the tensile strength of weld metal and σ_u^B is it of base metal.

Figure 1 shows the relationships between the tensile strength of all soft welded joints (σ_u^W / σ_u^B) and the Sr -value. A line ③ in **Fig. 1** is the line whose inclination angle to abscissa is 45 degrees. What all experimental values of the tensile strength are above the line ③, shows that the tensile strength of soft

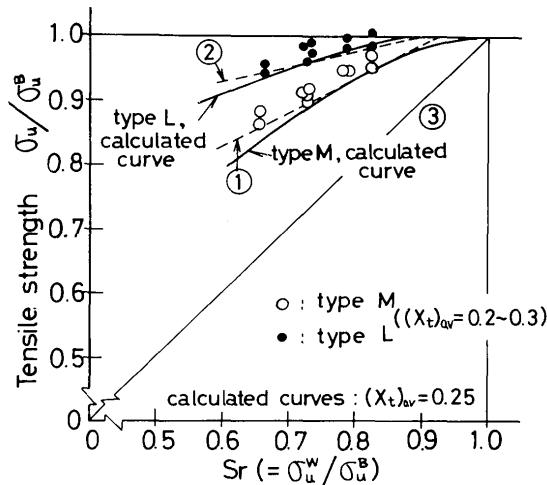
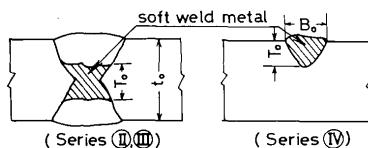
† Received on Nov. 25, 1972

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Table 1. Contents of experiments.

Series	Welded joint	Contents of experiments
I	All soft welded joint	(a) Effect of soft ratio (strength level of weld metal; HT80, HT60, HT50)
		(b) Effect of specimen width (type L: $W_o = 500$ mm, type M: $W_o = t_o = 70$ mm)
		(c) Effect of groove shape (X, U)
II	Root partial soft welded joint	(b) Effect of width (welding length) ($W_o = 3 \sim 92$ mm)
		(d) Effect of thickness (T_o) of soft weld metal (type A: $T_o/t_o \approx 1/2$, type B: $T_o/t_o \approx 1/4$, type S: all soft welded joint, type N: normal joint)
III	Root partial soft welded joint	(a) Effect of soft ratio (strength level of weld metal; HT80, HT60, HT50, MS)
		(b) Effect of width (B_o) of soft weld metal (type A: $B_o \approx 20$ mm, type B: $B_o \approx 10$ mm)
IV	Soft repair welded joint	(a) Effect of soft ratio (strength level of weld metal; HT80, HT60, HT50, MS)
		(e) Effect of width (B_o) of soft weld metal (type A: $B_o \approx 20$ mm, type B: $B_o \approx 10$ mm)

Fig. 1. Effect of soft ratio Sr on tensile strength σ_u/σ_u^B of all soft welded joints.

welded joints is larger than it of weld metal itself. As the soft ratio Sr is closer to unity, σ_u/σ_u^B approaches unity, that is, the strength of welded joints becomes nearly equal to strength of base metal.

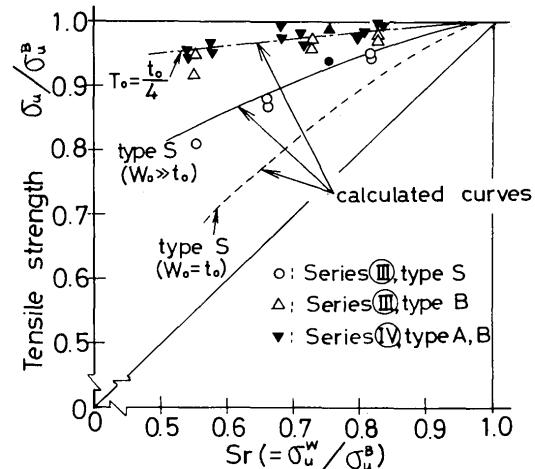
The mark \circ in **Fig. 1** shows the results for a specimen having square cross-section (type M, $W_o = t_o = 70$ mm) and the mark \bullet shows it for large width specimen (type M, $W_o = 500$ mm). Comparing the both, the strength of large width welded joints is larger than it of square section welded joints. As mentioned in the previous reports,^{3), 5)} the strength for type L is almost the same as the one in a infinite wide plate.

In the previous reports^{2)~5)} theoretical studies on tensile strength of welded joint including a soft

interlayer were made. Using these results, ultimate tensile strength of soft welded joints can be calculated if dimensions of test specimen and soft weld metal is known. The solid curves in **Fig. 1** show the results calculated using authors' theoretical analysis for type L or type M, respectively. In **Fig. 1**, the experimental values agree well with the theoretical results. In this experiment, high tensile strength steel (HT 80) of 80 kg/mm² strength level was used as base metal. Considering the experimental results of the former fundamental study,⁴⁾ this relationships between σ_u/σ_u^B and Sr in **Fig. 1** also hold true regardless of strength level of base metal.

2.3 Tensile strength of Partial soft welded joints

Figure 2 shows the relationships between the

Fig. 2. Effect of soft ratio Sr on tensile strength σ_u/σ_u^B of partial soft welded joints.

tensile strength σ_u / σ_u^B and the soft ratio Sr obtained in the test Series (III) -type S (\bigcirc -mark), -type B (\triangle -mark) and Series (IV) -type A, B (\blacktriangledown -mark).

Tensile strength of partial soft welded joints is of course larger than it of all soft welded joints. And as the size T_o of soft weld metal becomes smaller, tensile strength of welded joints becomes larger.

The black symbols (\blacktriangledown -mark) in **Fig. 2** show the results for Series (IV), or the welded specimens having soft weld metal in a part of plate surface. The experimental results in Series (III) (type B) and Series (IV), in both which the ratio of the thickness of soft weld metal T_o to the plate thickness t_o is nearly equal to 1/4, are on one curve as shown **Fig. 2**. It is concluded that the tensile strength of partial soft welded joints having a certain constant value of T_o/t_o is constant, regardless of the position of soft weld metal. The curves in **Fig. 2** show the results calculated using authors' theoretical analysis^{2)~5)}. The experimental values agree well with the theoretical results in the same manner as **Fig. 1**.

2.4 Ductility of soft welded joints

In the soft welded joints, their strength is generally elevated from it of the soft weld metal itself, while their ductility becomes smaller than it of the soft weld metal or base metal.

When the ductility of tensile test specimens is represented by the elongation in percent in a certain gauge length L_o , it is affected significantly by the magnitude of the gauge length L_o . The elongation measured after fracture is the sum of local elongation and uniform elongation. In the percent elongation measured over the gauge length L_o , the term concerned with the uniform elongation is independent of the gauge length, while the term concerned with the local elongation depends upon L_o . As the percent elongation in tensile test specimens depends upon the gauge length L_o , it becomes a serious matter of great concern to choose the value of gauge length L_o in the evaluation of the ductility of welded joints. If the ductility of welded joints is evaluated by the uniform elongation ϵ_u , the problem how long the gauge length should be chosen can be taken away.

Figure 3 shows the relationships between uniform elongation ϵ_u and soft ratio Sr for various Series. As the Sr -value becomes smaller, uniform elongation ϵ_u becomes smaller than it of base metals or normal welded joints whose weld metal has same strength level as its base metal. Uniform elongation ϵ_u of partial soft welded joints is larger than it of all soft welded joints. If $Sr \geq 0.8$ in partial soft welded joints and $Sr \geq 0.9$ in all soft welded joints, uniform elongation of soft welded joints becomes nearly equal to it

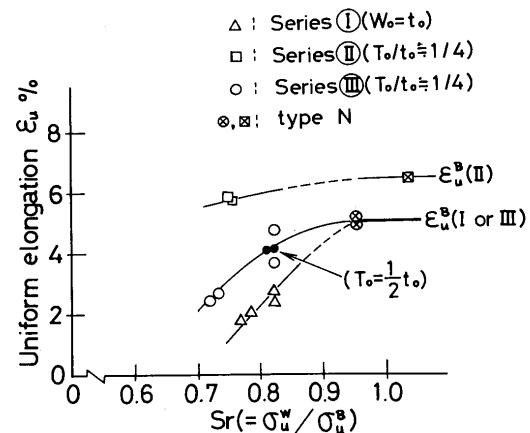


Fig. 3. Relation between uniform elongation ϵ_u and soft ratio Sr .

of base metals.

2.5 Soft ratio required to guarantee the standard strength as welded joints

Mechanical properties such as tensile strength and ductility of welded joints must be different by the procedures of welding and the combinations between base metals and welding rods, because there is mechanical heterogeneity in welded joints. The values of mechanical properties required as welded joints must be dependent on the welding structures and the basic idea of design. In this paper, that basic idea of design does not be discussed in detail and the following two standards are considered as the required strength σ_u of welded joints.

(Standard I) $\sigma_u \geq \sigma_u^B$ (strength of base metal)

(Standard II) $\sigma_u \geq$ (guaranteed strength for design)

Tensile strength σ_u of soft welded joints can be calculated by analytical method as above mentioned, but in a engineering sight, it is considered that relationships between tensile strength σ_u and soft ratio Sr are estimated by a straight lines connecting the lowest experimental values in each series as shown in **Figs. 4**, 5. These lines are summarized in **Fig. 6**.

In **Fig. 6**, the all lines from (1) to (4) becomes $\sigma_u / \sigma_u^B = 1.0$ in $Sr = 0.9 \sim 0.93$. When $Sr (= \sigma_u^w / \sigma_u^B) \geq 0.93$, ultimate tensile strength of all kinds of soft welded joints becomes almost equal to it of base metal.

The soft ratio Sr^p required to guarantee the standard strength of base metal in standard (II) is a function of σ_u^B / σ_u^D because the tensile strength σ_u^B of base metal is generally larger than the standard strength σ_u^D of base metal. If it is considerd that the relationship between σ_u / σ_u^B and Sr in all soft welded joints is represented by the line (1) in **Fig. 6** and it in partial soft welded joints is represented by the line (4) in **Fig. 6**, the Sr^p -values show as a function of σ_u^B / σ_u^D as dotted curves (1) or (2) in **Fig. 7**.

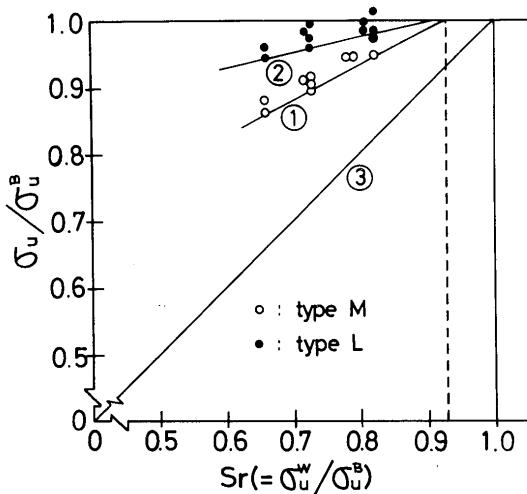


Fig. 4. Relation between Sr and tensile strength. (all soft welded joints)

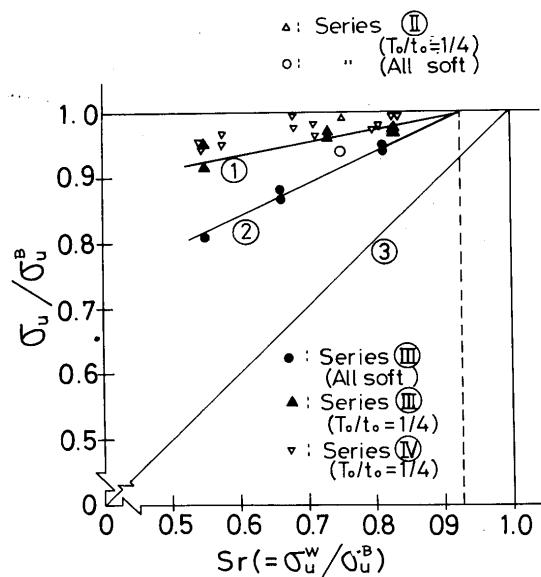


Fig. 5. Relation between Sr and tensile strength. (Partial soft welded joints)

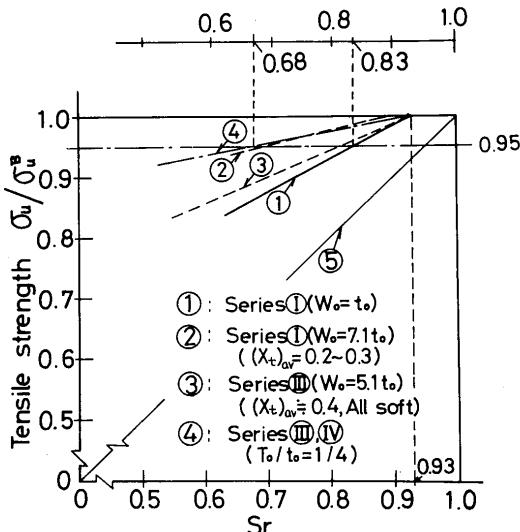


Fig. 6. Effect of Sr on tensile strength (Series ①~④).

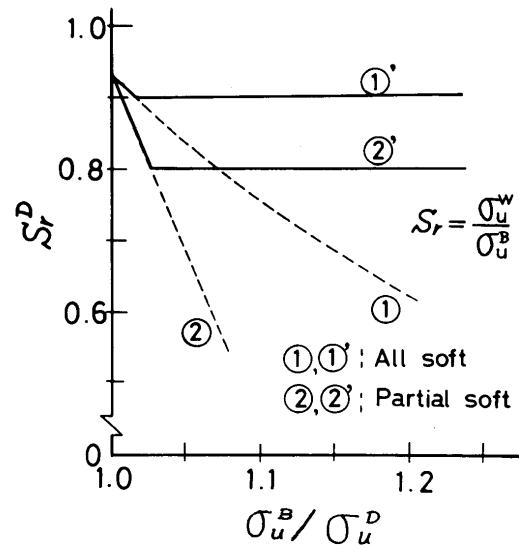


Fig. 7. Relation between Sr^D and σ_u^B / σ_u^D .

As mentioned above, when

$Sr < 0.9$ (in all soft welded joints)

$Sr < 0.8$ (in partial soft welded joints, $T_o/t_o = 1/4$), the uniform elongation of soft welded joints becomes smaller than it of base metal. The soft ratio Sr^D required to guarantee the standard strength σ_u^D and the uniform elongation as same as it of base metal are given as the solid curves ①', ②' in Fig. 7.

3. Brittle fracture behaviors of soft welded joints

3.1 Experiment

Tensile tests of soft welded joints having notch in weld metal were carried out and the brittle fracture behaviors of soft welded joints are investigated.

Two plates of a high tensile strength steel (HT80) of 80 kg/mm² strength level were submerged welded with electrodes having 80, 60 and 50 kg/mm² strength level. The average thickness (H_o)_{av} of weld metal is 13~14 mm. **Table 2** shows the chemical compositions, the mechanical properties at room temperature and results of V-notch Charpy test of the material.

Figure 8 (a) shows the size of deep notch test specimens and **Fig. 8 (b)** shows the shape and size of small scale bending COD specimen to estimate the critical COD Φ_c of base metal and weld metals.

The details on experiments are found in another report.⁶⁾

3.2 Experimental results

Figure 9 shows the relationships between fracture net stress and temperature. The curves $\sigma_y(\bigcirc)$, $\sigma_y(\triangle)$ etc. in **Fig. 9** show the temperature dependence of the yield stress (0.2 % proof stress) of base metal (HT80) and weld metals.

The fracture stress-temperature curves of welded

Table 2. Chemical compositions and mechanical properties.

Steel	Chemical composition (%)									Y. S. kg/mm ²	T. S. kg/mm ²	νT_s °C
	C	Si	Mn	P	S	Mo	Ni	Cr	V			
B.M.	0.14	0.23	0.90	0.012	0.008	0.44	Tr.	0.73	0.03	75.3	82.1	-88
W.M. (80)	0.10	0.47	1.25	0.014	0.016	0.45	1.20	0.59	0.01	59.0	81.3	-43
W.M. (60)	0.10	0.37	1.31	0.015	0.013	0.45	0.04	0.39	0.01	56.3	70.8	-75
W.M. (50)	0.13	0.24	0.91	0.011	0.009	0.40	0.02	0.79	0.025	49.4	64.4	-53

Tr. : Trace

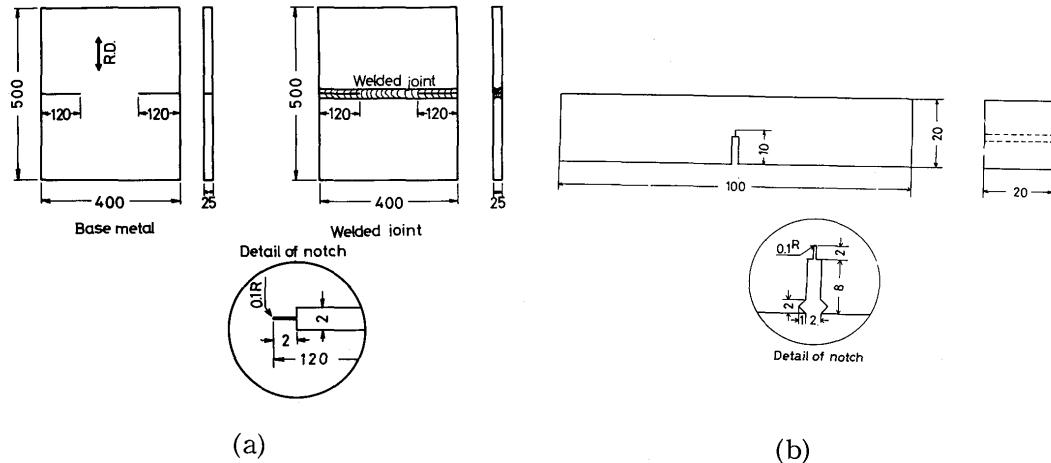
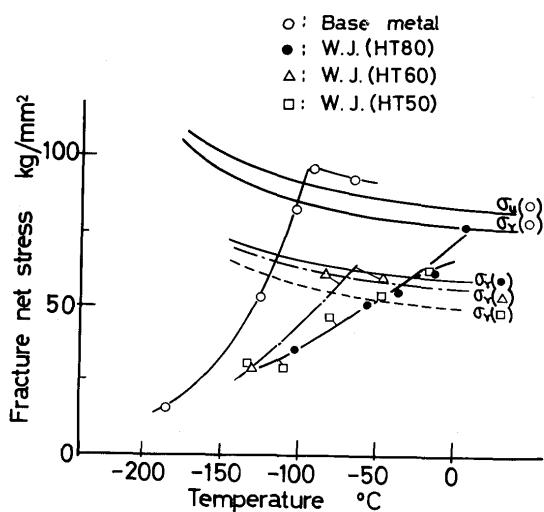


Fig. 8. Deep notch specimen and COD bending specimen.

Fig. 9. Relation between fracture net stress σ_f and test temperature.

joints shift to high temperature side in comparison with it of base metal (HT80). In this experiment, the welded joints using welding wires for HT60 have the largest strength in comparison with the other welded joints. There is little difference in the fracture strength between the welded joints having welding wires for HT80 and these for HT50. Comparing the size of the νT_s (°C)-values in these weld metal, weld metal for HT60 has the lowest value and it for HT50, for HT80 is in order. The fracture strength depends largely on the fracture toughness (νT_s -value). Even if

the strength of the weld metal is lower than it of base metal, the fracture strength of the welded joints using welding rods which have a higher toughness value becomes larger than it of base metal or welded joints using welding rods which have the same strength level as base metal.

Figure 10 shows the relationships between the critical crack opening displacement Φ_c and the reciprocal of testing temperature $1/T$ (°K). The lines in

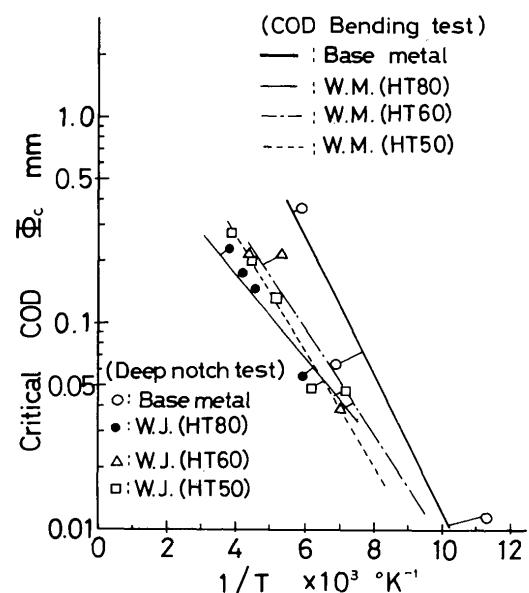
Fig. 10. Relation between critical COD Φ_c and $1/T$.

Fig. 10 shows the Φ_c - $1/T$ relationships obtained by small scale bending COD testing and the experimental values plotting in **Fig. 10** are the Φ_c -values obtained from Deep Notch Test. The both results agree very well. In Φ_c -value, also, it of welding rod for HT60 is largest value and it for HT50, for HT80 in order becomes smaller.

As mentioned in our another report,⁶⁾ the fracture behaviors of the soft welded joints are affected with the plastic constraint of the harder base metal. However, in this experimental range, it may be recognized the effect of this plastic constraint be neglected.

3.3 Brittle fracture initiation temperature $(T_{io})_{\%}$ and soft ratio of weld metal

Denoting the brittle fracture initiation temperature at which the fracture stress $\sigma_f = 1/2 \sigma_{yo}$ (σ_{yo} : yield stress at sub-zero) by $(T_{io})_{\%}$, the authors employ the $(T_{io})_{\%}$ -value as the parameter representing the brittle fracture behaviors.

Let define the ratio of yield stress of weld metal σ_{yo}^w to it of base metal σ_{yo}^b , or $\sigma_{yo}^w/\sigma_{yo}^b$ as Soft Ratio (Sr)_y of yield stress of weld metal. The temperature $(T_{io}^b)_{\%}$ at which the fracture stress σ_f of soft welded joints having a notch in weld metal becomes equal to $1/2 \sigma_{yo}^b$ can be calculated equally well by Φ_c or ρ_c^+ criterion. In this paper, the basic concept employed expediently for discussion is that brittle fracture should initiate when tensile yield zone ρ^+ formed ahead of a pre-existing crack attaines a critical size ρ_c^+ , because the authors adopt the experimental equations showed by Koshiga et al.⁷⁾ as the relationship between fracture toughness ρ_c^+ and temperature and between ρ_c^+ and νT_s -value. The relationship between ρ_c^+ -value and temperature was given by Koshiga et al. as follows.

$$\rho_c^+ = \alpha (T/100)^5 \quad (\alpha \text{ in mm, } T \text{ in } ^\circ\text{K}) \quad (1)$$

where α is a material constant.

The tensile yield zone size ρ^+ in a infinite plate subjected to uniform tensile stress σ is determined by

$$\frac{c}{a} = \cos \left(\frac{\pi}{2} \frac{\sigma}{\sigma_y} \right) \quad (2)$$

where

$$a = c + \rho^+$$

When $\sigma < 0.6 \sigma_y$ (σ_y : yield stress), the relationship between ρ^+ and σ is given approximately as follows.

$$\frac{\rho^+}{c} = \frac{\pi^2}{8} \left(\frac{\sigma}{\sigma_y} \right)^2 \quad (3)$$

It is generally recognized that relation between yield stress σ_y and temperature $T(^{\circ}\text{K})$ is given as follows

$$\sigma_y = \sigma_{yo} \exp \left\{ D \left(\frac{1}{T} - \frac{1}{273} \right) \right\} \quad (4)$$

where D is a material constant.

Denoting the material constants of base metal by α^b , D^b and these of weld metal by α^w , D^w , the $(T_{io}^b)_{\%}$ -value at which $\sigma_f = 1/2 \sigma_{yo}^b$ can be calculated by following equations for base metal and soft welded joints respectively.

$$\text{Base metal : } \frac{\alpha^b}{c} \left\{ \frac{(T_{io}^b)_{\%}}{100} \right\}^5 = \frac{\pi^2}{32} \exp \left\{ \frac{2D^b}{273} - \frac{2D^b}{(T_{io}^b)_{\%}} \right\} \quad (5)$$

$$\text{Welded joints : } \frac{\alpha^w}{c} \left\{ \frac{(T_{io}^b)_{\%}}{100} \right\}^5 = \frac{\pi^2}{32} \frac{1}{(Sr)_y^2} \times \exp \left\{ \frac{2D^w}{273} - \frac{2D^w}{(T_{io}^b)_{\%}} \right\} \quad (6)$$

Let consider the relationship between $(Sr)_y$ -value and fracture toughness in the case which $(T_{io}^b)_{\%}$ -value for soft welded joints becomes equal to $(T_{io}^b)_{\%}$ -value of base metal. If the $(T_{io}^b)_{\%}$ -value of welded joints is equal to it of base metal, from eqs. (5), (6),

$$\frac{\alpha^b}{\alpha^w} = (Sr)_y^2 \exp \left\{ 2(D^w - D^b) \left(\frac{1}{(T_{io}^b)_{\%}} - \frac{1}{273} \right) \right\} \quad (7)$$

The $(T_{io}^w)_{\%}$ -value at which $\sigma_f = 1/2 \sigma_{yo}^w$ is employed as the parameter representing the brittle fracture toughness of weld metal. $(T_{io}^w)_{\%}$ is given as follows.

$$\frac{\alpha^w}{c} \left\{ \frac{(T_{io}^w)_{\%}}{100} \right\}^5 = \frac{\pi^2}{32} \exp \left\{ \frac{2D^w}{273} - \frac{2D^w}{(T_{io}^w)_{\%}} \right\} \quad (8)$$

From eqs. (7), (8), the relationship between $(T_{io}^b)_{\%}$ and $(T_{io}^w)_{\%}$ is given as following equation.

$$(Sr)_y = \exp \left\{ \frac{D^w}{(T_{io}^w)_{\%}} - \frac{D^b}{(T_{io}^b)_{\%}} \right\} \left\{ \frac{(T_{io}^b)_{\%}}{(T_{io}^w)_{\%}} \right\}^{-5/2} \quad (9)$$

The relationship between D -value and σ_{yo} is given approximately as following as shown in previous report.⁸⁾

$$D = 325 - 65 \ln \sigma_{yo} \quad (10)$$

So that

$$D^w = D^b - 65 \ln (Sr)_y \quad (11)$$

When the yield strength of base metal is determined the relationship between $(Sr)_Y$ -value and $\Delta(T_{io})_{1/2}$ ($= (T_{io}^W)_{1/2} - (T_{io}^B)_{1/2}$) can be calculated from eq. (13).

Figure 11 shows the relationship between $(Sr)_Y$ and $\Delta(T_{io})_{1/2}$ when the $(T_{io}^B)_{1/2}$ -value of soft welded joints becomes equal to $(T_{io}^B)_{1/2}$ -value of base metal, for example in $\sigma_{yo}^B = 70 \text{ kg/mm}^2$. As the $(Sr)_Y$ -value becomes small, $-\Delta(T_{io})_{1/2}$ -value becomes larger. For example when $(Sr)_Y = 0.8$, if $-\Delta(T_{io})_{1/2} \approx 15 \sim 20^\circ\text{C}$, the fracture initiation temperature of soft welded joints becomes nearly equal to it of base metal.

In the foregoing considerations, we adopted the $(T_{io})_{1/2}$ -value as the parameter which was a typical example of fracture toughness. It is very convenient that transition temperature obtained from the small scale testing, for example V-notch Charpy impact test, can be adopted as that parameter. It was shown by Koshiga et.al.⁷⁾ that the relatively good correlation between the fracture toughness ρ_c^+ -value and the fracture transition temperature νT_s may exist. The relationship between the α -value showed in eq.(1) and νT_s -value is given as follows by Koshiga's report.⁷⁾

$$\alpha = 1.53 \exp \left\{ -\frac{\nu T_s (\text{ }^\circ\text{C})}{40} \right\} \quad (12)$$

Denoting the fracture transition temperature of base metal and weld metal by νT_s^B and νT_s^W respectively, the relationship between $(Sr)_Y$ and $\Delta \nu T_s$ ($= \nu T_s^W - \nu T_s^B$) when the $(T_{io}^B)_{1/2}$ -value of soft welded joints becomes equal to it of base metal can be obtained from eqs. (7), (8), (12) as following equation.

$$\Delta \nu T_s = \nu T_s^W - \nu T_s^B = 80 \left\{ \ln (Sr)_Y \right\} \left\{ 1 - 65 \left(\frac{1}{(T_{io}^B)_{1/2}} - \frac{1}{273} \right) \right\} \quad (13)$$

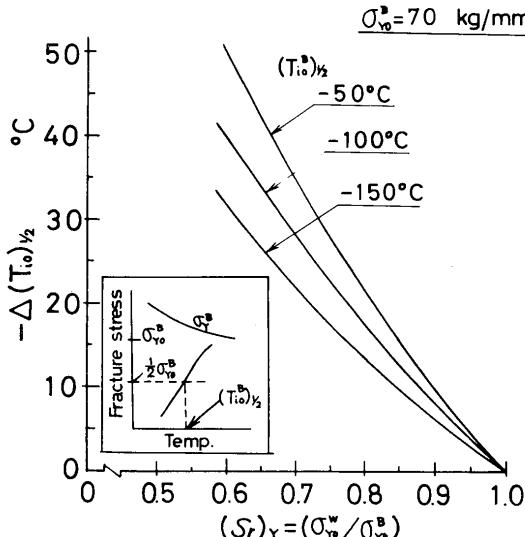


Fig. 11. Relation between $-\Delta(T_{io})_{1/2}$ and $(Sr)_Y$.

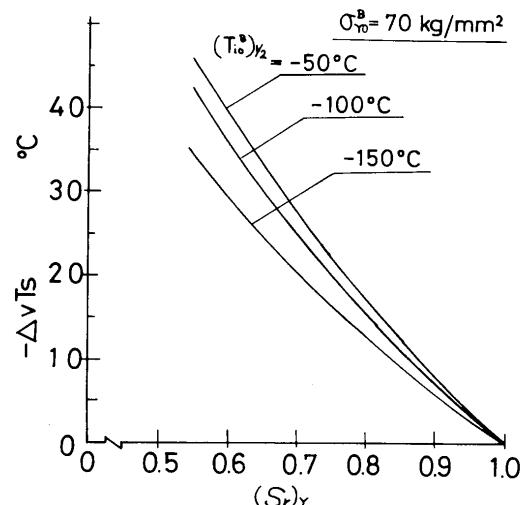


Fig. 12. Relation between $-\Delta \nu T_s$ and $(Sr)_Y$.

Figure 12 shows the relationship between $-\Delta \nu T_s$ and $(Sr)_Y$ calculated from eq.(13). The results in **Fig. 12** showed results approximately similar to those in **Fig. 11**.

Figure 13 shows the relationship between the $-\Delta \nu T_s$ ($= \nu T_s^B - \nu T_s^W$) required to guarantee the design brittle fracture strength in the soft welded joints whose Soft Ratio is Sr^D , where the νT_s^D -value is the νT_s -value of weld metal required to guarantee the design strength when its strength level is equal to it of base metal. The $\Delta \nu T_s$ -value is affected with the strength of base metal and yield ratio of materials.

When $(Sr)_Y / Sr = 1.0$,

- (1) All soft welded joints; $|\nu T_s| \geq 8^\circ\text{C}$ ($\sigma_y^W / \sigma_y^B = 0.9$)
- (2) Partial soft welded joints; $|\nu T_s| \geq 17^\circ\text{C}$ ($\sigma_y^W / \sigma_y^B = 0.8$)

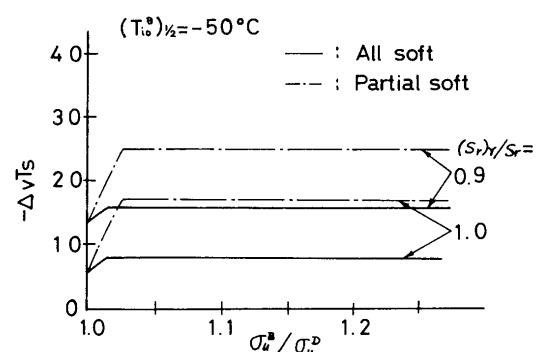


Fig. 13. Relation between $-\Delta \nu T_s$ and σ_u^B / σ_u^D .

4. Conclusion

The results obtained in this report are summarized as follows:

- (1) Static tensile strength and elongation in percent of soft welded joints are affected by the "Soft Ratio" Sr ($= \sigma_u^W / \sigma_u^B$) of welded metal. The minimum

soft ratio Sr^D required to guarantee the standard strength of base metal and ductility as same as these of base metal is determined from the results of this experiments (Fig. 7). Although the Sr^D -value is influenced by the tensile strength σ_u^B of base metal and the size of soft weld metal, the Sr^D -values are given nearly as following equations.

In all soft welded joints; $Sr^D=0.9$

In partial soft welded joints; $Sr^D=0.8$
 $(T_o = t_o/4)$

- (2) The fracture toughness of weld metal required to guarantee the brittle fracture strength which is standard strength of design can be calculated when the soft ratio of weld metal is determined. The soft welded joints whose fracture toughness is a little better than it of the ordinary weld metal, guarantee the sufficiently brittle fracture strength (Fig. 13).

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