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# Physically-motivated feedback models and the IGM metal enrichment in cosmological hydrodynamic simulations

by

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degree of Doctor of Philosophy

in the

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# *Abstract*

The elucidation of the structure formation history of the Universe is a major goal in both astrophysics and cosmology, and understanding the formation processes of galaxies, the building blocks of the cosmic large-scale structure, is a central challenge. Cosmological hydrodynamic simulations are widely used as a tool to provide direct theoretical predictions for this challenge. In galaxy formation in the  $\Lambda$ CDM universe, the standard model of modern cosmology, both observation and theory suggest that feedback from astronomical phenomena such as supernovae (SNe) and active galactic nuclei (AGN) is essential. However, dealing directly with pc-scale astrophysical effects in cosmological simulations with computational domains exceeding Mpc is computationally infeasible, and it is necessary to introduce a subgrid model of feedback effects.

Models of feedback are the largest source of uncertainty in cosmological hydrodynamic simulations, and many previous studies have used phenomenological models fine-tuned to reproduce galaxy observations. However, it has recently been pointed out that even models that reproduce galaxy observations fail to reproduce observations of the circumgalactic medium. Models based on pc-scale physics are needed for a comprehensive understanding of galaxy formation and for theoretical predictions for future high-sensitivity observations.

In this study, we develop a physically-motivated SN feedback model based on high-resolution simulations that resolve the pc scale. Considering the physical effects of the SN feedback and numerical constraints, the model incorporates both the mechanical effects of the feedback on the interstellar gas and the effects of the galactic wind on the circumgalactic medium. We then implement this model in the cosmological hydrodynamic simulation code GADGET4-OSAKA. We also implement a model of the formation and growth of supermassive black holes, which cause feedback as AGNs, and a chemical evolution model accounting for the metallicity dependence of the initial stellar mass function. We show that this simulation, named CROCODILE, generally reproduces observational statistics such as the galaxy mass function.

We analyze the CROCODILE dataset to investigate the impact of SN and AGN feedback on metal enrichment in the intergalactic medium. The results show that SN feedback plays a major role in metal enrichment. Additionally, the AGN feedback affects the metal distribution below redshift two and creates characteristic metal enrichment regions on the scale of a few Mpc.

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# Abbreviations

**$\Lambda$ CDM**  $\Lambda$  cold dark matter.

**AGB** asymptotic giant branch.

**AGN** active galactic nucleus.

**BH** black hole.

**CCSN** core-collapse supernova.

**CGM** circumgalactic medium.

**CIC** cloud-in-cell.

**CMB** cosmic microwave background.

**EoS** equation of state.

**FoF** Friend-of-Friends.

**HN** hypernova.

**ICMF** initial stellar cluster mass function.

**IGM** intergalactic medium.

**IMF** initial mass function.

**IR** infrared.

**ISM** interstellar medium.

**LMC** Large Magellanic Cloud.

**LRG** luminous red galaxies.



**PDS** pressure-driven snowplow.

**SFR** star formation rate.

**SN** supernova.

**SPH** smoothed particle hydrodynamics.

**sSFR** specific star formation rate.

**SSP** simple stellar population.

**UV** ultraviolet.

**YMC** young massive star cluster.

*To My Parents*

# Chapter 1

## Introduction

### 1.1 Structure formation in the $\Lambda$ CDM universe

Within the  $\Lambda$  cold dark matter ( $\Lambda$ CDM) model, the theory of structure formation in the universe has been extensively developed. The time evolution of the universe is dictated by the Friedmann equation, which is the reduced form of Einstein's equation on the Friedmann–Lemaître–Robertson–Walker metric, a metric on a homogeneous and isotropic universe,

$$H^2 = \frac{8\pi G}{3c^2}\rho + \frac{\Lambda c^2}{3} - \frac{Kc^2}{a^2}. \quad (1.1)$$

where  $H$  is the Hubble parameter,  $\rho$  is the energy density of matter,  $\Lambda$  is the cosmological constant,  $K$  is the curvature of the universe, and  $a$  is the scale factor. The (flat)  $\Lambda$ CDM model is the case where we have non-zero  $\Lambda$ , the matter in the universe is composed of 'cold' dark matter, i.e., the kinetic energy of dark matter is much less than the mass energy, and the universe is flat, i.e.,  $K = 0$ .

This model gives robust predictions of the distribution of matter on large scales, where the gravitational influence of dark matter is the major driver of these distributions (e.g., Blumenthal et al., 1984, Davis et al., 1985, Ostriker and Steinhardt, 1995, Perlmutter et al., 1998, Bahcall et al., 1999). Figure 1.1 shows the matter power spectrum at  $z = 0$ . The data points are inferred from observations on different scales and at different redshifts; the cosmic microwave background (CMB) on scales of  $\gtrsim 10$  Mpc at  $z \sim 1100$ , the luminous red galaxies (LRG) on scales of  $\sim 10$  Mpc at  $z \sim 0.35$ , the cosmic shear (weak gravitational lensing) on scales of  $\sim 1$  Mpc at  $z = 0.2$ -1.3, and the Ly $\alpha$  forest on scales of  $\sim 1$  Mpc at  $z = 2.2$ -4.6. Given the cosmological parameters calibrated to the *Planck* CMB observation, the theoretical expectation from  $\Lambda$ CDM model consistently reproduces these observations.

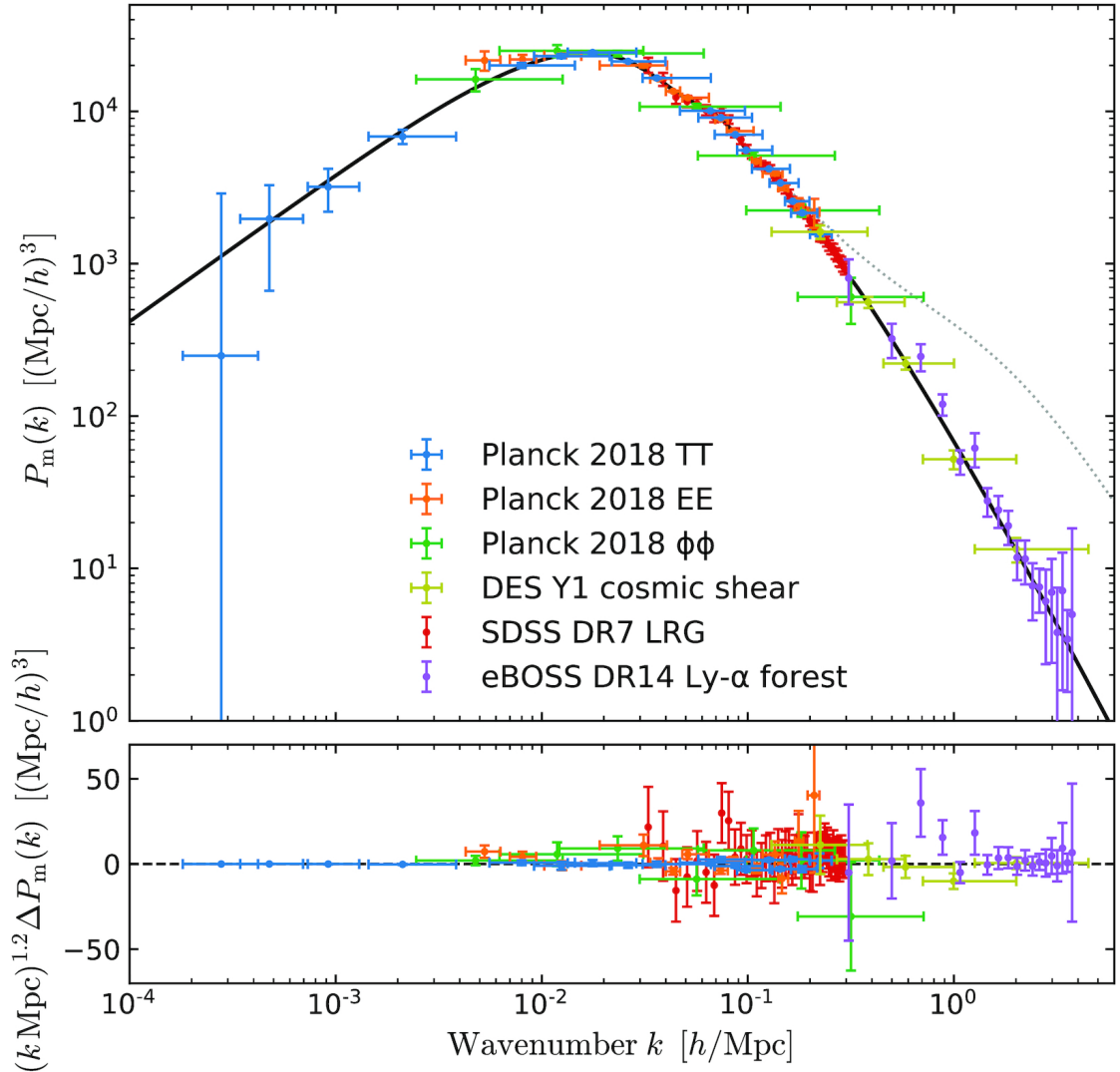


FIGURE 1.1: Top: The linear 3D matter power spectrum at  $z = 0$ . Data points show inferences of the 3D linear matter power spectrum from *Planck* CMB data on the largest scales (Planck Collaboration et al., 2020), SDSS galaxy clustering (Reid et al., 2010) on intermediate scales, SDSS Ly $\alpha$  clustering (Abolfathi et al., 2018) and DES cosmic shear data (Troxel et al., 2018) on the smallest scales. The solid black line is the theoretical expectation given the best-fitting *Planck* 2018  $\Lambda$ CDM model. The dotted line for reference shows the theoretical spectrum, including non-linear effects. Bottom: Deviation of the data from the *Planck* best-fitting  $\Lambda$ CDM 3D matter power spectrum.

Reprinted from Figure 1 of Chabanier et al. (2019) with permission.

However, this model faces difficulties at smaller scales. Here the influences of astrophysical and hydrodynamical processes become increasingly important. This adds complexity to our understanding of the distribution of baryonic matter and the evolution and formation of galaxies and black holes throughout cosmic history.

## 1.2 Galaxy formation and supernova feedback

A **supernova (SN)** is a massive explosion with a typical energy of  $10^{51}$  erg, but it affects only several tens of parsec of the **interstellar medium (ISM)**, which is three orders of magnitude smaller than the size of a galaxy, e.g., the radius of Milky Way is  $\sim 10$  kpc. **SN** is still important as a feedback source due to its collective effect. In our Milky Way Galaxy, the typical number of star formation rate is  $1 M_{\odot} \text{yr}^{-1}$ , the occurrence rate of **SN** per stellar mass is  $10^{-2} M_{\odot}^{-1}$ , and the rotation time of the galactic disk is 200 Myr. Combining these numbers, we obtain  $2 \times 10^6$  **SNe** per galactic rotation, whose energy is comparable to the gravitational bounding energy of a galaxy. This nature of **SN** feedback as a collective effect of numerous **SN** explosions and its spatial and temporal scales makes it difficult to obtain direct observational evidence nor perform direct simulations to draw a comprehensive picture of **SN** feedback.

In this section, I summarize the observational and theoretical implications of how **SN** feedback affects galaxy formation.

### 1.2.1 Observational suggestion

In this subsection, I describe observations related to **SN** feedback, starting from statistics of the stellar mass of galaxies, then the galactic wind of an individual galaxy, and finally, a superbubble formed by **SN** explosions.

#### 1.2.1.1 Galaxy stellar mass function

The existence of the astrophysical feedback effect is realized by the fact that star formation is inefficient in galaxies. Figure 1.2 compares the dark matter halo mass function and galaxy stellar mass functions in the nearby universe ( $z \sim 0.1$ ). The dashed black line is the mass function of baryons in dark matter halos. One would expect that the dashed black line corresponds to the galaxy stellar mass function, assuming gas is converted to stars without feedback. However, Figure 1.2 shows that the dashed black line deviates from the observed galaxy stellar mass function, and star formation is more inefficient

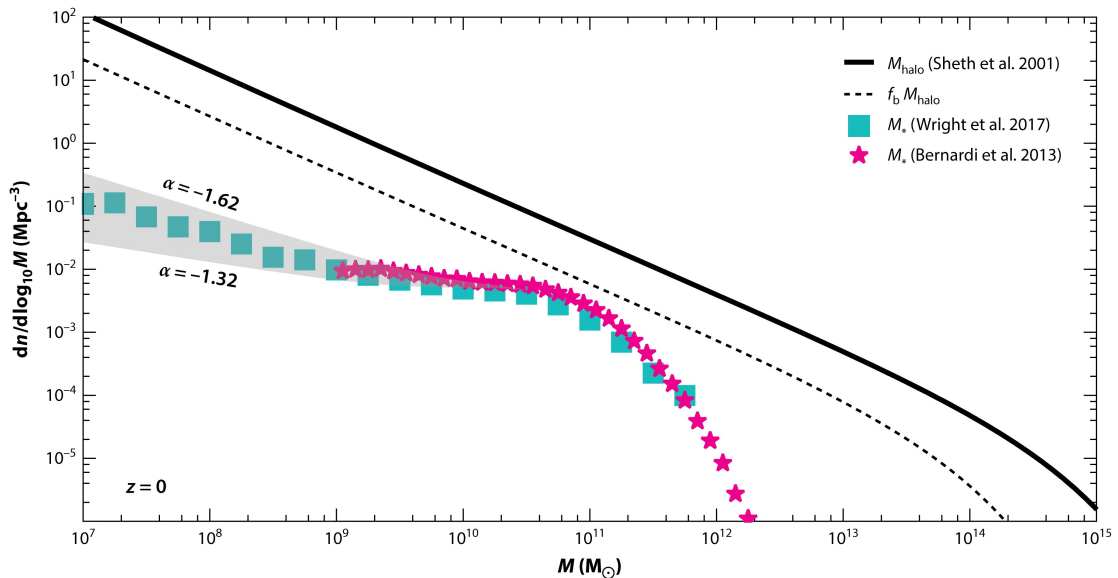


FIGURE 1.2: Comparing the dark matter halo mass function with galaxy stellar mass function. The thick black solid line is a theoretical dark halo mass function by [Sheth et al. \(2001\)](#), and the dashed black line is shifted by the baryon mass fraction. The observed galaxy stellar mass function is from [Bernardi et al. \(2013, magenta star\)](#) and [Wright et al. \(2017, cyan box\)](#). Reprinted from Figure 5 of [Bullock and Boylan-Kolchin \(2017\)](#) with permission.

than naively expected. This inefficiency suggests the existence of astrophysical feedback suppressing star formation.

There are some possible sources of feedback, e.g., stellar radiation, stellar wind, [SN](#), and [active galactic nucleus \(AGN\)](#). Among these possibilities, the [SN](#) is considered a dominant feedback source ([Dekel and Silk, 1986](#)). The galaxy stellar mass function suggests the existence of feedback, but it does not tell us about the physical process of feedback.

### 1.2.1.2 Galactic wind

A more direct observational evidence of [SN](#) feedback is the galactic winds. The galactic winds are the outflowing gas from galaxies driven by [SN](#) explosions, and they are observed in nearby and distant universes. Figure 1.3 shows the optical image of M82 galaxy, which has prominent galactic wind features due to its central starburst and subsequent [SN](#) explosions. The image is taken by the *Hubble* space telescope, and the orange filaments above and below the stellar disk indicate the hydrogen  $H\alpha$  emission from the galactic wind.

There are observations at multiple wavelengths, from X-ray to radio, tracing hot plasma to cold molecular cloud, for the M82 galaxy. [Shoppell and Bland-Hawthorn \(1998\)](#)



FIGURE 1.3: Observed image of M82 galaxy by the *Hubble* Space Telescope. The image is composed of four images taken with different filters; the red, green, and blue images are taken with wide band filters around 814, 555, and 435 nm, respectively, which capture starlight, and the orange image is taken with a narrow band filter at 658 nm, which captures the  $H\alpha$  line. From <https://hubblesite.org/contents/media/images/2006/14/1876-Image.html>. Image courtesy of NASA, ESA, and The Hubble Heritage Team (STScI/AURA). Acknowledgment: J. Gallagher (University of Wisconsin), M. Mountain (STScI), and P. Puxley (National Science Foundation). Public domain.

observed warm ( $\sim 10^4$  K) ionized gas emitting  $H\alpha$ , [N II], and [O III] spectral lines in optical wavelength. They measured the velocity of the outflowing optical filaments as seen in Figure 1.3 to be  $\sim 600 \text{ km s}^{-1}$ . Also, from their measurement of mass and length of filament, the mass outflow rate is estimated to be  $\sim 7 M_{\odot} \text{ yr}^{-1}$ , comparable to the star formation rate of M82. Strickland and Heckman (2009) observed hot ( $\gtrsim 10^7$  K) plasma in X-ray. Their measurement showed that the wind velocity of hot gas is  $\sim 2000 \text{ km s}^{-1}$ , considerably higher than that of warm ionized medium, and the mass outflow rate is  $\sim 2 M_{\odot} \text{ yr}^{-1}$ . Salak et al. (2013) observed cold ( $\sim 10$  K) molecular gas using CO emission line. The measured wind velocity was  $\sim 200 \text{ km s}^{-1}$ , and the mass outflow rate is estimated to be  $\sim 100 M_{\odot} \text{ yr}^{-1}$ , considerably higher than those of hot and ionized gas. These observations show that the galactic wind is multiphase in nature, with the hotter phase flowing faster and being less massive, while the colder phase has a

slower velocity and is more massive.

The different properties of different phases result in different feedback impacts on galaxy formation. The wind velocity of the hot phase is larger than the escape velocity of M82, and the hot phase can entrain mass, energy, and metals to the [intergalactic medium \(IGM\)](#). The cold phase has a smaller velocity, but it expels a lot of gas out from the galaxy. The mass loading efficiency of galactic wind is characterized by a ratio between the mass outflow rate and the star formation rate of the galaxy, which is termed mass loading factor,  $\eta_m = \dot{M}_{\text{wind}}/\dot{M}_*$ . The cold phase has  $\eta_m \sim 10$ , meaning that the gas, the fuel of star formation, is lost at a rate of 10 times faster than star formation. This massive outflow is considered to be one of the major mechanisms of supernova feedback, but its contribution is still under debate. The massive outflow can halt star formation by removing star-forming gas, but the gas falls back in a timescale of the order of Gyr, which is 10 times shorter than the cosmic age. Therefore, the galactic wind alone would not be enough to explain the low star formation efficiency in galaxies.

### 1.2.1.3 Superbubble

Stars are born in molecular clouds and form star clusters, and massive stars with more than  $8 M_{\odot}$  typically explode as core-collapse [SN](#) at the end of their life. In star clusters, multiple [SNe](#) occur clustered in space and time, and the clustered [SN](#) explosions form a large bubble called superbubble. The left panel in [Figure 1.4](#) shows the N44 superbubble in the [Large Magellanic Cloud \(LMC\)](#). There are contributions of stellar radiations and winds to form the superbubble, but the X-ray emission inside the superbubble indicates the energetic [SN](#) explosions in the past. The superbubble expands driven by the pressure of internal hot gas and sweeps up the surrounding [ISM](#). The superbubble eventually mixes with [ISM](#), adding kinetic energy to drive interstellar turbulence.

The size of the superbubble is approximately 300 pc, and in the right panel of [Figure 1.4](#), it is compared with the size of entire [LMC](#), whose diameter is roughly 4 kpc. Superbubbles are commonly observed in star-forming regions, and indeed many superbubbles can be found in the right panel of [Figure 1.4](#). Although each superbubble is small compared to the galaxy, multiple superbubbles occur across it, affecting its evolution.

## 1.2.2 Theoretical suggestion

In this subsection, I describe the theoretical works of feedback using simulations.





FIGURE 1.4: Left: The composite image of the N44 superbubble in the LMC. The purple and pink colors are X-ray images taken by the *Chandra* satellite, and the orange and light blue colors are optical images taken by the *Hubble* satellite. Credit: Enhanced Image by Judy Schmidt (CC BY-NC-SA) based on images provided courtesy of NASA/CXC/SAO & NASA/STScI. Right: The telescopic photograph of the LMC. Credit: Pablo Carlos Budassi, CC BY-SA 4.0, via Wikimedia Commons

### 1.2.2.1 Cosmological hydrodynamic simulation

The galaxy formation involves multiple astrophysical phenomena in the cosmological framework. To tackle these complexities, a powerful and direct approach has emerged in the form of cosmological hydrodynamical simulations. These simulations integrate gravity and hydrodynamics within the  $\Lambda$ CDM cosmology, while incorporating a range of astrophysical effects. This method has proved instrumental in advancing our comprehensive understanding of structure formation (for a technical review, see [Vogelsberger et al., 2020](#)).

Recent advances in cosmological hydrodynamical simulations have successfully reproduced key observed galaxy statistics, such as the galaxy stellar mass function as shown in Figure 1.5. Pioneering simulations like Illustris ([Genel et al., 2014](#)), Magneticum ([Hirschmann et al., 2014](#)), EAGLE ([Schaye et al., 2015](#)), MassiveBlack-II ([Khandai et al., 2015](#)), Horizon-AGN ([Kaviraj et al., 2017](#)), MUFASA ([Davé et al., 2016](#)), Romulus ([Tremmel et al., 2017](#)), IllustrisTNG ([Pillepich et al., 2018a](#)), SIMBA ([Davé et al., 2019](#)), ASTRID ([Bird et al., 2022](#)), FIREbox ([Feldmann et al., 2023](#)), MillenniumTNG ([Pakmor et al., 2023](#)), and FLAMINGO ([Schaye et al., 2023](#)) have shown remarkable

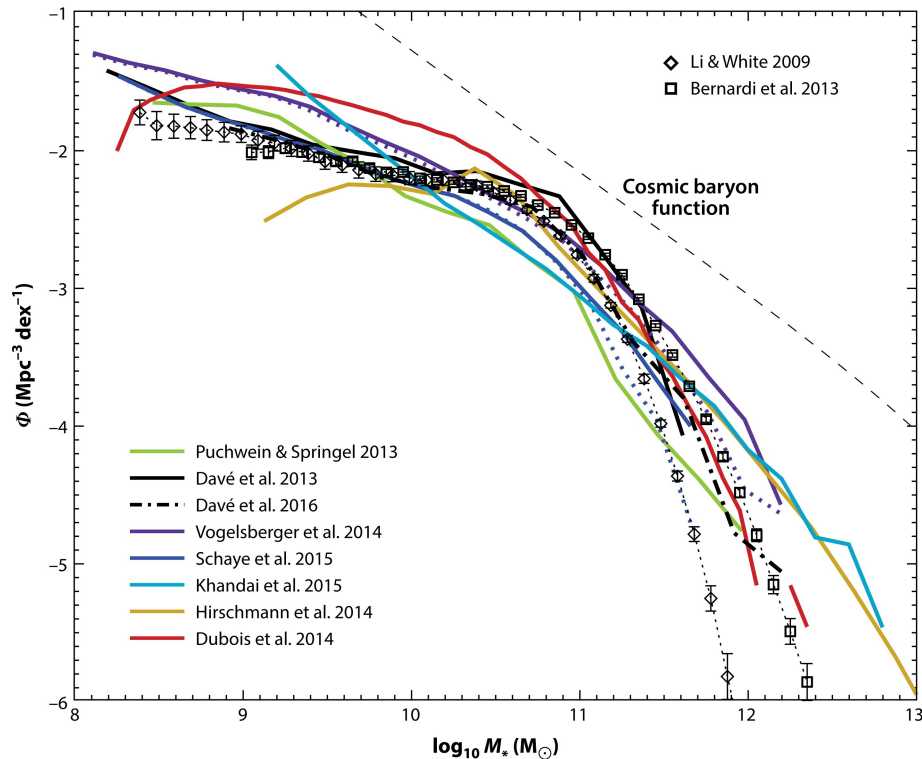


FIGURE 1.5: Comparing the predicted galaxy stellar mass functions from cosmological simulations at  $z = 0$ . The thick lines are the results of cosmological situations, and the dotted lines with points are observed galaxy stellar mass functions. The predicted galaxy abundance can vary by an order of magnitude, but they show general agreement with observations. Reprinted from Figure 4 of [Naab and Ostriker \(2017\)](#) with permission.

agreement with the observed galaxy stellar mass functions at various redshifts, but obtaining a perfect match at every redshift remains an ongoing challenge, reflecting the complexity and dynamic nature of galaxy evolution.

These simulations adopt the concordance  $\Lambda$ CDM cosmology and include a number of sophisticated subgrid models, including radiative cooling, extragalactic ultraviolet (UV) background radiation, star formation, and SN feedback. In addition, several of these simulations also integrate AGN feedback, adding a further layer of sophistication and fidelity to the simulation of galactic behavior and evolution.

The diverse but consistent success of several independent simulation projects, each using different subgrid models, has fostered a broad consensus within the scientific community. This consensus highlights the critical role of SN and AGN feedback in galaxy formation. The capability of these simulations to faithfully reproduce observed galaxy stellar mass functions, particularly through the calibration of feedback models, further underlines the central role of these phenomena in galaxy formation ([Somerville and Davé, 2015](#), [Naab and Ostriker, 2017](#)).

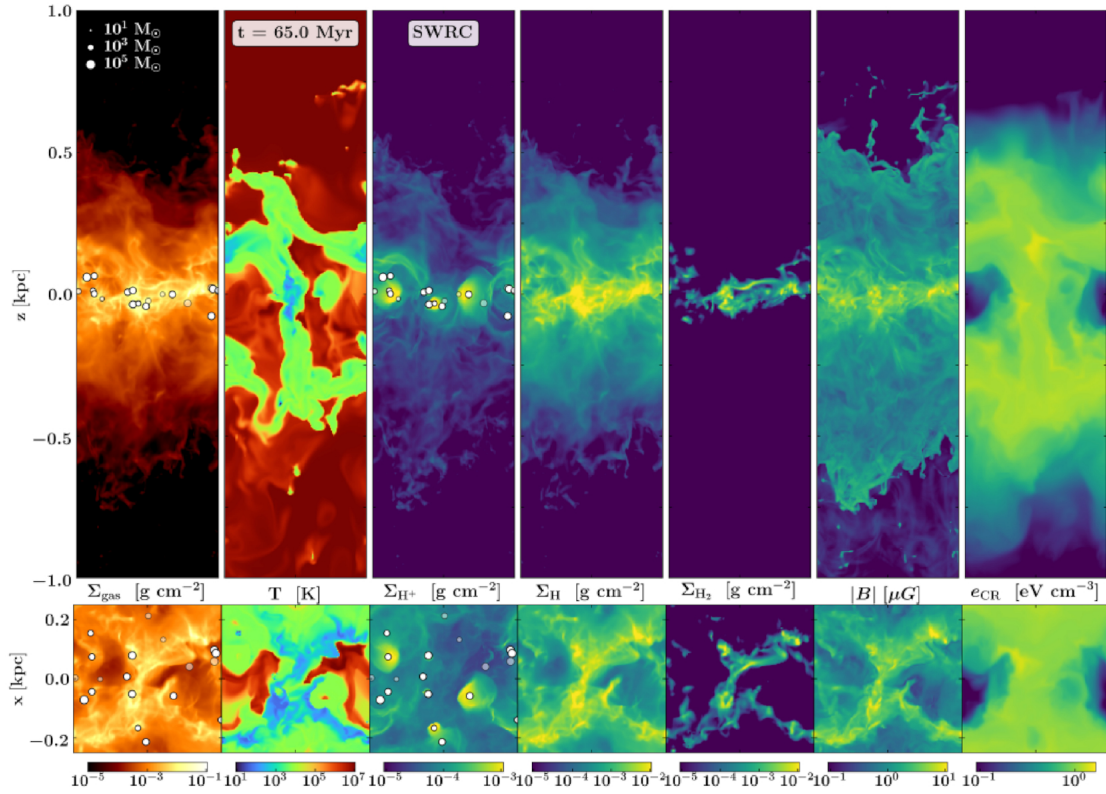


FIGURE 1.6: Overview of the SILCC high-resolution simulation. The simulation box has a size of  $0.5 \text{ kpc} \times 0.5 \text{ kpc} \times 4 \text{ kpc}$  and the resolution is  $4 \text{ pc}$ . Shown are the edge-on (top row) and face-on (bottom row) views of the total gas column density, temperature, ionized-, atomic-, and molecular hydrogen column densities, magnetic field strength, and cosmic ray energy density. The white circles in the first and third panels indicate star clusters with different masses. Reprinted from Figure 1 of Rathjen et al. (2021) with permission.

### 1.2.2.2 Small-box high-resolution simulation

The drawbacks of cosmological simulation are its low resolution and dependency on subgrid modeling. The small-box high-resolution simulations have a resolution of an order of  $1 \text{ pc}$ , small enough to resolve the Sedov–Taylor phase of a SN remnant, and they predict the outcome of feedback activities without depending on subgrid treatments, although sacrificing the spatial scale and cosmological context.

Figure 1.6 shows the overview of the SILCC simulation (Rathjen et al., 2021), simulating the ISM at solar neighborhood condition with star formation and stellar feedback in forms of stellar winds, ionizing radiation, SN, and cosmic rays. The resolution is high enough to resolve individual SN remnant, and a highly structured and turbulent multiphase ISM is naturally generated by the stellar feedback. They showed clustered SNe drives multiphase galactic wind, consistently with the observational facts as described in Section 1.2.1.2 and 1.2.1.3

Ostriker and Kim (2022) have investigated how the physical state of ISM is set by stellar feedback by analyzing their TIGRESS high-resolution simulations. They formulated the pressure balance of gravity, thermal pressure, and turbulent pressure due to momentum injection by SN feedback, finding agreement of their theory with simulations and observations. Their result indicates that the SN feedback maintains the suppressed star formation in the galactic disk by driving turbulence.

As described above, the high-resolution simulations give us deep insight into feedback physics. However, they neglect some important processes in galaxy evolution, like the recycling of outflowing gas, cosmic inflow, galactic merger, and the redshift evolution of galactic morphology due to their limited box size.

### 1.2.3 Challenges and future directions

As described in Section 1.2.2.1, cosmological simulations have successfully reproduced the observed galaxy stellar mass function (Section 1.2.1.1), and as described in Section 1.2.2.2, small-box high-resolution simulations have reproduced superbubble formed by clustered SN (Section 1.2.1.3) and the SN-driven multiphase galactic wind (Section 1.2.1.2). However, there are still disagreements between simulations and observations about the properties of circumgalactic medium (CGM) and IGM.

Figure 1.7 shows the physical state of IGM of cosmological simulations using ASTRID (Bird et al., 2022, Ni et al., 2022), IllustrisTNG (Weinberger et al., 2017, Pillepich et al., 2018b), and SIMBA (Davé et al., 2019) models, performed as a part of CAMELS project (Ni et al., 2023). The IGM temperature of the SIMBA run is visibly higher than those of others, reflecting the treatment of subgrid SN and AGN feedback. The difference between the ASTRID and TNG run is minor, but the cosmic filament is more diffused in the TNG run.

Butler Contreras et al. (2023) have used the CAMELS project data set (Villaescusa-Navarro et al., 2023) to study the O VII column density at low redshift ( $z < 0.3$ ) in simulations performed with the same code used for the IllustrisTNG and SIMBA simulations, and compared with the stacked *Chandra* observations of X-ray absorption lines on a line of sight of a background quasar from Kovács et al. (2019). They found that for a given H I column density, SIMBA predicts a lower O VII column density than the IllustrisTNG model by order of magnitude. They also found that the O VII column density in the simulations is lower than that observed by Kovács et al. (2019) by more than an order of magnitude, even for all ranges of SN and AGN feedback parameters explored in CAMELS.



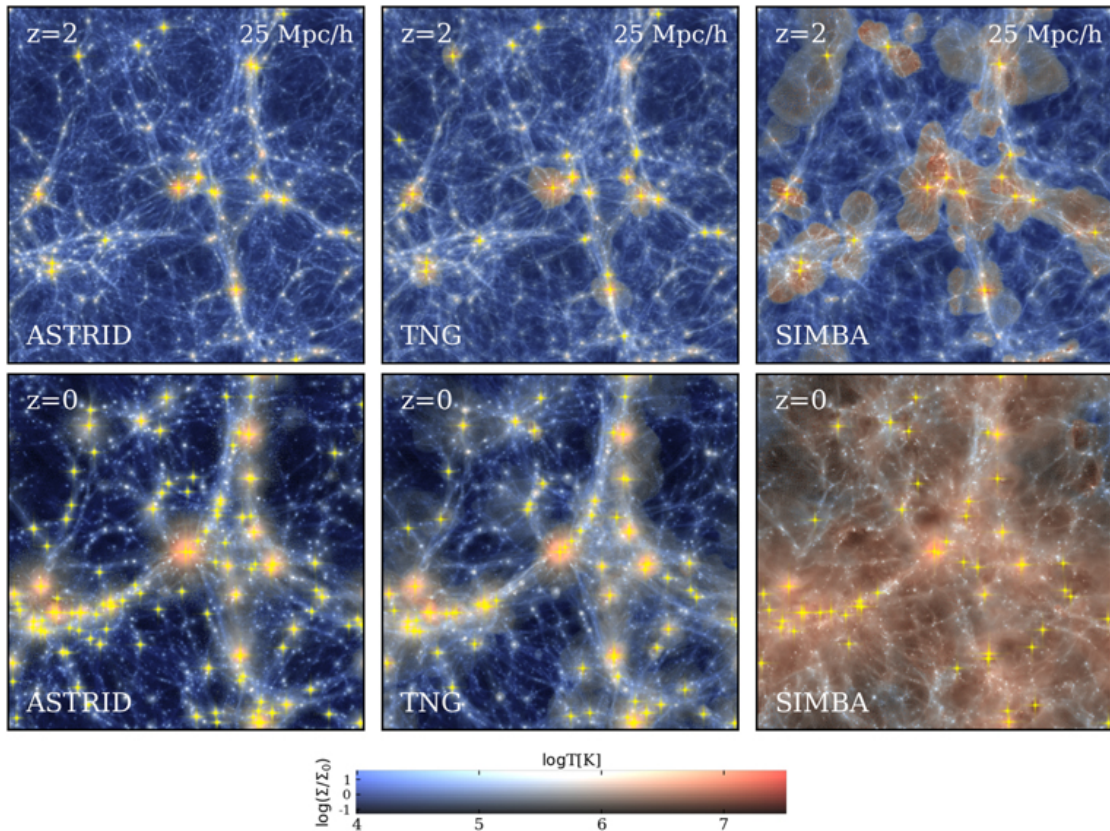


FIGURE 1.7: Comparison of the IGM simulated using ASTRID, IllustrisTNG, and SIMBA models. The intensity indicates the gas density, and the color indicates temperature (as indicated by the 2D color map) over the full box comoving volume of  $(25 h^{-1} \text{Mpc})^3$  at  $z = 2$  (top panels) and  $z = 0$  (bottom panels). The locations of massive BHs with  $M_{\text{BH}} > 10^8 M_{\odot}$  are marked by the yellow spikes. Reprinted from Figure 1 of Ni et al. (2023). CC BY 4.0.

Strawn et al. (2024) have analyzed a series of zoom-in simulations performed as part of the AGORA project (Roca-Fàbrega et al., 2021). These simulations were performed using a variety of simulation codes, both grid-based and particle-based, with various feedback models calibrated to match the values of the stellar-to-halo mass ratio predicted by the semi-empirical models. They have investigated column densities of four ions, namely Si IV, C IV, O VI, and Ne VIII, in the CGM. They found that there were considerable differences in the ion column densities between the simulations and the observations. At  $z = 3$ , the simulations differed by three orders of magnitude from the observations. They also found the ion column densities from the grid-based code generally to be higher than those from the particle-based code, with varying scatter due to different feedback prescriptions. The discrepancy in the properties of the CGM and IGM found in these works is due to the feedback models used in the simulations. Therefore, it is necessary to improve the feedback modeling based on small-scale physics.

The discrepancy seen in the IGM property in the simulations, in turn, indicates that the study of the IGM offers a distinct and robust means of constraining feedback physics.

Especially, the spatial distribution and abundance patterns of metals in the IGM serve as historical records of feedback activities. It is still a challenge to observe dilute IGM. However, it is possible to perform ‘IGM tomography,’ an observational technique to reconstruct the three-dimensional distribution of foreground absorbers from absorption lines on multiple lines of sight of galaxies and quasars (Lee et al., 2014, 2018, Newman et al., 2020). The advent of future wide-field and high-spectral-resolution IGM tomography utilizing advanced multiplexed fiber spectrographs such as Subaru/PFS (Greene et al., 2022), WHT/WEAVE (Jin et al., 2023), VLT/MOONS (Cirasuolo et al., 2014), MSE (The MSE Science Team et al., 2019), ELT/ANDES (Maiolino et al., 2013) and ELT/MOSAIC (Japelj et al., 2019) promises to revolutionize our understanding. These innovative tools are expected to reveal the intricate three-dimensional metal distribution within the IGM, providing unprecedented insights into the formation of cosmic structures.

Predicting the matter distribution from numerical simulations is necessary for deducing information on feedback physics from IGM tomographic observations. Nagamine et al. (2021) have highlighted the potential of IGM tomography as a powerful tool for probing feedback. They have used the GADGET3-OSAKA cosmological simulation (Shimizu et al., 2019) and revealed variations in the Ly $\alpha$  optical depth on small scales. These variations were affected by the details of the feedback model, as well as the treatment of gas self-shielding, star formation, and UV background radiation. While Nagamine et al. (2021) focused primarily on the distribution of neutral hydrogen, investigation of the metal distribution can give further insight into the feedback physics.

### 1.3 This thesis

In this thesis, I describe the development of a physically-motivated SN feedback model based on high-resolution simulations and cosmological simulation using the model. This thesis is based on our following two papers.

In Oku et al. (2022), we developed a SN feedback model based on high-resolution simulations. The adiabatic phase of a SN remnant is rarely resolved in cosmological simulations, and then the hydro-solver cannot resolve the conversion between kinetic and thermal energy. We thus consider the kinetic and thermal feedback effect of SN feedback respectively (see also Chaikin et al., 2023). The kinetic feedback takes into account the momentum of a superbubble formed by clustered SNe, driving interstellar turbulence. The thermal feedback accounts for the fact that some superbubbles break out of the galactic disk to generate hot galactic winds, as observed in M82 (Strickland and Heckman, 2009). In simulations of Milky Way-mass isolated galaxies, we have shown that the

kinetic feedback supports a galactic disk against gravitational collapse to suppress star formation, and the thermal feedback drives the hot metal-rich galactic wind.

In Oku and Nagamine (2024), we have introduced the CROCODILE<sup>1</sup> (Cosmological hydrodynamical simulation of structure formation and feedback physics in galaxy Evolution) cosmological simulation. This CROCODILE is performed using the GADGET4-OSAKA smoothed particle hydrodynamics (SPH) code (Romano et al., 2022a,b, a modified version of GADGET-4, Springel et al. 2021), which features our updated SN feedback model developed in Oku et al. (2022) and includes the active galactic nuclei (AGN) feedback model following Rosas-Guevara et al. (2015), Schaye et al. (2015), Crain et al. (2015). Oku and Nagamine (2024) have demonstrated CROCODILE’s capability in reproducing essential galaxy statistics and investigated the impacts of SN and AGN feedback on the metal enrichment of the IGM.

This thesis is organized as follows: Chapter 2 describe the development of our SN feedback model. Chapter 3 details the methodology of our cosmological simulation CROCODILE, including the numerics and the subgrid models for stellar feedback and black holes. In Chapter 4, we present the results of our CROCODILE simulations, with a focus on the basic statistical properties of galaxies to validate our simulation framework. In Chapter 5, we analyze the distribution of metals in the IGM in CROCODILE. We highlight the impact of SN and AGN feedback, and this section serves as a preliminary study, setting the theoretical groundwork for future tomographic surveys. Our findings are summarized, and future research directions are outlined in Chapter 6. Additionally, Appendix A discusses the evolution of a superbubble in idealized ISM, which serves as a basis of our SN feedback model. Appendix B describes the technical details of introducing feedback in simulation.

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<sup>1</sup>Named in homage to Osaka University’s official mascot, Dr. Wani, a crocodile (<https://www.osaka-u.ac.jp/sp/drwani/en/>)



OSAKA UNIVERSITY mascot Dr. Wani as a science member

## Chapter 2

# Supernova feedback model

In this chapter, we discuss the supernova feedback model developed in [Oku et al. \(2022\)](#).

### 2.1 Necessity of feedback model

Due to a lack of resolution, it is challenging to spatially and temporally resolve SN explosions in galaxy formation simulations. SN explosions were modeled as thermal energy injections in the early days of cosmological galaxy simulation (i.e., the 1990s) ([Cen and Ostriker, 1992](#), [Katz et al., 1996](#), [Cen and Ostriker, 1999](#)). However, the thermal energy was dissipated and radiated away as soon as it was injected due to low resolution (i.e., the overcooling problem, [Katz, 1992](#)).

Here, we analytically calculate the mass resolution requirement for thermal and kinetic feedback. [Dalla Vecchia and Schaye \(2012\)](#) estimated the resolution necessary for effective thermal feedback. They compared the sound-crossing time,  $t_s$ , with the cooling time,  $t_c$ . The sound-crossing time across a scale of spatial resolution  $\Delta x = (m_{\text{gas}}/\rho)^{1/3}$  is

$$\begin{aligned} t_s &= \frac{\Delta x}{c_s} = \left( \frac{\mu m_{\text{H}}}{\gamma k_{\text{B}} T} \right)^{\frac{1}{2}} \left( \frac{m_{\text{gas}}}{\rho} \right)^{\frac{1}{3}} \\ &= 1.0 \times 10^5 \text{ yr} \times \left( \frac{\mu}{0.59} \right)^{\frac{1}{6}} \left( \frac{T}{10^{7.5} \text{ K}} \right)^{-\frac{1}{2}} \left( \frac{m_{\text{gas}}}{10^4 \text{ M}_{\odot}} \right)^{\frac{1}{3}} \left( \frac{n_{\text{H}}}{1 \text{ cm}^{-3}} \right)^{-\frac{1}{3}}, \end{aligned} \quad (2.1)$$

where  $c_s$  is the local sound speed. The cooling time is

$$t_c = \frac{nk_{\text{B}}T}{(\gamma - 1)\Lambda_{ff}}, \quad (2.2)$$

where  $\Lambda_{ff}$  is the cooling rate by bremsstrahlung. Here, the cooling time of gas with  $T > 10^7 \text{ K}$  is considered, where bremsstrahlung is the dominant cooling process. Note



that this cooling time is not the cooling time of a point explosion, i.e., the shell-formation time for a SN remnant. We compare the sound-crossing time to the cooling time for a gas particle with fixed density to evaluate if the heated gas particle cools down within the simulation time step. The overcooling can be avoided if the cooling time is longer than the simulation time step. However, as discussed later in this section, avoiding overcooling does not ensure that we resolve the Sedov–Taylor phase.

The cooling rate by bremsstrahlung is (Draine, 2011)

$$\Lambda_{ff} = 1.14 \times 10^{-23} \text{ erg cm}^{-3} \text{ s}^{-1} \left( \frac{n_{\text{H}}}{1 \text{ cm}^{-3}} \right)^2 \left( \frac{T}{10^{7.5} \text{ K}} \right)^{1/2}, \quad (2.3)$$

where we have assumed that the number density ratio of hydrogen to helium is 10:1, the plasma is fully ionized, and the gaunt factor is 1.19. Combining Eq. (2.2) and (2.3), we obtain the cooling time as:

$$t_c = 4.2 \times 10^7 \text{ yr} \left( \frac{n_{\text{H}}}{1 \text{ cm}^{-3}} \right)^{-1} \left( \frac{T}{10^{7.5} \text{ K}} \right)^{1/2}. \quad (2.4)$$

The ratio between the sound-crossing and cooling times is:

$$\frac{t_c}{t_s} = 4.2 \times 10^2 \times \left( \frac{\mu}{0.59} \right)^{-1/6} \left( \frac{n_{\text{H}}}{1 \text{ cm}^{-3}} \right)^{-2/3} \left( \frac{T}{10^{7.5} \text{ K}} \right) \left( \frac{m_{\text{gas}}}{10^4 M_{\odot}} \right)^{-1/3}. \quad (2.5)$$

The thermal feedback becomes effective if the cooling time is sufficiently longer than the sound-crossing time,  $t_c/t_s > 10$ , which translates to

$$T > 7.5 \times 10^5 \text{ K} \left( \frac{\mu}{0.59} \right)^{1/6} \left( \frac{n_{\text{H}}}{1 \text{ cm}^{-3}} \right)^{2/3} \left( \frac{m_{\text{gas}}}{10^4 M_{\odot}} \right)^{1/3}. \quad (2.6)$$

The criterion temperature  $T = 7.5 \times 10^5 \text{ K}$  is lower than the temperature where metal line radiative cooling dominates over bremsstrahlung. Therefore, thermal feedback is effective when it is energetic enough to heat a gas particle to  $T > 10^{7.5} \text{ K}$ .

The condition for kinetic feedback is more stringent than that for thermal feedback. Kim and Ostriker (2015) performed 3D simulations using the ATHENA code (Stone et al., 2008) and studied the resolution dependence of the terminal momentum of a SN remnant. They showed that the criterion for the terminal momentum to be converged within 25% is  $\Delta x/R_{\text{sf}} < 1/3$ , where  $\Delta x$  is the spatial resolution, and  $R_{\text{sf}}$  is the shell-formation radius (Eq. A.7). This criterion can be converted to the mass resolution requirement in SPH:

$$\frac{(m_{\text{gas}}/\rho)^{1/3}}{23 E_{51}^{0.29} n_0^{-0.42} \Lambda_{6,-22}^{-0.13} \text{ pc}} < \frac{1}{3}, \quad (2.7)$$

where  $m_{\text{gas}}$  is the SPH particle mass. Solving this inequation for  $m_{\text{gas}}$ , we obtain

$$m_{\text{gas}} < 6.6 M_{\odot} \left( \frac{\mu}{0.59} \right) n_0^{-0.26} E_{51}^{0.87} \Lambda_{6,-22}^{-0.39}. \quad (2.8)$$

Hu (2019) investigated the resolution dependence of the terminal momentum of a SN remnant. They used their modified version of GADGET-3 SPH code and simulated the remnant formed by a SN explosion with  $E_{\text{SN}} = 10^{51}$  erg in a uniform medium of  $n_{\text{H}} = 1 \text{ cm}^{-3}$  at four mass resolutions,  $m_{\text{gas}} = 0.1, 1, 10,$  and  $100 M_{\odot}$ . They found the convergence of the terminal momentum in the cases of  $m_{\text{gas}} = 0.1,$  and  $1 M_{\odot}$ . The terminal momentum in the case of  $m_{\text{gas}} = 10 M_{\odot}$  was about 15% smaller than that for  $m_{\text{gas}} = 0.1,$  and  $1 M_{\odot}$ , and this result is roughly consistent with the criterion in Eq. (2.8). The reason for the 15% convergence of the terminal momentum in the case of  $m_{\text{gas}} = 10 M_{\odot}$  might be because the spatial resolution of SPH becomes better in a dense shell. In the case of lowest resolution at  $m_{\text{gas}} = 100 M_{\odot}$ , the terminal momentum is underestimated by a factor of three due to overcooling.

We can also solve Eq. (2.7) for  $E (= E_{51} \times 10^{51} \text{ erg})$  to find the injection energy large enough to generate an explosion that can be resolved with the given mass resolution  $m_{\text{gas}}$ :

$$E > 4.5 \times 10^{54} \text{ erg} \left( \frac{\mu}{0.59} \right)^{-1.2} \left( \frac{m_{\text{gas}}}{10^4 M_{\odot}} \right)^{1.2} n_0^{0.30} \Lambda_{6,-22}^{0.45}, \quad (2.9)$$

and obtain the temperature at which the criterion is satisfied:

$$T = \frac{\mu m_{\text{H}}}{(\gamma - 1) m_{\text{gas}} k_{\text{B}}} \frac{E}{m_{\text{gas}}} > 1.6 \times 10^9 \text{ K} \left( \frac{\mu}{0.59} \right)^{-0.2} \left( \frac{m_{\text{gas}}}{10^4 M_{\odot}} \right)^{0.2} n_0^{0.3} \Lambda_{6,-22}^{0.45}. \quad (2.10)$$

This temperature is much higher than the temperature needed for the thermal feedback to be effective (Eq. 2.6), meaning that the condition for kinetic feedback is more difficult to realize in actual simulations.

## 2.2 Main idea of modeling

To model SN feedback, we must consider what to model. As described in Figure 2.1, SN feedback affects galaxy evolution via both kinetic feedback (driving turbulence) and thermal feedback (generating hot bubbles and outflows). When the resolution is high enough to resolve the Sedov–Taylor phase, its kinetic and thermal energies get converted to one another, and the difference between the thermal and kinetic form, or a combination of both forms, is negligible (Durier and Dalla Vecchia, 2012). However, in most cases of cosmological galaxy simulations, such small scales cannot be resolved as we described in Section 2.1. Hence, we need to include both kinetic and thermal feedbacks in the



FIGURE 2.1: Schematic image of the idea of supernova feedback model.

SN feedback model. We note that simply distributing thermal energy is ineffective (Hu, 2019) because it leaves the mass of the SN ejecta unresolved in simulations, as long as we use simple stellar population (SSP) approximation and the particle masses of stars and gas are comparable (Dalla Vecchia and Schaye, 2012). Therefore, the effective modeling of thermal feedback is necessary.

## 2.3 Mechanical feedback

In this section, we develop a mechanical feedback model based on high-resolution superbubble simulation using ATHENA++ code. The simulation is performed as a part of my master thesis work, and the details of the simulation, as well as the basic analytic theory of superbubble evolution, is described in Appendix A to avoid the duplication in theses in main contents and clarify the contribution made in PhD course.

### 2.3.1 Averaged momentum per SN for a stellar population

From the fitting function in Appendix A.2.3, we derive the expression for momentum of a superbubble per SN, averaged over an initial stellar cluster mass function (ICMF). We assume the ICMF to be described by the power-law  $dN/dM_c \propto M_c^{-2}$  with high-mass cutoff, where  $M_c$  is the mass of the stellar cluster (Krumholz et al., 2019) and stellar initial mass function (IMF) is fixed. We also assume SNe occurs at a constant rate. The ICMF can be translated to an SN number function (probability distribution function of the number of SN explosions occurring in a stellar cluster)

$$\frac{dN}{dN_{\text{SN}}} = AN_{\text{SN}}^{-2}, \quad (2.11)$$

where  $N_{\text{SN}}$  is the number of SN explosions occurring in a stellar cluster and  $A$  is the normalization factor. The range of the number of SN explosions is assumed as  $N_{\text{SN}} = N_{\text{SN,min}} - N_{\text{SN,max}}$ , where we adopt the range of  $(N_{\text{SN,min}}, N_{\text{SN,max}}) = (1, 500)$ , and the normalization factor is  $A = 1/\ln 500$ . The value of  $N_{\text{SN,max}} = 500$  is the number of SN explosions expected to happen in the largest young massive star cluster (YMC) in the Milky way with a mass of  $M = 5 \times 10^4 M_{\odot}$  (Portegies Zwart et al., 2010). The choice of high-mass cutoff has little effect on the result since such high-mass YMCs are rare objects. The SN interval is obtained by dividing their duration by their number,  $\Delta t_{\text{SN}} = (t_{\text{SN,end}} - t_{\text{SN,start}})/N_{\text{SN}}$ , where  $t_{\text{SN,start}}, t_{\text{SN,end}}$  are the times at the first and the last Type II SN after the formation of the stellar cluster, i.e., the minimum and the maximum lifetimes of stars causes Type II SNe. The lifetimes of stars depend on their mass and metallicity. We calculate SNe duration using CELIB<sup>1</sup> (Saitoh, 2017), which compute it using the metallicity-dependent stellar lifetime table by Portinari et al. (1998). We assume the mass range of the progenitors of Type II SNe to be 13–40  $M_{\odot}$ . In the range of  $Z = 10^{-6}$ – $10^{-2}$ , SNe duration is

$$t_{\text{SN,end}} - t_{\text{SN,start}} \sim 1.2 \times 10^7 \text{ yr}. \quad (2.12)$$

Single SN explosion energy is set to  $10^{51}$  erg. The average momentum per SN is

$$\hat{p}(n_0, Z) = \int_{N_{\text{SN,min}}}^{N_{\text{SN,max}}} p(n_0, Z, \Delta t_{\text{SN}}(N'_{\text{SN}})) \frac{dN}{dN'_{\text{SN}}} dN'_{\text{SN}}. \quad (2.13)$$

The final integral is well-fitted by the following function:

$$\hat{p}(n_0, Z) = 1.75 \times 10^5 M_{\odot} \text{ km s}^{-1} n_0^{-0.05} \Lambda_{6,-22}^{-0.17}, \quad (2.14)$$

and the momentum input by  $\mathcal{N}_{\text{SN}}$  SNe (superbubble momentum,  $p_{\text{SB}}$ ) is estimated as

$$p_{\text{SB}}(\mathcal{N}_{\text{SN}}, n_0, Z) = \mathcal{N}_{\text{SN}} \hat{p}(n_0, Z). \quad (2.15)$$

Here, we used a slightly different font of  $\mathcal{N}_{\text{SN}}$  for the total number of SNe for a star particle in the simulation (i.e., a collection of stellar clusters, rather than a population of stars in a single stellar cluster).

### 2.3.2 Shock radius for a star particle

We similarly calculate the shock radius of SN feedback of a star particle. Assuming that stellar clusters follow the power-law ICMF, we determine the shock radius of the SN

<sup>1</sup><https://bitbucket.org/tsaitoh/celelib>

feedback as the radius of a sphere whose volume is the sum of those of the superbubbles. We first consider the averaged volume shocked by SN feedback *per SN* considering the variation of superbubbles created by a range of star clusters:

$$\hat{V}(n_0, Z) = \int_{N_{\text{SN},\text{min}}}^{N_{\text{SN},\text{max}}} \frac{4}{3}\pi R(n_0, Z, \Delta t_{\text{SN}}(N'_{\text{SN}}))^3 \frac{dN}{dN'_{\text{SN}}} dN'_{\text{SN}}. \quad (2.16)$$

Then the effective radius is obtained as

$$\hat{R}(n_0, Z) = \left( \frac{3\hat{V}}{4\pi} \right)^{1/3} = 61 \text{ pc } n_0^{-0.22} \Lambda_{6,-22}^{-0.04}, \quad (2.17)$$

and the shock radius by  $\mathcal{N}_{\text{SN}}$  SNe is calculated as

$$R(\mathcal{N}_{\text{SN}}, n_0, Z) = \mathcal{N}_{\text{SN}}^{1/3} \hat{R}(n_0, Z). \quad (2.18)$$

Here,  $\mathcal{N}_{\text{SN}}$  is meant to be the number of SNe occurring in the stellar population of a star particle. Since Eq. (2.16) gives the averaged superbubble volume *per SN*, the effective volume for  $\mathcal{N}_{\text{SN}}$  SNe for a star particle would be  $\mathcal{N}_{\text{SN}}\hat{V}$  and the effective radius would be  $\mathcal{N}_{\text{SN}}^{1/3}\hat{R}$  as given in Eq. (2.18).

### 2.3.3 Feedback assignment

We use the ‘Spherical superbubble model’ described in Appendix B to assign physical quantities related to feedback. Using the superbubble momentum  $p_{\text{SB}}$  computed in Eq. (2.15), we deposit the following momentum on the  $i$ -th gas particle:

$$\Delta \mathbf{p}_i = p_{\text{SB}} \frac{\Omega_i}{4\pi} \mathbf{n}_i, \quad (2.19)$$

where  $\mathbf{n}_i$  is the normal vector of the face on the Voronoi polyhedron. When the number of neighboring gas particles falls below four (which prevents the construction of a Voronoi polyhedron), we inject the same amount of momentum and determine  $\mathbf{n}_i$  so that the total momentum is conserved. The total momentum of the surrounding gas should be conserved before and after the SN event. For this, we compute the total momentum input as:

$$\Delta \mathbf{p}_{\text{tot}} = \sum_i \Delta \mathbf{p}_i, \quad (2.20)$$

and modify momentum input to  $i$ -th gas particle to

$$\Delta \mathbf{p}'_i = \Delta \mathbf{p}_i - \frac{\Omega_i}{4\pi} \Delta \mathbf{p}_{\text{tot}}. \quad (2.21)$$

The kinetic energy input by momentum kick may exceed the SN energy input due to particle distribution. Thus, we limit the momentum input to each neighboring particle based on the Sedov–Taylor solution. The resulting momentum input is:

$$\Delta \mathbf{p}_i'' = \frac{\Delta \mathbf{p}_i'}{|\Delta \mathbf{p}_i'|} \min \left( |\Delta \mathbf{p}_i'|, \sqrt{2(m_i + \Delta m_i) \Delta E_{\text{kin},i}} \right), \quad (2.22)$$

where  $m_i$  is the mass of the  $i$ -th gas particle and  $\Delta E_{\text{kin},i}$  is the solid-angle-weighted kinetic energy from SN feedback.  $\Delta E_{\text{kin},i}$  is given as

$$\Delta E_{\text{kin},i} = \epsilon_{\text{kin}} E_{\text{SN}} \frac{\Omega_i}{4\pi}, \quad (2.23)$$

where  $\epsilon_{\text{kin}}$  is a fraction of the SN energy deposited as kinetic energy, and we adopt  $\epsilon_{\text{kin}} = 0.3$  as the default value (Shimizu et al., 2019). Equation (2.22) essentially corresponds to equation (A1) in Kimm and Cen (2014) and equation (32) in Hopkins et al. (2018).

The momentum input above is calculated with respect to the frame moving with the star particle. To ensure exact conservation, we require a term accounting for the relative motion between the gas and the star (Hopkins et al., 2018). Finally, the momentum input boosted back to the simulation frame is

$$\Delta \mathbf{p}_i''' = \Delta \mathbf{p}_i'' + \Delta m_i \mathbf{v}_{\text{star}}, \quad (2.24)$$

where  $\mathbf{v}_{\text{star}}$  is the star velocity.

In summary, we first compute  $\Delta \mathbf{p}_i$  for the momentum that we want to assign the neighboring gas particles with. Then  $\Delta \mathbf{p}_i'$  makes it isotropic, and we ensure energy conservation by  $\Delta \mathbf{p}_i''$ . Finally,  $\Delta \mathbf{p}_i'''$  takes care of the motion of the originating stellar particle. By giving  $\Delta \mathbf{p}_i'''$ , the momentum feedback is basically guaranteed to be isotropic, energy-conserving, and momentum-conserving.

To be more specific, it is possible that momentum conservation could be broken when the second term in the RHS of Eq. (2.22) is chosen. However, such a situation does not arise very often because we do not have sufficient to resolve the Sedov–Taylor phase. In fact, we have checked our isolated galaxy simulations performed in Section 2.5, the second term was chosen only  $3.4 \times 10^{-5} \%$  of the cases for the Fiducial run, and  $1.1 \times 10^{-4} \%$  for the High-reso run.

## 2.4 Galactic wind feedback

Several groups have studied the SN-driven outflow using high-resolution small-box simulations. Hu (2019) investigated SN-driven outflow of a dwarf galaxy. They showed the entropy  $S \equiv k_B T n^{1-\gamma}$  of the hot outflow to be  $10^8 - 10^9 k_B \text{ K cm}^2$ , and it is almost constant after being launched from the galaxy. Although their result is on a dwarf galaxy, the energy loading factor and specific energy of the hot outflow by Hu (2019) are similar to those of a Milky-way-mass galaxy (Li et al., 2017, Armillotta et al., 2019, Kim and Ostriker, 2018, Kim et al., 2020b), according to Li and Bryan (2020).

It is suggested that the hot outflow is driven by buoyancy and its entropy is its fundamental physical quantity; if the entropy of the hot bubble is higher than that of the surrounding CGM, the hot bubble becomes buoyant and drives the outflow (Bower et al., 2017). Keller et al. (2020) analytically calculated the entropy of superbubbles and the virialized Milky-way-mass halos to be about  $10^8 k_B \text{ K cm}^2$ . The buoyancy-driven outflow framework is supported by the MUGS2 simulations (Keller et al., 2015, 2016), and the framework may explain the ineffectiveness of SN feedback in halos more massive than  $10^{12} M_\odot$  (Keller et al., 2020).

In this work, we update the stochastic thermal feedback model (Dalla Vecchia and Schaye, 2012) by using the entropy of hot outflow  $S_{\text{OF}}$  as a free parameter, setting  $S_{\text{OF}} = 10^8 k_B \text{ K cm}^2$  as the default value. When SN feedback occurs, thermal energy is stochastically injected to heat neighboring particles to target entropy,  $S_{\text{OF}}$ . The thermal energy required to heat the  $i$ -th gas particle is

$$\Delta E_{\text{req},i} = \frac{1}{\gamma - 1} \frac{m_i}{\mu m_H} n_i^{2/3} S_{\text{OF}}, \quad (2.25)$$

where  $n_i$  is the number density of the  $i$ -th gas particle. The probability of injecting thermal energy is the ratio between the solid-angle-weighted thermal energy from SN feedback (Appendix B),

$$\Delta E_{\text{th},i} = \epsilon_{\text{th}} E_{\text{SN}} \frac{\Omega_i}{4\pi}, \quad (2.26)$$

and the required thermal energy:

$$P_i = \frac{\Delta E_{\text{th},i}}{\Delta E_{\text{req},i}}, \quad (2.27)$$

where  $\epsilon_{\text{th}} = 1 - \epsilon_{\text{kin}}$  is a fraction of the SN energy deposited as thermal energy, and we adopt  $\epsilon_{\text{th}} = 0.7$  as the default value (Shimizu et al., 2019). We draw a random number  $0 < \theta_i < 1$  for each gas particle, and inject thermal energy  $\Delta E_{\text{req},i}$  to  $i$ -th gas particle if  $\theta_i < P_i$ . When  $P_i > 1$ , we simply inject a thermal energy of  $\Delta E_{\text{th},i}$  to the  $i$ -th gas particle.

The original stochastic thermal feedback model by [Dalla Vecchia and Schaye \(2012\)](#) uses temperature increase  $\Delta T$  as a free parameter and stochastically heats gas that magnitude. Their default value  $\Delta T = 10^{7.5}$  K was set for a numerical reason; the expectation value for the number of heated gas particles per SN is about 1. If this value is much smaller than 1, most SN feedback events do not inject energy into their surroundings, leading to poor sampling of the SN feedback cycle ([Schaye et al., 2015](#)). Although they provide a good reason to use  $\Delta T$  as a parameter for their stochastic feedback model, the outflow properties depend on  $\Delta T$  ([Dalla Vecchia and Schaye, 2012](#)), and a better parameter choice is desired. In this work, we use outflow entropy as a free parameter, motivated by the high-resolution simulations ([Hu, 2019](#)) and buoyancy-driven outflow framework ([Bower et al., 2017](#), [Keller et al., 2020](#)).

## 2.5 Isolated galaxy simulation with GADGET3-OSAKA

In this section, we implement the SN feedback model based on the high-resolution ATHENA++ simulations described in the earlier sections and demonstrate its effect on star formation and galactic outflow in an isolated galaxy simulation.

### 2.5.1 Simulation Setup

We use the GADGET3-OSAKA cosmological SPH code ([Aoyama et al., 2017](#), [Shimizu et al., 2019](#)), which is a modified version of GADGET-3 (originally described in [Springel 2005](#), as GADGET-2<sup>2</sup>). We solve the SPH equation of motion, following the entropy-conserving, density-independent SPH formulation ([Hopkins, 2013](#), [Saitoh and Makino, 2013](#)):

$$\frac{d\mathbf{v}_i}{dt} = - \sum_j m_j (S_i S_j)^{1/\gamma} \left[ \frac{f_{ij} \bar{P}_i}{\bar{P}_i^{2/\gamma}} \nabla_i W(r_{ij}, h_{\text{sml},i}) + \frac{f_{ji} \bar{P}_j}{\bar{P}_j^{2/\gamma}} \nabla_i W(r_{ij}, h_{\text{sml},j}) \right], \quad (2.28)$$

$$f_{ij} = 1 - \frac{h_{\text{sml},i}}{3S_j^{1/\gamma} \rho_i} \frac{\partial \bar{P}_i^{1/\gamma}}{\partial h_{\text{sml},i}} \left( 1 + \frac{h_{\text{sml},i}}{3\rho_i} \frac{\partial \rho_i}{\partial h_{\text{sml},i}} \right)^{-1}, \quad (2.29)$$

where  $m_i$ ,  $\mathbf{v}_i$ ,  $S_i$ ,  $h_{\text{sml},i}$ , and  $\bar{P}_i$  denote the mass, velocity, entropy (defined as  $S \equiv \bar{P}/\rho^\gamma$ ), smoothing length, and smoothed pressure defined as

$$\bar{P}_i = \left[ \sum_j m_j S_j^{1/\gamma} W(r_{ij}, h_{\text{sml},i}) \right], \quad (2.30)$$

<sup>2</sup><https://wwwmpa.mpa-garching.mpg.de/gadget/>



of the  $i$ -th gas particle, respectively. In this formulation, the thermal energy of a particle is computed from its entropy and smoothed pressure. When thermal feedback injects energy, updating entropy assuming fixed pressure leads to the wrong result because the smoothed pressure field itself depends on the entropy. Therefore, we use an iterative method to calculate entropy change by energy injection from feedback and energy dissipation by radiative cooling (Schaye et al., 2015, Borrow et al., 2021). The self-gravity of SPH and collisionless particles are also considered. We adopt the quintic B-spline kernel (Schoenberg, 1946, Morris, 1996), and set the number of neighboring particles for each SPH particle to  $N_{\text{ngb}} = 128 \pm 8$ . Our code includes the time-step limiter (Saitoh and Makino, 2009, Durier and Dalla Vecchia, 2012).

Radiative cooling is calculated using the GRACKLE-3 chemistry and cooling library<sup>3</sup> (Smith et al., 2017), which solves non-equilibrium primordial chemistry and cooling for the H, D, and He species, including molecular H<sub>2</sub> and HD. The library also includes tabulated rates of metal cooling calculated with the photoionization code CLOUDY (Ferland et al., 2013) and photoheating and photoionization from the UV background radiation, and we adopt the UV background value at  $z = 0$  by Haardt and Madau (2012). We applied a nonthermal Jeans pressure floor that forces the local Jeans length to be resolved to avoid artificial numerical fragmentation (Hopkins et al., 2011, Kim et al., 2016):

$$P_{\text{Jeans}} = \frac{1}{\gamma\pi} N_{\text{Jeans}}^2 G \rho_{\text{gas}}^2 \Delta x^2, \quad (2.31)$$

where  $\gamma = 5/3$  is the adiabatic index,  $N_{\text{Jeans}} = 4$  is the Jeans number adopted from Truelove et al. (1997),  $G$  is the gravitational constant, and  $\rho_{\text{gas}}$  is the gas density.  $\Delta x$  is chosen from the larger one of either the gravitational softening length of an SPH particle or the spatial resolution of hydrodynamics  $(m_{\text{gas}}/\rho_{\text{gas}})^{1/3}$ , where  $m_{\text{gas}}$  is the mass of the gas particle.

We used an initial condition taken from the AGORA project<sup>4</sup> (Kim et al., 2016). The galaxy has properties characteristic of Milky Way-mass galaxies at redshift  $z \sim 1$ . The galaxy is composed of the following components: a dark matter halo with  $M_{\text{DM}} = 1.25 \times 10^{12} M_{\odot}$ , a stellar disk with  $M_{\text{disc}} = 4.30 \times 10^9 M_{\odot}$ , a stellar bulge with  $M_{\text{bulge}} = 3.44 \times 10^{10} M_{\odot}$ , and a gas disk with  $M_{\text{gas}} = 8.59 \times 10^9 M_{\odot}$ . The total mass of the galaxy is  $1.3 \times 10^{12} M_{\odot}$ . In the fiducial run, we employed  $10^5$  dark matter particles,  $10^5$  gas (SPH) particles, and  $10^5$  and  $1.25 \times 10^4$  collisionless particles representing the stars in the disk and the bulge, respectively. We also added a hot gaseous halo following Shin

<sup>3</sup><https://grackle.readthedocs.io>

The default solar metallicity in GRACKLE-3 is  $Z_{\odot} = 0.0134$ . This value is smaller than the value of  $Z_{\odot}$  that was used in Eq. (A.10) by a factor of 1.45. This difference will affect the calculation of terminal momentum in Eq. (A.16), however the power index on  $\Lambda_{6,-22}$  term is small so that the impact on the value of  $p_{\text{sf,m}}$  is negligible.

<sup>4</sup><http://www.AGORAsimulations.org>

et al. (2021). We randomly sampled  $4 \times 10^4$  dark matter particles and added gas particles with the same mass as that of originally existing gas particles at the same position as those sampled dark matter particles. We adopt a fixed gravitational softening length of  $\epsilon_{\text{grav}} = 80$  pc. We allowed the minimum gas smoothing length to reach 10 percent of the spline size of gravitational softening  $2.8 \epsilon_{\text{grav}}$ .<sup>5</sup> We first evolve the system to 0.5 Gyr adiabatically for relaxation to set up the initial condition, and then evolve it to 1 Gyr with the sub-grid physics including cooling, UV background heating, star formation, and stellar feedback.

## 2.5.2 Star formation and Stellar feedback

### 2.5.2.1 Star formation

We assume star formation to occur when the gas number density  $n > 10 \text{ cm}^{-3}$  and temperature  $T < 10^4$  K. We use the same star formation prescription as Shimizu et al. (2019), a Schmidt-type star formation law (Schmidt, 1959). The star formation rate (SFR) density is (Cen and Ostriker, 1992, Katz, 1992, Nagamine et al., 2001, Springel and Hernquist, 2003, Stinson et al., 2006, Kim et al., 2014, 2016)

$$\dot{\rho}_* = \epsilon_* \frac{\rho_{\text{gas}}}{t_{\text{ff}}}, \quad (2.32)$$

where  $\epsilon_*$  is the star formation efficiency,  $\rho_{\text{gas}}$  is the gas density, and  $t_{\text{ff}} = \sqrt{3\pi/(32G\rho_{\text{gas}})}$  is the local free-fall time. We adopt  $\epsilon_* = 0.05$ . The star particles are stochastically spawned from gas particles to follow the SFR density. Each gas particle can spawn a maximum of  $n_{\text{spawn}}$  star particles. The initial mass of the star particle is defined as  $m_* = m_{\text{gas}}/n_{\text{spawn}}$ , where  $m_{\text{gas}}$  is the mass of the gas particle. We have adopted  $n_{\text{spawn}} = 2$  throughout this paper, using a SSP approximation and assuming each star particle to consist of a cluster of stars whose mass function follows the Chabrier IMF (Chabrier, 2003) with a mass range of 0.1-100  $M_{\odot}$ .

<sup>5</sup>We use the definitions of the smoothing length and the gravitational softening length in GADGET-2 code (Springel, 2005) in this paper; the gravitational softening length is equivalent to the Plummer softening length, while the smoothing length is the kernel size beyond which kernel value vanishes (see also Appendix C in Kim et al., 2016). We define the SPH spatial resolution as the smoothing length widely used in literature,  $\Delta x = \eta(m/\rho)^{1/3}$  (see e.g., Rosswog, 2009, for review). The parameter  $\eta$  is usually set to  $\eta \sim 1.3$ , but we set it to  $\eta = 1$  for simplicity. In our GADGET3-OSAKA simulation, we adopt the quintic spline kernel and  $N_{\text{ngb}} = 128$ . If we consider the quintic spline kernel to truncate at  $3h$  as in Price (2012) (see also Dehnen and Aly, 2012, for another definition of the smoothing length in terms of the smoothing kernel), we set to  $\eta = 1.04$  in our simulation, effectively.

### 2.5.2.2 Stellar feedback

We consider stellar wind from massive stars, Type II SNe, Type Ia SNe, and stellar wind from the asymptotic giant branch (AGB) stars as stellar feedback while distributing the physical quantities from them using the spherical superbubble model (Appendix B). We use CELIB to calculate time and metallicity-dependent mass, metal, and energy input from Type II SNe, Type Ia SNe, and AGB stars (see Shimizu et al., 2019, figure 1). To deposit energy and metals gradually rather than at a single instant, we divide each feedback from the star particle into  $n_{\text{fb}}$  events and adopt  $n_{\text{fb}} = 8$  throughout this paper (Shimizu et al., 2019).

**Type II SN feedback** We assume the range of the progenitor mass to be  $13 - 40 M_{\odot}$  and the hypernova (HN) fraction to be  $f_{\text{HN}} = 0.05$ . In the case of solar metallicity, the specific energy of Type II SNe is  $\epsilon_{\text{SNII}} = 7.19 \times 10^{48} \text{ erg } M_{\odot}^{-1}$ . We assume the SN energy to be  $10^{51} \text{ erg}$  and estimate shock radius and momentum input from SN feedback using equations (2.18) and (2.15). When SN feedback occurs at a low-density void formed by previous feedback events, we may overestimate the shock radius. Thus, we set an upper limit on the mass enclosed inside the shock radius  $M(R_{\text{max}}) = 2 \times 10^3 m_*/n_{\text{fb}}$ . This limit comes from a rough estimate of the SN remnant mass at fade away under an assumption that the terminal momentum per SN is  $p \sim 2 \times 10^5 M_{\odot} \text{ km s}^{-1}$ , the sound speed of star-forming cloud is  $c_s \sim 1 \text{ km s}^{-1}$ , and the SN rate is  $N_{\text{SN}} \sim m_*/(100 M_{\odot})$ .

**Type Ia SN feedback** We adopted the delay-time distribution function with a power law of  $t^{-1}$  for Type Ia SNe event rate (e.g., Totani et al., 2008, Maoz and Mannucci, 2012), using equations (2.18) and (2.15) to estimate shock radius and momentum input, although Type Ia SN explosions are intermittent. One can estimate the momentum input from a single Type Ia SN using equation (A.9), assuming the SN remnant formed by a single SN to acquire about 77 % of its terminal momentum by the shell-formation time (Kim and Ostriker, 2015). For Type Ia SN feedback, we ignore thermal feedback because the formation of a hot bubble by stochastic thermal feedback represents superbubble formation by clustered Type II SNe. We used the same upper limit as Type II SN feedback on the shock radius.

**Stellar wind from OB stars** For stellar wind feedback from OB stars, we consider only mechanical feedback. We calculated the energy of the stellar wind from OB star using STARBURST99<sup>6</sup> (Leitherer et al., 1999, Vázquez and Leitherer, 2005, Leitherer et al.,

<sup>6</sup><https://www.stsci.edu/science/starburst99/docs/default.htm>

2010, 2014) and set the specific energy of stellar wind to  $\epsilon_{\text{SW}} = 1.5 \times 10^{48} \text{ erg } M_{\odot}^{-1}$ . Assuming 30 % of the energy turns into kinetic energy, we estimate the shock radius and momentum input using the equation (2.18) and (2.15) by setting  $N_{\text{SN}} = m_* \epsilon_{\text{SW}} / (10^{51} \text{ erg})$ . Here we choose to use the equation of superbubble momentum because the specific luminosity of stellar wind and Type II SNe are similar (e.g., Agertz et al., 2013). We set an upper limit on the mass enclosed inside the shock radius  $M(R_{\text{max}}) = 2 \times 10^2 m_* / n_{\text{fb}}$ . This limit is one order smaller than that of SN feedback because the amount of energy injected by stellar winds is about one order smaller than that injected by SNe. The adopted numbers above translates to a specific momentum injection rate of  $\dot{p}/M \sim 100 \text{ km s}^{-1} \text{ Myr}^{-1}$ . However, Lancaster et al. (2021b) have shown that the wind specific momentum injection rate from O star winds in a cluster is  $\dot{p}/M \sim 10 \text{ km s}^{-1} \text{ Myr}^{-1}$  due to fractal mixing boundary layer. Our model here can be regarded as an upper limit of O star winds.

We do not use our stochastic thermal feedback model for OB stars because ionization heating is limited to  $2 \times 10^4 \text{ K}$  by hydrogen recombination, and heating to higher temperature is unphysical. Just heating to  $2 \times 10^4 \text{ K}$  is ineffective due to overcooling. In reality, radiation pressure and ionization heating form low-density H II bubbles, but we don't have a reasonable subgrid model for the bubble formation process.

**AGB feedback** For stellar wind from AGB stars, we only consider mass and metal input. We cannot resolve the circumstellar envelope of an AGB star at  $R \lesssim 1 \text{ pc}$  (e.g., Höfner and Olofsson, 2018). In our simulations, a star particle represents a star cluster; however, in reality, stars are dispersed. To account for this, we consider the star particle to be representative of stars in the surrounding gas with a mass of  $100 m_*$ , assuming the star formation efficiency to be  $\epsilon_* \sim 0.01$ . Thus, we set the mass enclosed inside the shock radius of the AGB feedback to  $M(R_{\text{shock}}) = 100 m_*$  and distribute the mass and metals to gas particles inside the shock radius. We do not consider the mechanical feedback from stellar winds because it is slower ( $\sim 10 \text{ km s}^{-1}$ ) than (and negligible in comparison to) SN feedback. However, we add a boost-back momentum for momentum conservation. If the relative velocity between the star and gas particles is large, the boost-back momentum can have a significant impact (Hopkins et al., 2018, Su et al., 2019).

### 2.5.3 Results from GADGET3-OSAKA simulations

To explore the thermal and mechanical feedback effects, we ran five simulations with different feedback settings, as summarized in Table 2.1. We retained the amount of mass and metals ejected by SNe and AGB stars and changed only the energy and momentum injection models. When feedback is turned off, its energy is reduced. All simulations have AGB feedback.

TABLE 2.1: List of isolated galaxy simulations used in this chapter.

Run Name	Feedback Type				Note
	Type II SN mechanical FB	Type II SN thermal FB	Stochastic thermal FB	Type Ia & OB star mechanical FB	
Fiducial	✓	✓	✓	✓	Fiducial run with all feedback models
Non-stochastic	✓	✓		✓	Fiducial but thermal energy is distributed without stochastic treatment
SNII-kinetic	✓				Type II SN mechanical feedback only
SNII-thermal		✓	✓		Type II SN thermal feedback only
No-FB					No feedback

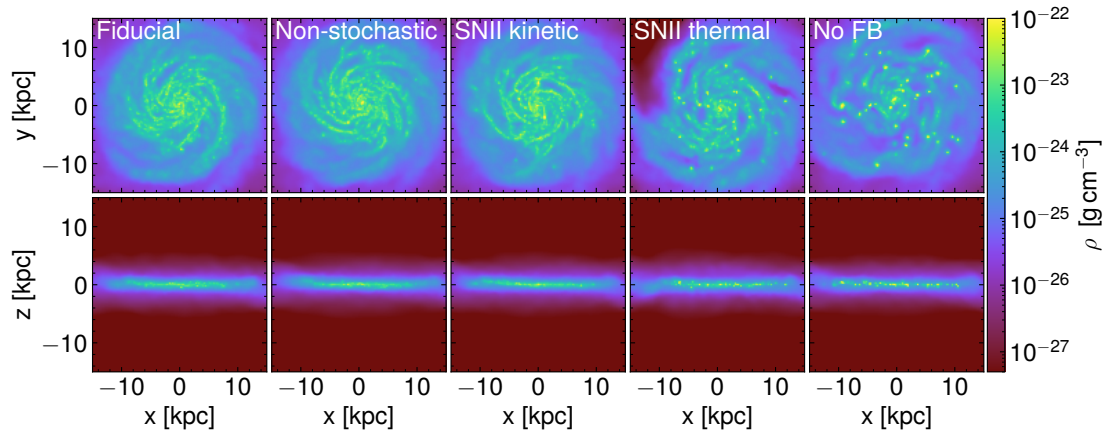


FIGURE 2.2: Projected gas density plots of the isolated galaxies in given Table 2.1 at  $t \simeq 1$  Gyr in  $30 \text{ kpc} \times 30 \text{ kpc}$  images. The top and bottom rows depict face-on and edge-on images, respectively. Here, we plot  $\sum \rho^2 / \sum \rho$  to enhance the contrast and to use the same density-weighted method for both temperature and metallicity.

### 2.5.3.1 Projection Maps

Figures 2.2, 2.3, and 2.4 show the density-weighted projection plots of density, temperature, and metallicity of the simulated galaxies at  $t \simeq 1$  Gyr. Galaxies are centered at the density-weighted center of gas mass,

$$\mathbf{r}_{\text{center}} = \frac{\sum_i \rho_i m_i \mathbf{r}_i}{\sum_i \rho_i m_i}. \quad (2.33)$$

In Figure 2.2, one can see that the density structure in the presence of mechanical feedback differs from that in its absence. The gas disk is maintained for 1 Gyr in three runs with Type II SN mechanical feedback (Fiducial, Non-stochastic, and SNII-kinetic), while the gas disks become clumpy in the other two runs. This result suggests that the galactic disk is supported against gravity by the turbulence driven by mechanical feedback. Comparing the Fiducial and Non-stochastic runs, the effect of stochastic thermal feedback is not clearly seen in the density distribution.

Figure 2.3 shows the density-weighted temperature. One can see the hot bubbles formed by the stochastic thermal feedback inside the gas disks in the Fiducial and SNII-thermal runs, which escape from the galactic disk to produce the hot outflow. This feature is observed in X-ray by Nakashima et al. (2018), who suggested that the hot, gaseous halo of the Milky Way is formed by the hot outflow resulting from stellar feedback. The low-density regions created by mechanical feedback or gas depletion are shown as  $\sim 10^6$  K because we set the initial temperature of the halo to  $10^6$  K.

The density-weighted metallicity is depicted in Figure 2.4. It should be noted that we did not change the metal injection model, and that these five runs are different at the

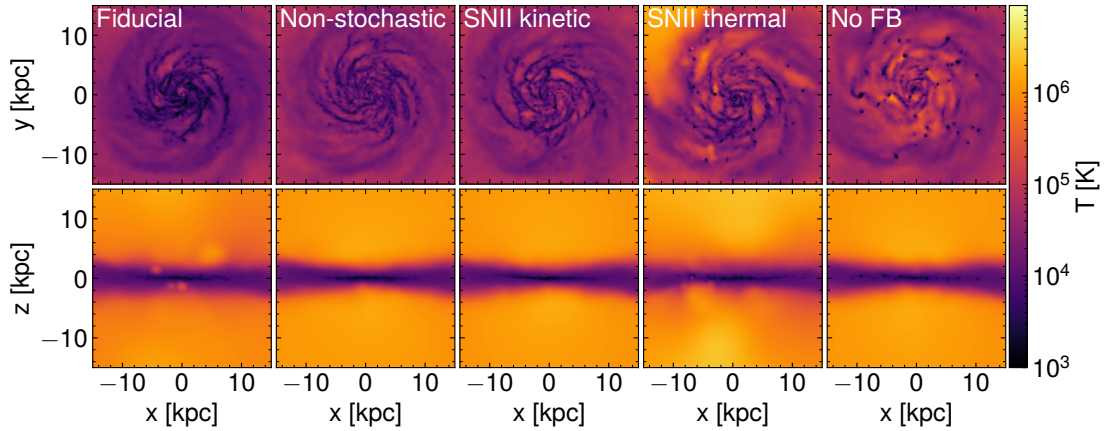


FIGURE 2.3: Projected temperature (density-weighted) of the isolated galaxies given in Table 2.1 at  $t \simeq 1$  Gyr. The top and bottom rows depict face-on and edge-on images. The hot gas above the disk in the No-FB run is due to the galactic halo gas with  $T = 10^6$  K implemented in the initial condition.

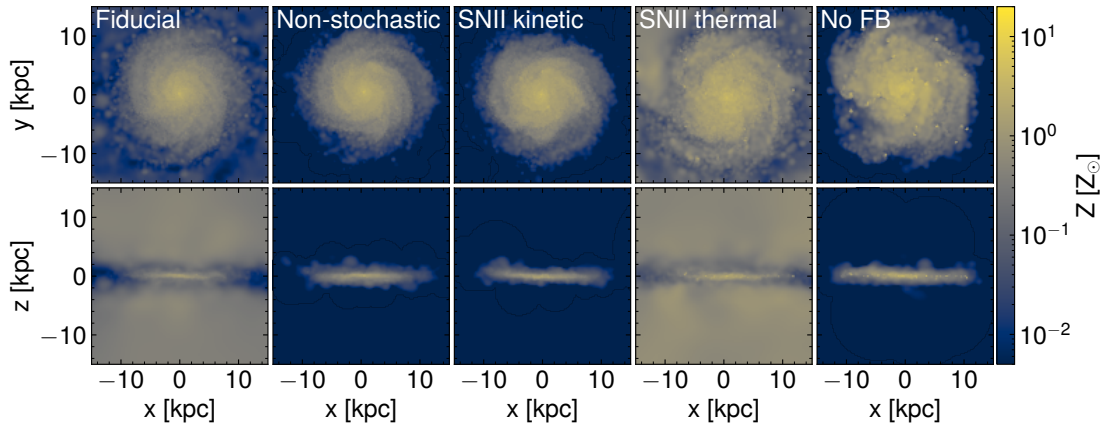


FIGURE 2.4: Projected metallicity (density-weighted) of the isolated galaxies given in Table 2.1 at  $t \simeq 1$  Gyr. The top and bottom rows depict face-on and edge-on images. Metals carried by the outflows are visible above and below the disk.

models of energy and momentum injection. The metal distribution above the galactic disks in the presence of stochastic thermal feedback differs from that in its absence. We also indicate the distribution of metals on the virial radius (205 kpc) scale in Figure 2.5. Metal outflows were not observed in the Non-stochastic run. This result is consistent with those of [Shin et al. \(2021\)](#), who demonstrated that metal outflow is suppressed by ram pressure from the hot gaseous halo using GADGET2 code with a simple thermal dump SN feedback model. On the other hand, the Fiducial run shows the metal outflows beyond the virial radius. We will further compare our work with that of [Shin et al. \(2021\)](#) in Section 2.5.3.5.



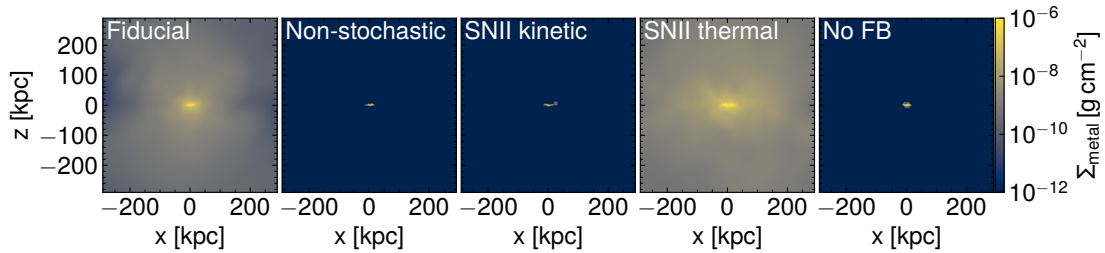


FIGURE 2.5: Large-scale, edge-on view of metal column density at  $t \simeq 1$  Gyr. It is clear that the metals are carried over large distances in the Fiducial and SNII-thermal runs.

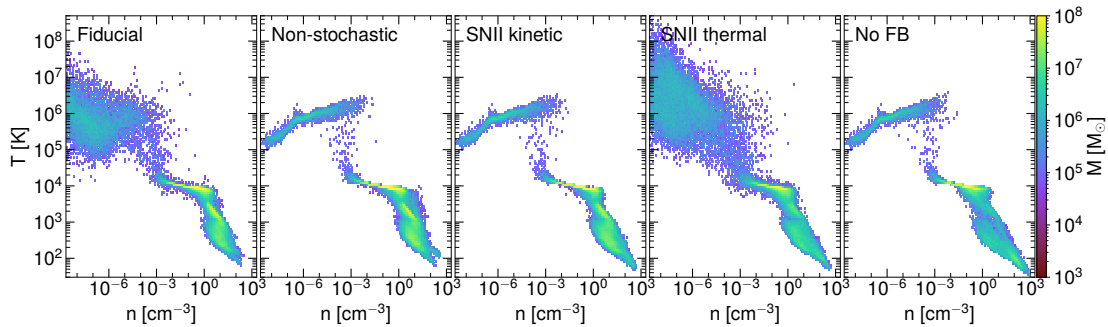


FIGURE 2.6: Phase diagram of the gas in the isolated galaxies given in Table 2.1 at  $t \simeq 1$  Gyr. The dense, cold gas ( $T < 10^3$  K) in the galactic disk is visible on the lower right corner. The hot, tenuous gas heated by feedback adiabatically cools and then joins the hot gaseous halo in the upper left region with  $T \sim 10^6$  K. The hot component is most visible in the SNII-thermal run due to the highest star formation rate and subsequent strong thermal feedback. The hot gas seen in the No-FB run is due to the hot halo implemented in the initial condition.

### 2.5.3.2 Phase Diagrams

Figure 2.6 shows the phase diagrams of simulated galaxies at  $t \simeq 1$  Gyr. The dense, cold gas ( $T < 10^3$  K) in the galactic disk is visible in the lower right corner. In three runs with mechanical SN feedback (Fiducial, Non-stochastic, and SNII-kinetic), two-phase ISM of the warm ( $T \sim 2 \times 10^3$  K) and cold ( $T \sim 3 \times 10^2$  K) phases were observed. Compared with them, the warm phase is less visible and the cold gas is more condensed at a lower temperature ( $T < 10^2$  K) in SNII-thermal and No-FB runs. The hot, tenuous gas heated by thermal feedback adiabatically cools and joins the hot gaseous halo in the upper left region with  $T \sim 10^6$  K. We do not see a difference in the upper left gas distributions of the Non-stochastic and No-FB runs, which indicates ineffective thermal feedback in the Non-stochastic run. The hot component is most visible in the SNII-thermal run due to its higher star formation rate and subsequent thermal feedback.



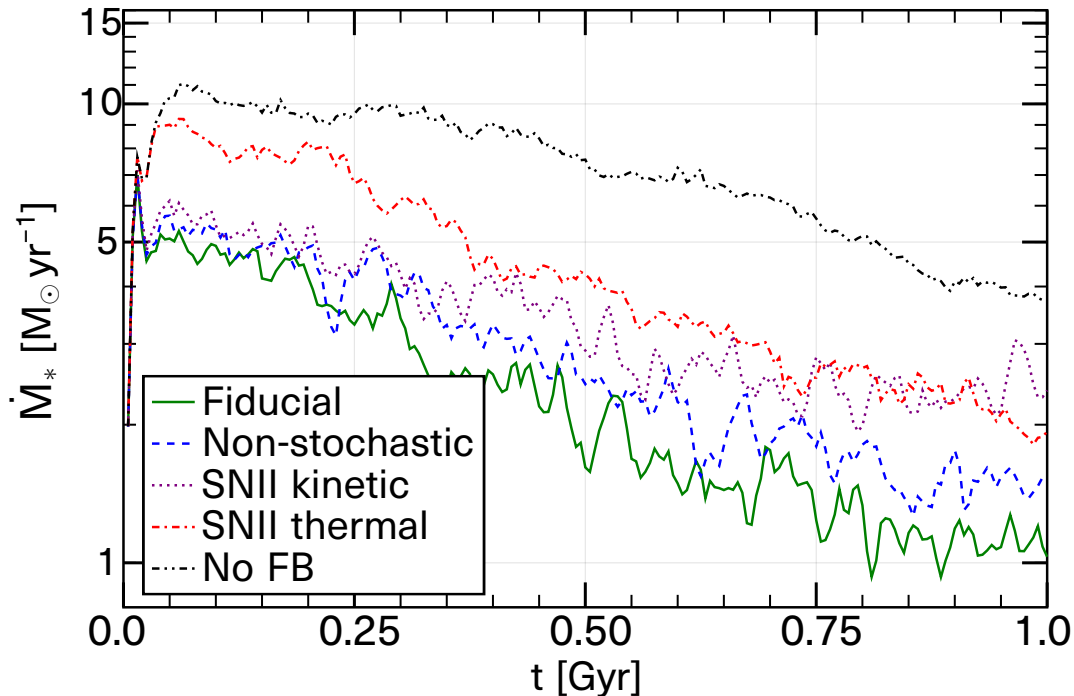


FIGURE 2.7: SFR as a function of time for the isolated galaxy simulations given in Table 2.1. The No-FB run has the highest SFR, and the SNII-thermal run shows weak suppression of SFR. In other runs, SFR is suppressed by the mechanical SN feedback efficiently.

### 2.5.3.3 Star Formation Histories

Figure 2.7 depicts the star formation history of the simulated galaxy. Star formation is suppressed in all the runs with feedback compared to the No-FB run. The thermal feedback suppresses star formation, and the mechanical feedback suppresses it further. Star formation rate in the Fiducial and Non-stochastic runs are slightly lower than that in the SNII-kinetic run because the mechanical feedback from Type Ia SNe and OB stars are not considered in the SNII-kinetic run. In our previous work Shimizu et al. (2019), we observed an ‘initial star burst’ which occurs just after the beginning of the simulations due to the collapse of gas without feedback. This phenomenon is weakened in this work because we first adiabatically evolve the initial condition to 0.5 Gyr for relaxation and then plot the star formation history with an interval of 5 Myr, which is approximately equal to the lifespan of a massive star.

### 2.5.3.4 Kennicutt–Schmidt Relation

Figure 2.8 shows the Kennicutt–Schmidt relations of the simulated galaxies given in Table 2.1 at  $t = 1$  Gyr calculated with  $500 \text{ pc} \times 500 \text{ pc}$  patches up to the galactic radius of  $R = 10 \text{ kpc}$ . The results from our simulations agree with the observed range by Bigiel

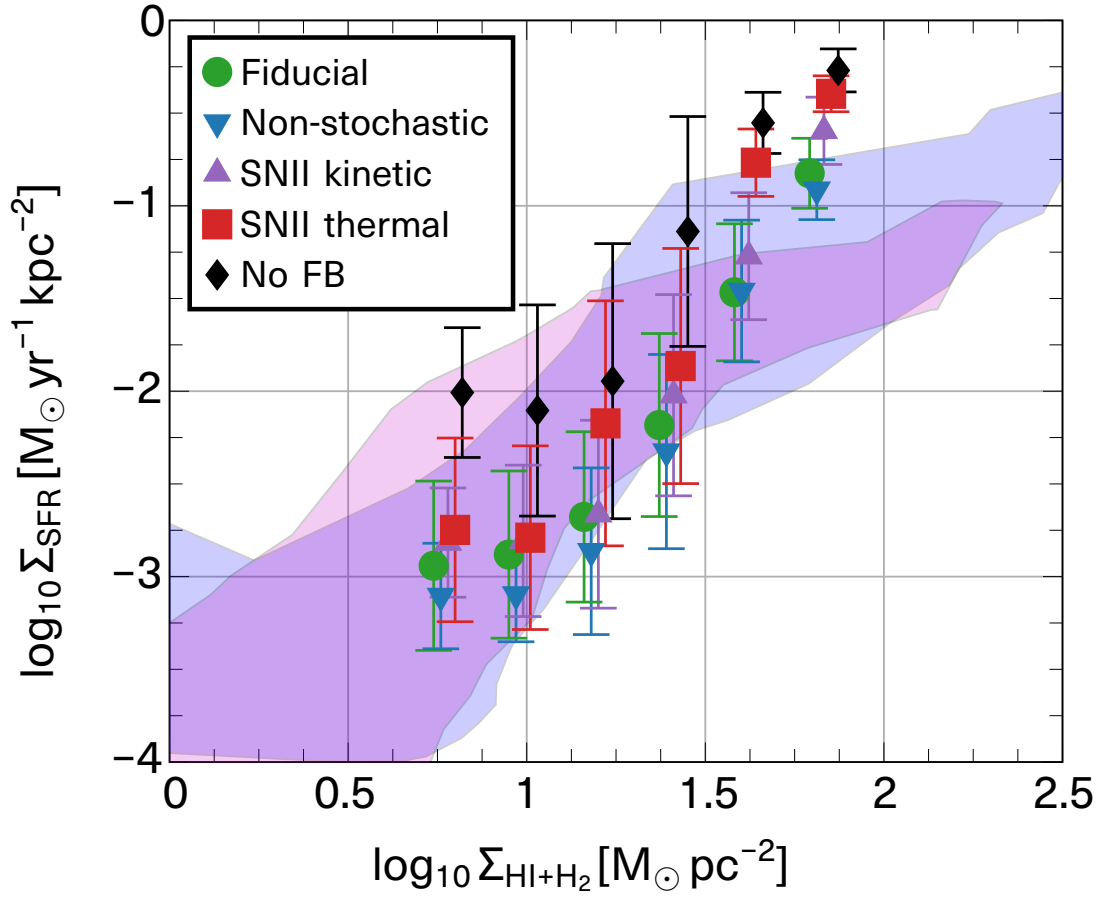


FIGURE 2.8: The Kennicutt–Schmidt relation of the simulated galaxies given in Table 2.1 at  $t \simeq 1$  Gyr, calculated with  $500 \text{ pc} \times 500 \text{ pc}$  patches. Colored regions depict the observational data of nearby spiral galaxies (blue: [Schruba et al. 2011](#); magenta: [Bigiel et al. 2008](#)).

[et al. \(2008\)](#), [Schruba et al. \(2011\)](#) with a similar slope and normalization, which is encouraging. The three runs with mechanical feedback (Fiducial, Non-stochastic, and SNII-kinetic) show similar results, and their star formation rate density is lower by a factor of 2–3 than that of No-FB run. The SNII-thermal run is inbetween No-FB and other runs consistently with Fig. 2.7. The simulated data fluctuates as a function of time but on average stays within the observed range. The Fiducial and Non-stochastic runs have the lowest  $\Sigma_{\text{SFR}}$  among all runs due to low SFR, as shown in Fig. 2.7.

The simulation data point corresponding to the highest gas column density is above the observed data; at this point, it is unclear if our results will turn over at higher column densities due to limitations in our resolution. The cut-off at the lower end of the simulation data is determined by mass resolution and by how well we can track star formation in a low-density region, which will be explored in future works.

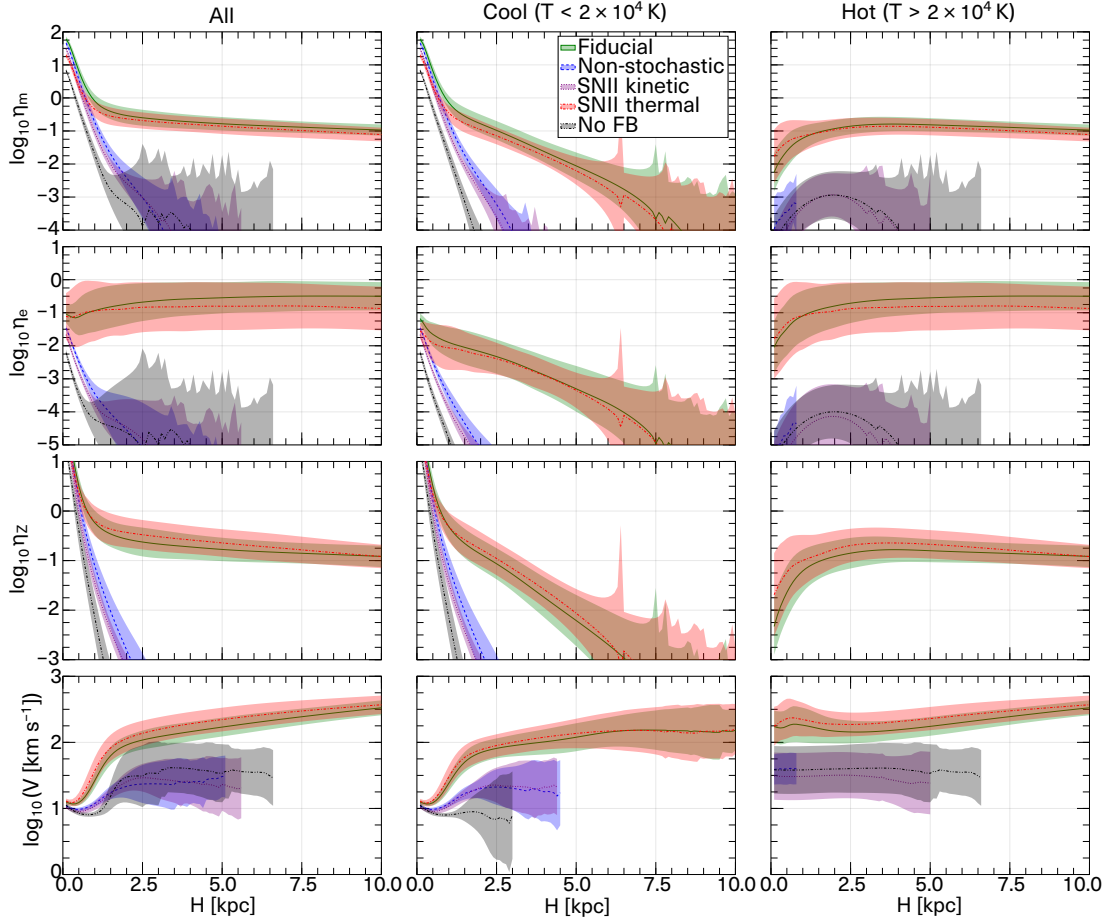


FIGURE 2.9: Mass (top row), energy (second row), and metal (third row) loading factors vs. the height above the galactic plane. The fourth row depicts outflow velocity vs. the height above the galactic plane. All quantities are measured using cylinders of different heights and a 10 kpc radius and averaged over  $t = 0.5 - 1.0$  Gyr. The lines indicate the average values during this time period, with  $\pm 1\sigma$  shade for time variation.

### 2.5.3.5 Outflow Profiles of Mass, Energy, Velocity, and Metals

The outflow rate of physical value  $X$  at a height  $H$  above the galactic plane is

$$\dot{X}_{\text{out}}(H) = \int \rho_X v_z dS_H = \int_{S_H} \sum_i X_i v_{i,z} W(r_{ij}, h_{\text{sml},i}) d\mathbf{r}_j, \quad (2.34)$$

where  $S_H$ ,  $\rho_X$ , and  $v_z$  denote the plane at height  $H$ , the density of  $X$ , and velocity in the  $z$ -direction, while  $W$  indicates the kernel function used in the simulation. Other symbols, such as  $r_{ij}$ ,  $v_{i,z}$ , and  $h_{\text{sml},i}$  denote the distance from the  $i$ -th gas particle to  $\mathbf{r}_j$ , the  $z$ -direction outflow velocity, and the smoothing length of the  $i$ -th gas particle, respectively. We rewrite this equation as follows, to compute the outflow rate from

simulation snapshots (Shimizu et al., 2020):

$$\dot{X}_{\text{out}}(H) = \sum_i X_i v_{i,z} \int_0^{\sqrt{h_{\text{sml},i}^2 - \zeta_i^2}} 2\pi\xi W\left(\sqrt{\zeta_i^2 + \xi^2}, h_{\text{sml},i}\right) d\xi, \quad (2.35)$$

where  $\zeta_i = |z_i - H|$  and  $z_i$  is the  $z$  coordinate of  $i$ -th particle.<sup>7</sup> To evaluate the intrinsic outflow, we take the summation over those outflowing gas particles that have non-zero metallicity. Since the metallicity is initially zero and metal mixing between gas particles is not considered, such particles are considered as metal-enriched outflows.

We depict the outflow profiles of mass, energy, and metal loading factor

$$\eta_m = \frac{\dot{M}_{\text{out}}}{\dot{M}_*}, \quad (2.38)$$

$$\eta_e = \frac{\dot{E}_{\text{out}}}{\epsilon_{\text{SNII}} \dot{M}_*}, \quad (2.39)$$

$$\eta_Z = \frac{\dot{M}_{Z,\text{out}}}{\mu_{Z,\text{SN}} \dot{M}_*}, \quad (2.40)$$

averaged over  $t = 0.5 - 1.0$  Gyr, in Fig. 2.9. Here,  $\dot{M}_{\text{out}}$ ,  $\dot{E}_{\text{out}}$ , and  $\dot{M}_{Z,\text{out}}$  are the outflow rates of mass, energy, and metals, while  $\dot{M}_*$  is the star formation rate and  $\mu_{Z,\text{SN}} = 0.01$  is the specific metal mass released by Type II SNe. We also compute density-weighted, average outflow velocity,

$$V_{\text{out}}(H) = \frac{\int \rho v_z dS_H}{\int \rho dS_H} = \frac{\sum_i m_i v_{i,z} \int_0^{\sqrt{h_{\text{sml},i}^2 - \zeta_i^2}} 2\pi\xi W\left(\sqrt{\zeta_i^2 + \xi^2}, h_{\text{sml},i}\right) d\xi}{\sum_i m_i \int_0^{\sqrt{h_{\text{sml},i}^2 - \zeta_i^2}} 2\pi\xi W\left(\sqrt{\zeta_i^2 + \xi^2}, h_{\text{sml},i}\right) d\xi}, \quad (2.41)$$

where  $m_i$  is the mass of the  $i$ -th gas particle. The profiles of the total mass and the metal loading factor are high at low altitudes, decrease rapidly to  $H \sim 1.0$  kpc, and become flatter at  $H \gtrsim 1.0$  kpc.

At  $H \lesssim 1.0$  kpc, the cool ( $T < 2 \times 10^4$  K) component dominates mass outflow (higher  $\eta_m$  in the top middle panel of Fig. 2.9), which is slow ( $V \lesssim 30 \text{ km s}^{-1}$ ) and falls back to the galaxy. We see that the mass loading factor of cool outflow in the runs with feedback is greater by  $\sim 0.8$  dex over that of No-FB run.

<sup>7</sup>We used the quintic B-spline kernel function in our simulations. In this case, the integral accounting for the cross-section of the SPH particle and the plane of height  $H$  can be analytically calculated as

$$\int_0^{\sqrt{h^2 - \zeta^2}} 2\pi\xi W\left(\sqrt{\zeta^2 + \xi^2}, h\right) d\xi = f_{\frac{1}{3},1}(\zeta, h) + f_{-2,\frac{2}{3}}(\zeta, h) + f_{5,\frac{1}{3}}(\zeta, h), \quad (2.36)$$

where

$$f_{a,b}(\zeta, h) = \frac{3^9 a}{359 h^2} \left(b - \frac{\zeta}{h}\right)_+^6 \left(\zeta + \frac{h}{7} \left(b - \frac{\zeta}{h}\right)_+\right). \quad (2.37)$$

Here,  $(\cdot)_+ \equiv \max(0, \cdot)$ .

At  $H \gtrsim 2.5$  kpc, the hot ( $T > 2 \times 10^4$  K) component dominates outflow. We see that the mass loading factor of hot outflow in runs with stochastic thermal feedback (Fiducial and SNII-thermal) is much higher than that of others, which indicates that stochastic thermal feedback launches hot outflow. Non-stochastic and SNII-kinetic runs shows much weaker hot outflow, demonstrating that simply distributing thermal energy from SN feedback is ineffective in launching hot outflow. The outflow profile of Fiducial run is qualitatively consistent with high-resolution small-box simulations solving a patch of galactic disk (Kim et al., 2020b).

Figure 2.10 shows the outflow profiles up to 200 kpc. We calculate the outflow rates at the surface of a sphere with a radius  $R$  centered at the galactic center, and show the loading factors and outflow velocity of all components. The hot component dominates at  $R > 10$  kpc with cool component disappearing at large  $R$ . We see the outflow is accelerated towards large  $R$  and reaches  $\gtrsim 560$  km s<sup>-1</sup> at  $R = 200$  kpc. The mass loading factor of Fiducial run at  $R = 200$  kpc is  $\eta_m \sim 0.3$ . In all the panels the SNII-thermal model shows somewhat higher loading factors and outflow velocity than the Fiducial run, which is due to higher SFR in the former model as was shown in Fig. 2.7.

For the presented isolated galaxy test, we followed Shin et al. (2021) in adding a gaseous halo to the initial condition. As shown in Fig. 2.9, metals are transported via the hot outflow driven by thermal feedback, while the cool outflow cannot transport metals beyond  $H = 5$  kpc. This is because the hot outflow driven by thermal feedback is not impeded by the ram pressure of the gaseous halo  $P_{\text{ram}} = \rho v^2$  due to its higher thermal pressure. On the other hand, the cool outflow is decelerated by the ram pressure of the gaseous halo because it is not accelerated after its initial launch by momentum feedback.

Our stochastic thermal feedback model heats the gas particles up to a higher temperature than simple thermal dump models do, driving hot outflow without increasing the total SN feedback energy by hand. The discrepancy in metal outflow between mesh-based (ENZO) and particle-based (GADGET-2 and GIZMO) simulations reported by Shin et al. (2021) could be due to the difference in mass resolution; particle-based simulations fix the mass resolution, but mesh-based simulations do not fix it and can effectively heat gas cells at low-density voids created by previous SN feedback events.

#### 2.5.4 Discussion on the SN feedback model

In our model, we assume that the superbubbles spread isotropically. However, when the ISM is highly non-uniform, the superbubbles spread selectively towards the low-density channel (Ohlin et al., 2019). In particular, when the superbubbles break out, the kinetic feedback to the local star formation may be weaker, as the energy flows out of the galaxy

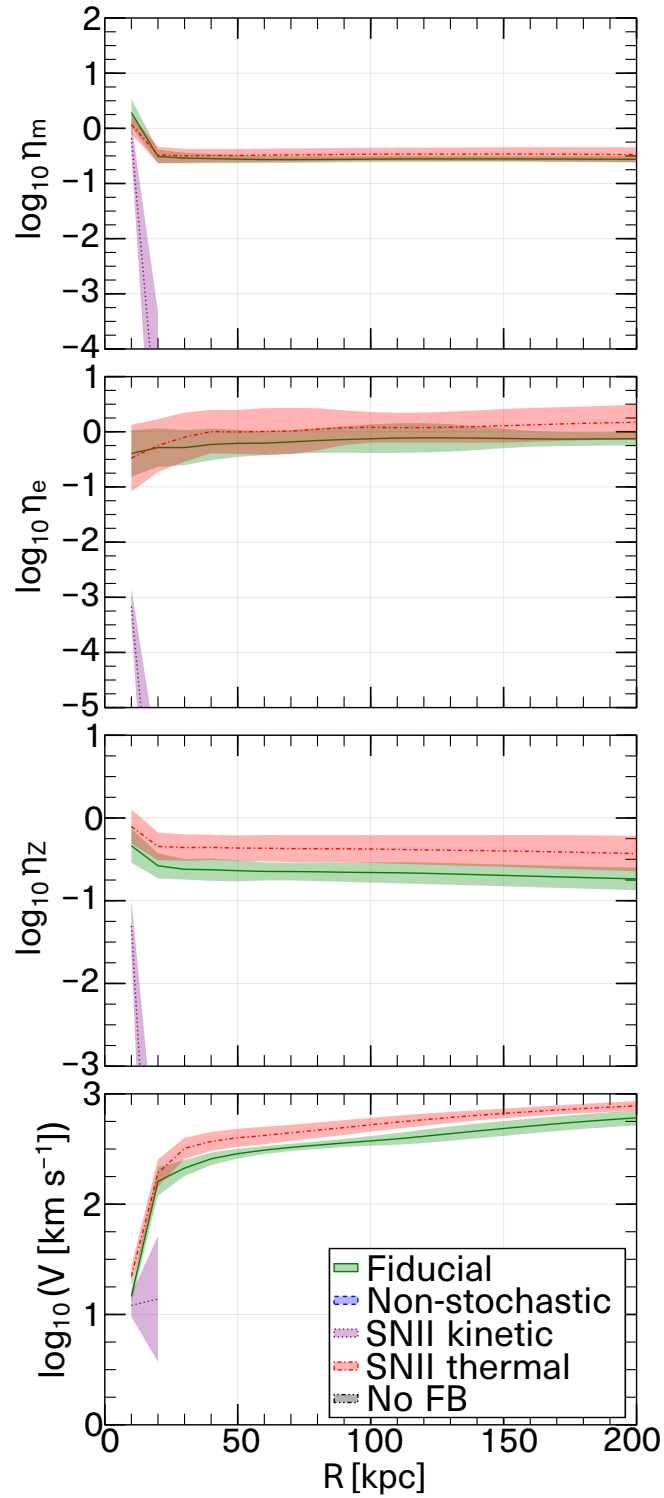


FIGURE 2.10: Same as Figure 2.9 but measured with spheres of different radii up to 200 kpc, centered at the galactic center and averaged between  $t = 0.5 - 1.0$  Gyr. The lines show the average during this time period with  $\pm 1\sigma$  shade for the time variation.

before the superbubbles gain momentum (Fielding et al., 2018). Although our feedback model considers the non-uniformity of the ISM via anisotropic particle distribution, the impact of non-uniform ISM needs to be examined in the future with a more realistic setup and a higher resolution. For example, an analytical model considering the effect of superbubble breakout could be incorporated to construct a more realistic feedback model (Orr et al., 2022b).

There are several different weighting schemes to distribute mechanical feedback in particle simulation such as Hopkins et al. (2018), Hu (2019), Marinacci et al. (2019). However, the detailed distribution of particles on sub-resolution scales is somewhat random, and the exact weighting scheme does not matter very much in the final outcome as long as it is isotropic.

The models of Kimm and Cen (2014) and Hopkins et al. (2018) estimated the momentum by scaling that of isolated supernova explosions. However, the superbubble momentum also depends on the time interval of supernova explosions as we show in this work. Here we develop a more realistic model by using a universal scaling relation for the superbubble terminal momentum and radius, and this is where our model is different from Kimm and Cen (2014) and Hopkins et al. (2018).

In addition to momentum feedback, thermal feedback was also considered by Kimm and Cen (2014) and Hopkins et al. (2018), where they simply injected thermal energy. However, thermal feedback will not work if the model is not constructed to avoid overcooling (Hu, 2019). Therefore, in our model, we adopt a stochastic thermal feedback model. In the isolated galaxy test, we show that the thermal outflow is driven by the stochastic model.

Dalla Vecchia and Schaye (2012) constructed a stochastic thermal feedback model with temperature rise,  $\Delta T$ , as a free parameter. However, the temperature is not constant during the evolution of high-temperature bubbles formed by supernova explosions. Therefore, a parameter survey is necessary to determine  $\Delta T$ , and using temperature as a model parameter is not so ideal as we discuss in Section 2.4. Instead, we use entropy as a parameter in our model. Since the high-temperature outflow gas expands adiabatically, the entropy is constant and its value can be determined based on high-resolution simulations.

In our model, we also provide momentum feedback in addition to thermal feedback. As shown in the isolated galaxy test, thermal feedback can only suppress star formation weakly. This is because the spatial resolution required to solve for the time evolution of SN remnant is more stringent than the mass resolution required to resolve for hot SN bubbles (Section 2.1).

Our thermal feedback model heats gas particles up to a fixed entropy, which means denser gas particles are heated to higher temperatures. In high- $z$  galaxies where the gas density is higher than in the local ones, our thermal feedback would become stronger. [Arata et al. \(2020\)](#) performed cosmological galaxy simulations using the stochastic thermal feedback model by [Dalla Vecchia and Schaye \(2012\)](#), with  $\Delta T = 10^{7.5}$  K and studied metal-emission lines from high- $z$  galaxies. They showed that the radial profile of [C II] surface brightness of simulated galaxies is lower at outer radius than observation. This discrepancy could be resolved by our stronger thermal feedback. In future works, we will investigate the impact of our SN feedback model in a cosmological context.

Our SN feedback model injects both terminal momentum and thermal energy from SNe, which may overestimate the feedback effect. In reality, some SN energy is used to drive a superbubble and the other is used to accelerate outflows after the break-out of the superbubble. [Orr et al. \(2022b\)](#) developed an analytic model for clustered SNe in a galactic disk, and their model predicts that the superbubble is more likely to break out in an environment with rich gas and short dynamical times, which is consistent with observations and simulations ([Orr et al., 2022a](#)). Their model could be incorporated into our SN feedback model in the future.



# Chapter 3

## Method

In this chapter, we describe the methodology of the cosmological hydrodynamic simulation.

### 3.1 Initial Condition

We generate an initial condition using MUSIC2-MONOFONIC<sup>1</sup> (Michaux et al., 2021, Hahn et al., 2021). The phase fixing technique (Angulo and Pontzen, 2016) is used to suppress the impact of cosmic variance, but we run only a single simulation for each model and do not include paired simulations for the analyses in this paper. We adopt the following cosmological parameters from Planck Collaboration et al. (2020),  $(\Omega_m, \Omega_b, \Omega_\Lambda, h, n_s, 10^9 A_s) = (0.3099, 0.0488911, 0.6901, 0.67742, 0.96822, 2.1064)$ .<sup>2</sup> The initial condition is generated at  $z_{\text{ini}} = 39$  using the third-order Lagrangian perturbation theory. The transfer function at  $z_{\text{ini}}$  is obtained by back-scaling the transfer function at reference redshift  $z_{\text{ref}} = 2$  computed by Boltzmann code CLASS<sup>3</sup> (Blas et al., 2011). The simulation box size is  $L_{\text{box}} = 50 h^{-1}$  cMpc, and the total number of particles is  $N_p = 2 \times 512^3$ ; the initial particle mass of dark matter and gas is  $m_{\text{DM}} = 6.74 \times 10^7 h^{-1} M_\odot$  and  $m_{\text{gas}} = 1.26 \times 10^7 h^{-1} M_\odot$ , respectively.<sup>4</sup>

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<sup>1</sup>The code's website is <https://bitbucket.org/ohahn/monofonic/src/master/>

<sup>2</sup>The best-fit parameters of the baseline model 2.20 base\_plikHM\_TTTEEE\_lowl\_lowE\_lensing\_post\_BAO\_Pantheon of Planck 2018 cosmological parameter table as of May 14, 2019 ([https://wiki.cosmos.esa.int/planck-legacy-archive/images/b/be/Baseline\\_params\\_table\\_2018\\_68pc.pdf](https://wiki.cosmos.esa.int/planck-legacy-archive/images/b/be/Baseline_params_table_2018_68pc.pdf)).

<sup>3</sup>The code's website is <http://class-code.net/>

<sup>4</sup>cMpc denotes Mega parsec in comoving coordinate.

## 3.2 Cosmological Hydrodynamic Simulation

We use the cosmological N-body/SPH code GADGET4-OSAKA (Romano et al., 2022a,b), which is a privately developed branch of GADGET-4<sup>5</sup> (Springel et al., 2021). The GADGET-4 is the successor of the GADGET-3 (last described in Springel, 2005, as GADGET-2), on which our GADGET3-OSAKA is based. GADGET-4 has improved performance and some useful modules for large-scale cosmological simulation over the earlier implementation.

The Newtonian gravity for dark matter and baryons is solved via

$$\Delta\Phi = 4\pi G\rho, \quad (3.1)$$

using the third-order TreePM method (Xu, 1995, Bagla, 2002, Springel, 2005). The same gravitational softening length is used for all particle types, and it is set to  $\epsilon_{\text{grav}} = 3.38 h^{-1} \text{ckpc}$  but limited to physical  $0.5 h^{-1} \text{kpc}$  at all times.

The SPH method (for reviews, see Rosswog, 2009, Springel, 2010a, Price, 2012) is used to solve the governing equations of hydrodynamics,

$$\frac{d\rho}{dt} = -\rho\nabla\cdot\mathbf{v} - \mathcal{S} + \mathcal{I}, \quad (3.2)$$

$$\frac{d\mathbf{v}}{dt} = \frac{\nabla P}{\rho} + \mathcal{K}, \quad (3.3)$$

$$\frac{du}{dt} = -\frac{P}{\rho}\nabla\cdot\mathbf{v} + \Gamma - \Lambda + \mathcal{T}, \quad (3.4)$$

where  $\rho$ ,  $P$ , and  $\mathbf{v}$  are density, pressure, and velocity, respectively, and  $\frac{d}{dt} = \frac{\partial}{\partial t} + \mathbf{v}\cdot\nabla$  is the material derivative. The integration is carried out on the expanding comoving coordinate. The  $\mathcal{S}$  and  $\mathcal{I}$  in the equation of continuity (3.2) denote gas mass converted to stars and mass injected from SNe and AGB stars. The  $\mathcal{K}$  in the equation of motion (3.3) denotes momentum injection by SN feedback, and  $\mathcal{T}$  in the energy equation (3.4) denotes thermal energy injection by SN and AGN feedback. The treatment of  $\mathcal{S}$ ,  $\mathcal{I}$ ,  $\mathcal{K}$ , and  $\mathcal{T}$  are described in the following subsections. The next subsection 3.3 describes the details and development of numerical treatment of hydrodynamics.

The heating rate,  $\Gamma$ , and the cooling rate,  $\Lambda$ , are computed using the GRACKLE<sup>6</sup> library (Smith et al., 2017), which solves the non-equilibrium primordial chemistry network of 12 chemical species, H, D, He, H<sub>2</sub>, HD, and their ions, with radiative cooling by metals and photo-heating and photo-ionization by uniform UV background. The metal cooling rate is precomputed using the photoionization code CLOUDY (Ferland et al., 2013), and the

<sup>5</sup>The code's website is <https://wwwmpa.mpa-garching.mpg.de/gadget4/>

<sup>6</sup>The code's website is <https://grackle.readthedocs.io/en/latest/>

UV background model by [Haardt and Madau \(2012\)](#) is assumed. In GRACKLE, we set the parameters related to the onset of UV background to `UVbackground_redshift_on=8` and `UVbackground_redshift_fullon=6`, and then the cosmic reionization occurs at  $z \sim 7$ . Our simulations do not include the heating by the cosmic ray and stellar radiation, and we ignore the self-shielding of the UV background by atomic hydrogen to avoid overcooling of neutral gas.

We follow 12 chemical elements, H, He, C, N, O, Ne, Mg, Si, S, Ca, Fe, and Ni, produced by core-collapse SNe, type-Ia SNe, and AGB stars. The metallicity floor is  $Z_{\text{floor}} = 10^{-6} Z_{\odot}$ , where  $Z_{\odot} = 0.0134$  is the solar metallicity ([Asplund et al., 2009](#)).

GADGET4-OSAKA solves the production and destruction of dust as described in [Romano et al. \(2022a\)](#) following the full dust grain size distribution; however, we do not focus on dust in this work and omit the description of the dust module here. The analysis of dust will be made in our future work.

We use the Smagorinsky-Lilly type turbulent metal and dust diffusion model ([Smagorinsky, 1963](#), [Shen et al., 2010](#), [Romano et al., 2022a](#)) with a diffusion parameter  $C_{\text{diff}} = 2 \times 10^{-4}$ .

The non-thermal Jeans pressure floor ([Hopkins et al., 2011](#), [Kim et al., 2016](#)) is applied to avoid artificial fragmentation as described in Section 3.3.1.4. The lower limit of the temperature is set to the higher value of the CMB temperature and  $T_{\text{min}} = 15$  K, and the upper limit is set to  $T_{\text{max}} = 10^9$  K.

The simulations presented in this chapter are performed at the SQUID supercomputer at Cybermedia Center, Osaka University, equipped with dual Intel Xeon Platinum 8368 processors (2.4 GHz) per compute node. Running the Fiducial model took  $1.12 \times 10^5$  CPU hours.

### 3.3 Numerical method

We here describe the numerical methodology of the cosmological hydrodynamics simulation by GADGET4-OSAKA.

#### 3.3.1 SPH

We determine the smoothing length by

$$\frac{4}{3}\pi h_i^3 n_i = N_{\text{ngb}}, \quad (3.5)$$

where

$$n_i = \sum_{j=1}^N W_{ij}(h_i) \quad (3.6)$$

is the SPH particle number density, and  $W_{ij}(h_i) \equiv W(|\mathbf{r}_i - \mathbf{r}_j|; h_i)$  is the kernel function. We use the Wendland C4 kernel function (Wendland, 1995, Dehnen and Aly, 2012) with neighbor number  $N_{\text{ngb}} = 120 \pm 2$ .

We use the pressure-energy formulation of SPH (Hopkins, 2013, Saitoh and Makino, 2013). The equation of motion of SPH particle is

$$\frac{dv_i}{dt} = - \sum_{j=1}^N m_j \left[ f_{ij} \frac{u_j \bar{P}_i}{u_i \bar{\rho}_i^2} \nabla_i W_{ij}(h_i) + f_{ji} \frac{u_i \bar{P}_j}{u_j \bar{\rho}_j^2} \nabla_i W_{ij}(h_j) \right]. \quad (3.7)$$

The energy equation is

$$\frac{du_i}{dt} = \sum_{j=1}^N m_j f_{ij} \frac{u_j \bar{P}_i}{u_i \bar{\rho}_i^2} (\mathbf{v}_i - \mathbf{v}_j) \nabla_i W_{ij}(h_i), \quad (3.8)$$

where

$$\bar{P}_i = \sum_{j=1}^N (\gamma - 1) m_j u_j W_{ij}(h_i) \quad (3.9)$$

is the smoothed pressure,  $\bar{\rho}_i = \bar{P}_i / [(\gamma - 1)u_i]$  is the internal-energy-weighted smoothed density, and

$$f_{ij} = \left[ \frac{h_i}{3(\gamma - 1)n_i m_j u_i} \frac{\partial \bar{P}_i}{\partial h_i} \right] \left( 1 + \frac{h_i}{3n_i} \frac{\partial n_i}{\partial h_i} \right)^{-1} \quad (3.10)$$

is the grad- $h$  term, which accounts for the variation of the smoothing length.<sup>7</sup>

We did not use the pressure-entropy formulation, another pressure-based SPH variant implemented in original GADGET-4. The pressure-entropy SPH cannot correctly increase or decrease energy without a costly iterative treatment when energy is added or reduced by subgrid physics (Borrow et al., 2021). This is because the smoothed density  $\bar{\rho}_i = (1/A_i^{1/\gamma}) \sum_j m_j A_j^{1/\gamma} W_{ij}(h_i)$  is coupled to the entropy  $A_i$ , and one cannot change the particle's energy  $u_i = A_i \bar{\rho}_i^\gamma$  as desired by simply updating entropy. In the pressure-energy formulation, each SPH particle explicitly has an internal energy variable, and modifying the energy is straightforward.

<sup>7</sup>Note that entropy and energy are simultaneously conserved in the pressure-energy SPH formulation derived from Lagrangian (Hopkins, 2013).

### 3.3.1.1 SIMD Vectorization

To execute large-scale simulations, it is necessary to improve the computational efficiency of the simulation code. We vectorized the density and hydro force evaluation kernel using the AVX-512 vector extension instruction set, which can perform arithmetic or logical instruction for eight 64-bit double variables in a single instruction (single instruction, multiple data; SIMD). The SPH calculation consists of a doubly-nested loop; 1) for all active particles, 2) we take kernel-weighted sums. [Springel et al. \(2021\)](#) reported that the original GADGET-4 code shows no significant improvement in the computational speed using the AVX2 instruction set. This would be likely because they vectorized the innermost SPH loop, where the memory bandwidth limits the calculation speed. Instead, we vectorize the outer loop by simultaneously processing a group of SPH particles ([Barnes, 1990](#)).

At the beginning of every SPH evaluation loop, we form groups consisting of, at most, eight particles using the indices of SPH particles. The indices are assigned using the Peano-Hilbert curve when the domain decomposition is carried out, and the particles that are close on the index list are also close in positions ([Springel et al., 2005](#)). To form groups, we check particles in the order of indices and add a particle to a group if their regions to search for neighbors overlap each other. We find twice the speed up of calculation in a realistic cosmological zoom-in simulation.

### 3.3.1.2 Artificial Conduction

We include artificial conduction, a diffusive term of internal energy, for a better capturing of pressure discontinuity, i.e., shocks. We implemented the artificial conduction of the following form ([Price, 2008](#)), which conserves the internal energy within the kernel:

$$\frac{du_i}{dt} = \sum_j m_j \alpha_{\text{cond},ij} v_{\text{sig},ij} \frac{u_i - u_j}{\rho_{ij}} \nabla_i \bar{W}_{ij}, \quad (3.11)$$

where  $m$  and  $u$  denote mass and internal energy,  $\rho_{ij} = (\rho_i + \rho_j)/2$  denotes the mean density of particle  $i$  and  $j$ , and  $\bar{W}_{ij} = [W_{ij}(h_i) + W_{ij}(h_j)]/2$  denotes the symmetrized kernel between  $i$  and  $j$ .

We use the conduction limiter proposed by [Borrow et al. \(2022\)](#) for the conduction coefficient  $\alpha_{\text{cond},ij}$ , which is computed as

$$\alpha_{\text{cond},ij} = \frac{\alpha_{\text{cond},i} P_i + \alpha_{\text{cond},j} P_j}{P_i + P_j} \quad (3.12)$$

with

$$\alpha_{\text{cond},i} = \alpha_{\text{cond}} \left( 1 - \frac{\alpha_{\text{max},i}}{\alpha_{\text{visc}}} \right) \quad (3.13)$$

and

$$\alpha_{\text{max},i} = \max_{r_{ij} < h_i} \alpha_{\text{tdav},j} \quad (3.14)$$

where  $\alpha_{\text{cond}}$  and  $\alpha_{\text{visc}}$  are constant coefficients of artificial conduction and viscosity,  $\alpha_{\text{tdav}}$  is the time-dependent coefficient of artificial viscosity, and  $P$  is thermal pressure. In this work, we use constant viscosity with field reconstruction as discussed below, but we also compute the time-dependent coefficient  $\alpha_{\text{tdav}}$  to limit the artificial conduction at shocks. We use the default time-dependent coefficient in GADGET-4, which was originally proposed by [Hu et al. \(2014\)](#).

For the conductivity signal velocity, we use the expression commonly used for simulations with self-gravity ([Wadsley et al., 2008](#)):

$$v_{\text{sig},ij} = \frac{|\mathbf{r}_{ij} \cdot \mathbf{v}_{ij}|}{r_{ij}}. \quad (3.15)$$

### 3.3.1.3 Field Reconstruction

Field reconstruction is commonly used in the finite-volume scheme. [Frontiere et al. \(2017\)](#) and [Rosswog \(2020\)](#) used velocity field reconstruction in SPH to reduce excessive artificial diffusion and showed encouraging results. Similar improvement is obtained by [Price and Laibe \(2020\)](#), who used a reconstructed velocity field to compute drag force between gas and dust particles in two-fluid SPH simulations.

We compute the artificial viscosity with velocities linearly reconstructed at the particle mid-point ([Frontiere et al., 2017](#), [Rosswog, 2020](#)). The high-order estimator of the velocity gradient by [Hu et al. \(2014\)](#) is used to reconstruct the velocity field.

### 3.3.1.4 Jeans pressure floor

The non-thermal Jeans pressure floor is introduced to avoid numerical fragmentation. This additional pressure term can be interpreted as unresolved interstellar turbulence and allows us to follow the thermal evolution of atomic gas to low temperature.

The floor is usually implemented as

$$P_{\text{hydro}} = \max\{P, P_{\text{Jeans}}\}, \quad (3.16)$$

and

$$P_{\text{Jeans}} = (\gamma\pi)^{-1}GN_{\text{Jeans}}^2\rho^2\Delta x^2, \quad (3.17)$$

where  $\gamma = 5/3$  is the adiabatic index,  $N_{\text{Jeans}} = 4$  is the Jeans number (Truelove et al., 1997), and  $\Delta x = \max(\epsilon_{\text{grav}}, (m/\rho)^{1/3})$  is the local resolution, which is the larger of the gravitational softening length and the mean particle separation. The  $P$  is the particle's pressure, and  $P_{\text{hydro}}$  is the pressure used in the hydro force evaluation. This implementation works as intended in the density-based SPH formulation; however, care is necessary when used with the pressure-based formulation.

The pressure used in the pressure-based SPH (Eq. 3.9) is obtained from the kernel sum of internal energy. Modifying the pressure alone causes inconsistency between the internal energy and pressure. The appropriate implementation is to introduce a floor in the internal energy.<sup>8</sup> For each SPH particle, we store floored internal energy,  $u_{\text{hydro}} = \max\{u, P_{\text{Jeans}}/[(\gamma - 1)\rho]\}$ , where  $\rho = \sum_j^N m_j W_{ij}(h_i)$  is physical density, in addition to the original internal energy. We use the floored internal energy to compute the smoothed pressure and hydro force. The original internal energy is kept to compute gas temperature.

### 3.3.1.5 Time Integration

In GADGET-4, the hydrodynamical force is integrated using the second-order predictor-corrector method (Springel et al., 2021). In the following, we call the integration width on the timeline a time step, and the point on the timeline where a previous time step ends and the next step begins a synchronization point.

We use the time step limiter that wakes up inactive SPH particles to force a time step constraint (Saitoh and Makino, 2009, Durier and Dalla Vecchia, 2012). For the constraint, we use the signal velocity timestep limiter (Springel, 2010b, Springel et al., 2021) instead of constraining the neighbor's time step within a fixed factor of difference. The signal velocity limiter is more general and flexible than the fixed factor limiter, as demonstrated in Springel (2010b). The implementation of the signal velocity time step limiter in the original GADGET-4 is one-sided, and information on neighboring particles is used to constrain the new time step of a particle. We extended the limiter to a mutual constraint in our GADGET4-OSAKA; when the particle  $i$  is updated, we search its neighbor  $j$  and impose the time step constraint  $\Delta t_j < C_{\text{CFL}}\Delta t_j^{\text{signal}}$ , where

$$\Delta t_j^{\text{signal}} = \frac{2h_j + r_{ij}}{c_i^{\text{snd}} + c_j^{\text{snd}} - \mathbf{r}_{ij} \cdot \mathbf{v}_{ij}/r_{ij}}, \quad (3.18)$$

<sup>8</sup>In the density-based SPH, modifying the particle's pressure is equivalent to modifying its internal energy.

and  $\mathbf{r}_{ij} = \mathbf{r}_i - \mathbf{r}_j$ ,  $\mathbf{v}_{ij} = \mathbf{v}_i - \mathbf{v}_j$ ,  $r_{ij} = |\mathbf{r}_{ij}|$ , and  $c_i^{\text{snd}}$  is the sound speed of  $i$ -th particle. This wake-up scheme ensures that all SPH particles maintain the signal velocity time step criterion even when the velocity and the sound speed of neighboring particles are updated due to feedback.

The evaluation of  $\Delta t_j^{\text{signal}}$  is carried out by walking on the oct-tree used for the neighbor search of SPH particles. For each node of the oct-tree, we store the maximum signal time step  $\Delta t_{\text{max}}^{\text{signal}}$ , the maximum of  $d^{\text{signal}} = c^{\text{snd}} \Delta t^{\text{signal}} - 2h$ , the maximum sound speed  $c_{\text{max}}^{\text{snd}}$ , and the maximum and the minimum of velocity in x-, y-, and z-direction ( $v_{\text{max}}^x, v_{\text{min}}^x, v_{\text{max}}^y, v_{\text{min}}^y, v_{\text{max}}^z, v_{\text{min}}^z$ ) of SPH particles in the node. When we encounter a node in the tree walk, we compute the node opening criterion,

$$d_{\text{min}} < d_{\text{max}}^{\text{signal}} + \Delta t_{\text{max}}^{\text{signal}} (c_i^{\text{snd}} - v_{\text{min}}^{\text{rel}}), \quad (3.19)$$

where  $v_{\text{min}}^{\text{rel}} = \min_j (\mathbf{r}_{ij} \cdot \mathbf{v}_{ij} / r_{ij})$  is the minimum relative velocity, i.e., the largest approaching velocity, between particle  $i$  and particles in the node, which can be constrained using the maximum and minimum velocity of particles in the node. The  $d_{\text{min}}$  is the smallest distance from the particle  $i$  to the node. If the opening condition is fulfilled, we open the node and continue walking on its daughter nodes. When we encounter a particle  $j$ , we compute Eq. (3.18) and update  $\Delta t_j^{\text{signal}}$  if it is smaller. If  $C_{\text{CFL}} \Delta t_j^{\text{signal}}$  is smaller than particle  $j$ 's time step  $\Delta t_j$ , we flag the particle. At the beginning of every synchronization point, we check flagged particles and wake them up if it is the point where a particle with the time step of  $C_{\text{CFL}} \Delta t_j^{\text{signal}}$  should be synchronized.

We note that the tree walk is carried out along with the evaluation of  $\Delta t_i^{\text{signal}}$ , and its node opening criterion is

$$d_{\text{min}} < d_i^{\text{signal}} + \Delta t_i^{\text{signal}} (c_{\text{max}}^{\text{snd}} - v_{\text{min}}^{\text{rel}}). \quad (3.20)$$

We actually open the tree node if the criteria (3.19) or (3.20) are fulfilled, and when we encounter a particle, we compute  $\Delta t_i^{\text{signal}}$  and update if it is smaller.

We also note that the number of neighbor particles can be large when there are particles with high temperatures and/or high relative velocities. In GADGET-4, the default tree walk method is to build a local essential tree, which requires a memory buffer to allocate data of tree nodes and particles on other memory space. When we have a large number of neighbors, the construction of the local essential tree can fail due to memory shortage. We thus implemented the tree-based time step limiter using the generic communication pattern, a C++ class of MPI communication routine available in GADGET-4. The tree walk can be costly when we have many neighbors, but the signal velocity time step



TABLE 3.1: Numerical settings of the models used in the test simulations. (1) Model name. (2) The SPH formulation (Section 3.3.1). (3) Check list of the usage of the artificial conduction (Section 3.3.1.2). (4) Check list of the usage of the velocity field reconstruction (Section 3.3.1.3).

Name (1)	SPH formulation (2)	Artificial conduction (3)	Velocity field reconstruction (4)
PU_AC_Rec	Pressure-Energy	✓	✓
PU_AC	Pressure-Energy	✓	
PU_Rec	Pressure-Energy		✓
PU	Pressure-Energy		
PE_AC_Rec	Pressure-Entropy	✓	✓
DE_AC_Rec	Density-Entropy	✓	✓

limiter chooses the optimal time step for each particle, and unnecessary calculation can be avoided to reduce the computational cost.

In addition to the signal velocity time step constraint, we activate particles that can be subject to stellar or AGN feedback. At the beginning of a synchronization point, we drift neighbor particles around the feedback site and find particles that will receive feedback energy. The neighbor particles are woken up if they are inactive. This ensures that the feedback effect is reflected in hydrodynamics without delay.

### 3.3.2 Code validation

In this subsection, we demonstrate the performance of the above numerical treatment using five test problems. We perform simulations with six different models of numerical settings as summarized in Table 3.1. We compare our fiducial model PU\_AC\_Rec with other runs without artificial conduction, velocity field reconstruction, or using different SPH formulation.

#### 3.3.2.1 Keplerian Disk

The Keplerian disk is a two-dimensional hydrodynamical test for the conservation of angular momentum and numerical diffusion by artificial viscosity and conductivity. The excess in numerical diffusion breaks the conservation of angular momentum and leads to the disruption of the disk. The initial condition has the same density profile as that used by Hopkins (2015) and Hosono et al. (2016);

$$\Sigma = \begin{cases} (r/0.5)^3 & (r < 0.5) \\ 1 & (0.5 < r < 2) , \\ [1 + (r - 2)/0.1]^{-3} & (r > 2) \end{cases} \quad (3.21)$$

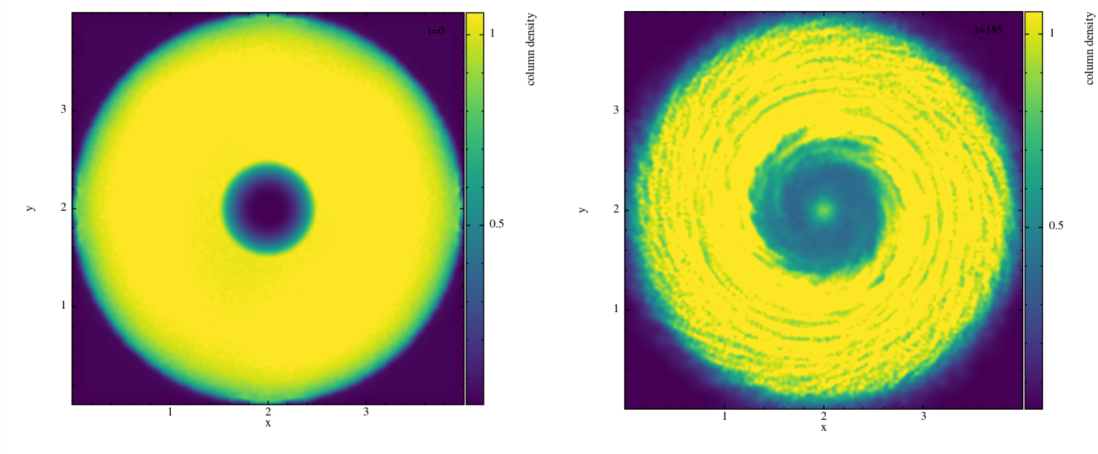


FIGURE 3.1: Surface density of simulated Keplerian disk at initial condition (left) and at the termination of the simulation when the L1 error of azimuthal velocity exceeds 0.01 (right).

where  $\Sigma$  is the gas surface density and  $r$  is the distance from the center. The disk is cold ( $P = 10^{-6}$ ) and is subject to the external Keplerian potential

$$\Phi = -(r^2 + \epsilon^2)^{-1/2}, \quad (3.22)$$

where  $\epsilon = 0.25$  is the gravitational softening length. The corresponding rotational velocity is

$$v_r = |\mathbf{r}|(r^2 + \epsilon^2)^{-3/4}. \quad (3.23)$$

We generate the initial condition using the glass-like initial condition generator WVTICS<sup>9</sup> (Donnert et al., 2017, Arth et al., 2019). The box length is 4 in unit length, and 46,560 SPH particles are employed. We monitor the L1 error of azimuthal velocity

$$L1 = \frac{1}{N} \sum_{0.5 < r < 2.0}^N \frac{|v_{j,\phi} - v_r(r_j)|}{v_r(r_j)}, \quad (3.24)$$

where  $v_{j,\phi}$  is the azimuthal velocity of  $j$ -th particle and  $v_r(r_j)$  is the rotational velocity at the radius of  $j$ -th particle, and terminates the simulation when  $L1$  exceeds 0.01.

The left panel of Figure 3.1 shows the surface density of the simulated Keplerian disk at the initial condition, whose density profile follows equation (3.21). The right panel of Figure 3.1 shows the surface density at the termination of the simulation. The excess artificial viscosity causes the loss of angular momentum of gas at the inner edge of the disk, and then the gas losing its angular momentum forms a gas clump at the center.

<sup>9</sup>The code's website is <https://github.com/jdonnert/WVTICS>

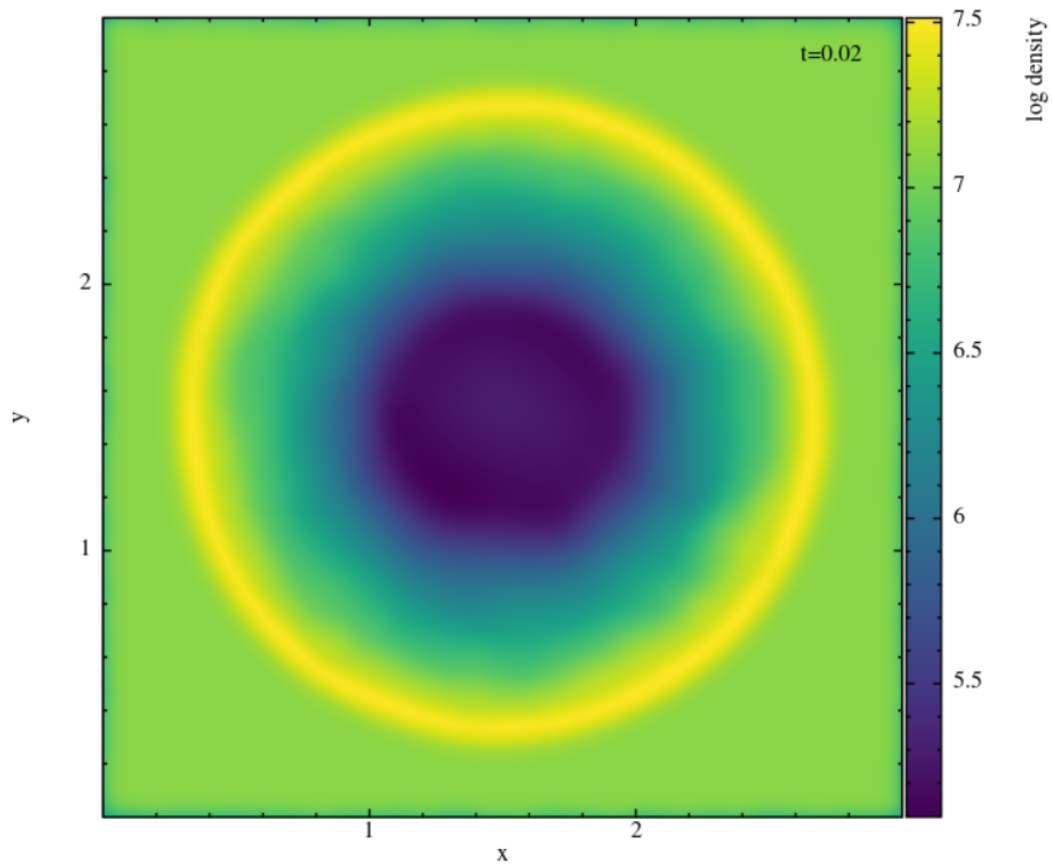


FIGURE 3.2: Density slice through the center of the simulated Sedov blast wave at  $t = 20$  Myr.

In the next subsection, we show the result of the Keplerian disk test in combination with the Sedov Blast test.

### 3.3.2.2 Sedov Explosion

The Sedov blast is a three-dimensional hydrodynamical test of shock capturing, conservation, and integration stability. The blast wave should evolve following the Sedov–Taylor solution.

We use the initial condition generator WVTICS to generate the initial condition, which is identical to that used by Hopkins (2013) and Hu et al. (2014). The box length is  $L = 3$  kpc, and  $64^3$  SPH particles are employed. The thermal energy of  $E = 6.78 \times 10^{53}$  erg is injected into the 63 central particles with a top-hat profile in a homogeneous density field of  $n = 0.5 \text{ cm}^{-3}$ . The ambient temperature is  $T = 10$  K with adiabatic index  $\gamma = 5/3$  and mean molecular weight  $\mu = 1$ .

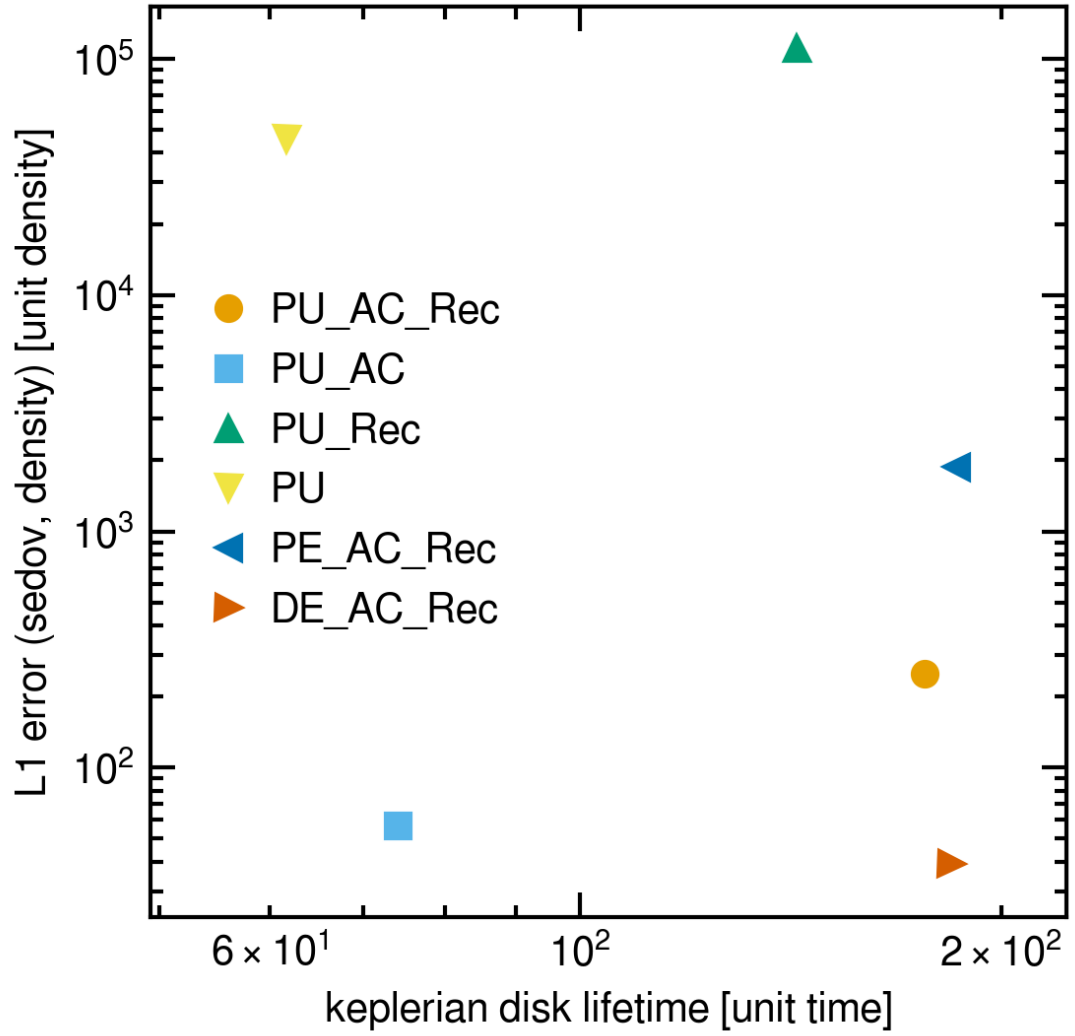


FIGURE 3.3: The comparison of the performance of the six numerical models in the Keplerian disk and Sedov blast tests. The x-axis shows the lifetime of the Keplerian disk, and the longer lifetime indicates the better angular momentum conservation. The y-axis shows the L1 error of density in the Sedov blast test, and the smaller L1 error indicates higher accuracy in the treatment of shocks. The models located in the bottom right perform nicely in both tests.

We calculate the Sedov–Taylor solution by numerical integration of the dimensionless equation of continuity, equation of motion, and energy equation on spherical coordinate and compare it with the snapshot at  $t = 20 \text{ Myr}$  to compute the L1 error of density, pressure, and radial velocity. The L1 error is computed on the range  $[0, 1.1R_{\text{shock}}]$ , where  $R_{\text{shock}}$  is the radius of the shock front. First, the range is linearly-equally divided into 20 bins and L1 error of  $X$  ( $X = \rho, p$ , or  $v$ )

$$L1_i = \frac{1}{N_i} \sum_{r_j \in [r_i, r_{i+1})}^{N_i} \frac{|X_j - X_{ST}(r_j)|}{X_{ST}(r_j)} \quad (3.25)$$

is computed for each bin, where  $X_{ST}(r)$  is the value of  $X$  of the Sedov–Taylor solution obtained by linear interpolation of the result of the numerical integration. Then the L1 error is computed as

$$L1 = \frac{1}{20} \sum_i^{20} L1_i. \quad (3.26)$$

Figure 3.2 shows the density slice through the center of the simulated Sedov blast at  $t = 20$  Myr. The blast wave expands isotropically in the uniform medium.

Figure 3.3 compares the results using the six models in the Keplerian disk and Sedov blast tests. In the Keplerian disk test, the artificial viscosity causes a loss of angular momentum, but in the Sedov explosion test, artificial viscosity is necessary to capture the shock. Triggering the artificial viscosity only when necessary is key to obtaining high performance in both tests. Our fiducial model PU\_AC\_Rec shows a long lifetime of the Keplerian disk and low L1 error in the Sedov blast test. Similar results are obtained with the DE\_AC\_Rec and PE\_AC\_Rec models. This is achieved using velocity field reconstruction, which reduces the artificial viscosity where the velocity field is smooth. This can be confirmed by comparing the PU\_AC\_Rec and PU\_AC run; the PU\_AC\_Rec has more than twice the lifetime of the Keplerian disk but keeps the same order of the L1 error in the Sedov blast test.

In the formulation of pressure-based SPH, we have assumed a smooth pressure field, which is not the case for the shock front. The large L1 error of the PU and PU\_Rec run results from the error at the huge pressure jump. This can be mediated by artificial conduction, which smoothes the pressure discontinuity. The comparison between PU\_AC\_Rec and PU\_AC runs shows that artificial conduction reduces error in resolving the shock with a minor effect in the Keplerian disk test.

### 3.3.2.3 Cold Blob

The cold blob is a three-dimensional hydrodynamic problem proposed by Agertz et al. (2007) to test the capability of the hydro solver to handle Rayleigh–Taylor and Kelvin–Helmholtz instabilities. A spherical cloud of gas is placed in a wind tunnel with periodic boundary conditions, and the cloud is disrupted through hydrodynamical instabilities. This test is designed to capture the same physical processes that occur during the formation and evolution of astrophysical structures and does not have an exact analytic solution. It is known that different hydro solvers show diverging results on this test as shown by Hopkins (2015) and Braspenning et al. (2023).

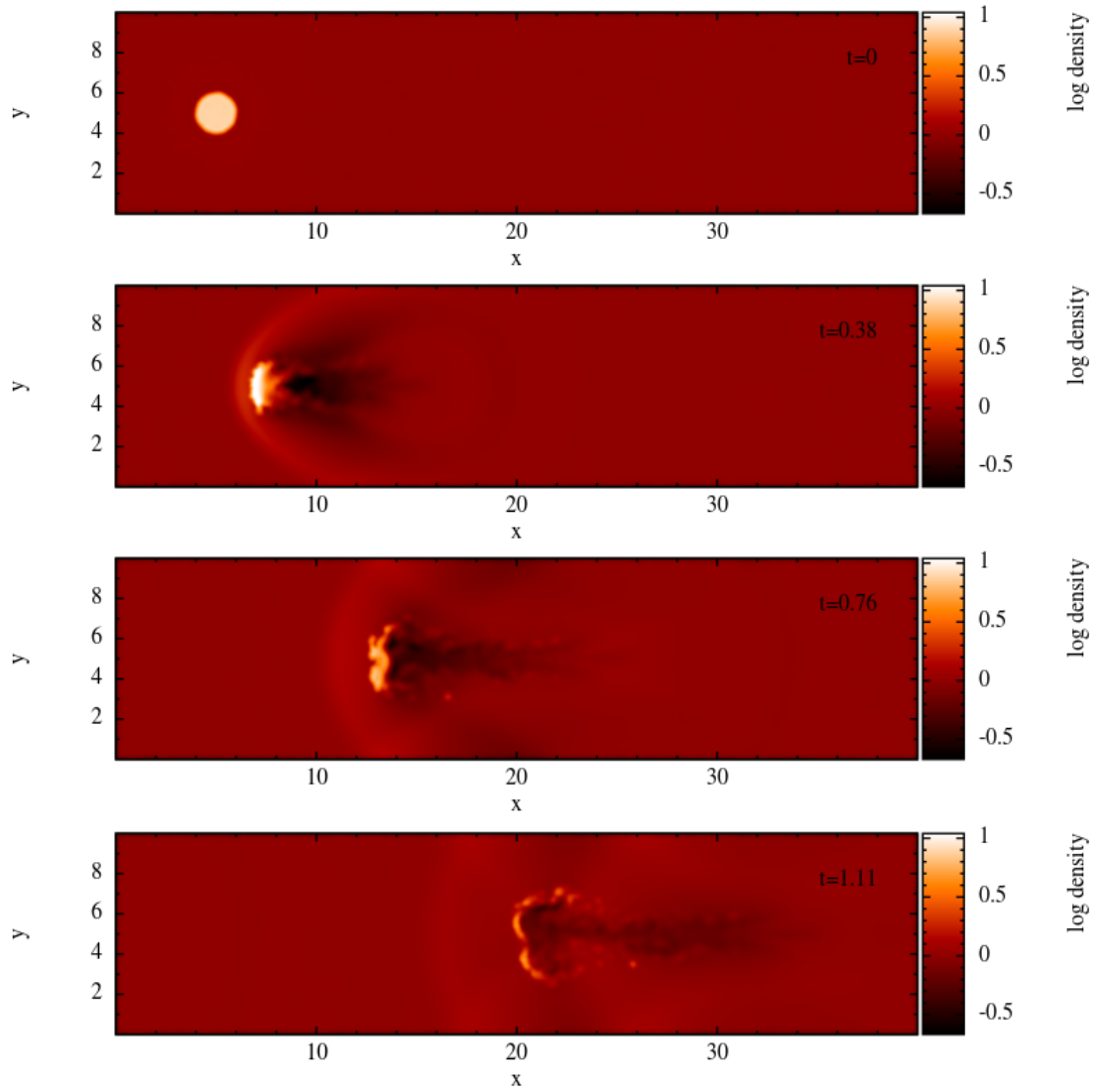


FIGURE 3.4: Density slice through the mid-plane of cold blob test at  $t = 0$ ,  $1 t_{\text{KH}}$ ,  $2 t_{\text{KH}}$ , and  $3 t_{\text{KH}}$  (from top to bottom).

The initial conditions for the blob test are set up in the following way. The simulation box has a size of  $(L_x, L_y, L_z) = (40, 10, 10)$  with periodic boundaries, and a cloud with radius 1 is centered at  $(5, 5, 5)$ . The densities of the cloud and the ambient gas are  $\rho_{\text{cl}} = 10$  and  $\rho_{\text{amb}} = 1$ , respectively. The specific internal energies of the cloud and the ambient gas are set to  $u_{\text{cl}} = 9$  and  $u_{\text{amb}} = 90$ , respectively, so that the cloud and the ambient gas are in pressure equilibrium. The cloud is stationary, and the velocity of the ambient gas is  $\mathbf{v} = (27, 0, 0)$ , corresponding to  $\mathcal{M} = 2.7$  with adiabatic gamma  $\gamma = 5/3$  and mean molecular weight  $\mu = 1$ .

Figure 3.4 shows the time evolution of the blob. The blob is disrupted by the Rayleigh–Taylor and Kelvin–Helmholtz instabilities caused by the surrounding flow.

Figure 3.5 show the cloud remaining fraction. The cloud is defined as being any gas that

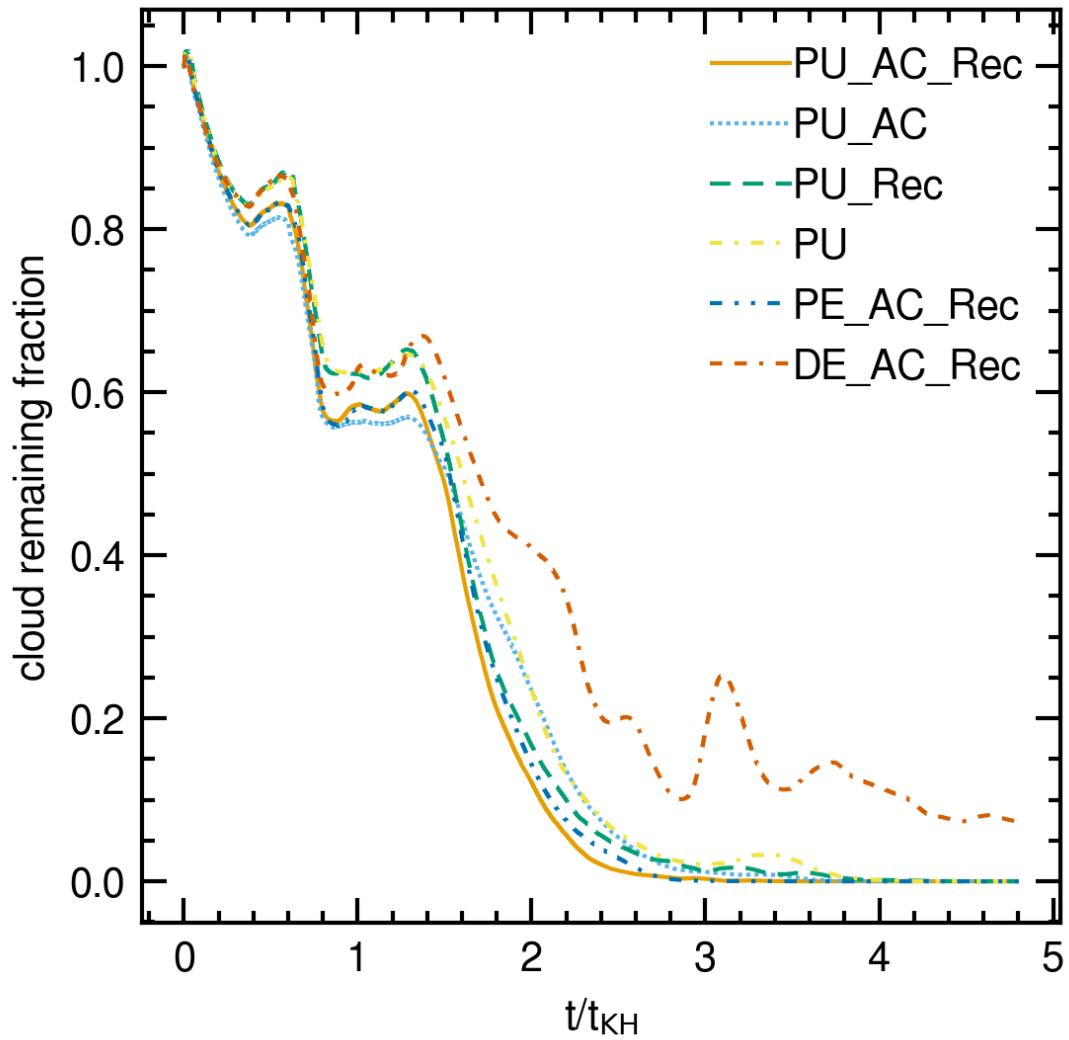


FIGURE 3.5: Cloud remaining fraction as a function of time in the cold blob test.

satisfies  $u < 0.9 u_{\text{amb}}$  and  $\rho > 0.64 \rho_{\text{cl}}$ . The cloud is disrupted at the time when the KHI mode of cloud size has grown fully. The timescale of disruption is often called  $t_{\text{KH}}$ , and its analytically estimated value is (Agertz et al., 2007)

$$t_{\text{KH}} = 1.6\tau_{\text{cr}} = 3.2 \frac{R_{\text{cl}}\chi^{0.5}}{v} \sim 0.375 \left(\frac{R_{\text{cl}}}{1}\right) \left(\frac{\chi}{10}\right)^{0.5} \left(\frac{v}{27}\right), \quad (3.27)$$

where  $\tau_{\text{cr}}$  is the cloud crushing time, and  $R_{\text{cl}}$ ,  $v$ , and  $\chi$  are cloud radius, flow speed, and density ratio between the cloud and surroundings, respectively.

In the runs except for the DE\_AC\_Rec run, the cloud fully disrupts at  $t \sim 2t_{\text{KH}}$ , consistent with the results from grid-based codes (Hopkins, 2015). The DE\_AC\_Rec run has a long disruption time because the density-based SPH formulation assumes a smooth density field. This assumption is broken at the contact discontinuity, and the density-based SPH is not good at solving the instabilities occurring there. In the other

runs using the pressure-based SPH formalism, there are only minor differences due to the usage of artificial conduction and velocity field reconstruction.

### 3.3.2.4 Zeldovich Pancake

The Zeldovich pancake is a three-dimensional test of cosmological hydrodynamics and cosmological integration. A single Fourier mode density perturbation of box size in a baryonic Einstein-de Sitter universe evolves from redshift 99 to 0.

The initial condition is almost identical to that used by Hopkins (2015). The simulation box has size of  $L_{\text{box}} = 64 h^{-1} \text{ Mpc}$  with periodic boundary, and the density parameters are  $(\Omega_{\text{m}}, \Omega_{\text{b}}, \Omega_{\Lambda}) = (1, 1, 0)$ . The number of particles is  $64^3$ . The gas is non-radiative; thus, the setup is independent of the Hubble constant. First, a three-dimensional uniform density field with glass (not grid) particle distribution is generated. Then, the particles are assigned velocities, and their positions are shifted using the Zeldovich approximation. The shifted particle x-coordinate on Eulerian comoving coordinate and x-direction peculiar velocity is

$$x(q, z) = q - \frac{1 + z_c}{1 + z} \frac{\cos(kq)}{k}, \quad (3.28)$$

$$v(q, z) = -H_0 \frac{1 + z_c}{\sqrt{1 + z}} \frac{\cos(kq)}{k}, \quad (3.29)$$

where  $q$  is the Lagrangian coordinate,  $z_c = 1$  is the redshift at the collapse of the perturbation,  $k$  is the wave number of the perturbation, and  $H_0 = 100h \text{ km s}^{-1} \text{ Mpc}^{-1}$  is the current Hubble constant. The Lagrangian coordinate  $q$  is the Eulerian coordinate of the unperturbed initial particle position. This Fourier mode collapses at  $x = L_{\text{box}}/2$  at  $z = 1$ . Here, note again that the Hubble constant is included in the length unit, and thus, the setup is independent of  $h$ . The initial gas temperature is uniformly set to 100 K. The perturbation is in the x-direction, the density is uniform in the yz-plane, and the velocity in the y- and z-direction is zero.

Figure 3.6 shows the time evolution of the Zeldovich pancake. Starting from the condition of almost uniform but with a single Fourier mode, the perturbation grows and collapses at  $z = 0$ , forming a thin plane, the Zeldovich pancake.

We randomly sample  $\sim 2000$  particles and output their x-coordinates, density, temperature, and x-velocity at  $z = 0$ . The x-coordinate is shifted by  $-L_{\text{box}}/2$  so that the pancake comes at  $x = 0$ . The gas is assumed to be primordial with hydrogen mass fraction  $X = 0.76$  and helium mass fraction  $Y = 1 - X$ , and temperature is computed assuming full ionization if  $T > 10^4 \text{ K}$  and atomic otherwise.



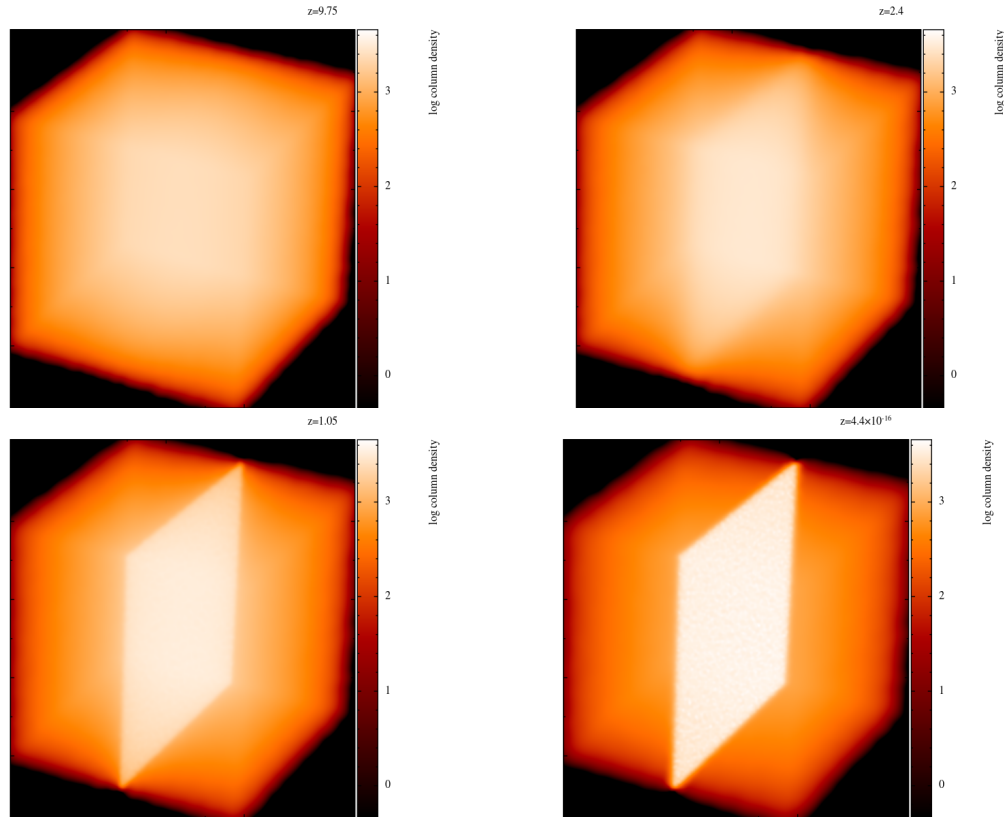


FIGURE 3.6: Density projection of the simulated Zeldovich pancake at  $z = 9.75$ , 2.4, 1.05, and 0 (from top left to bottom right).

The output is compared with the reference result of 1D piecewise parabolic method simulation with high resolution (8194 grids) taken from GIZMO’s test problem suite.<sup>10</sup>

Figure 3.7 shows the density, temperature, and velocity profiles at  $z = 0$ . All runs show agreement with the reference data, indicating the high accuracy of the cosmological integration of the hydro solver of GADGET4-OSAKA code.

### 3.3.2.5 Galaxy Cluster

The cluster test is a zoom-in simulation of a galaxy cluster with a total mass of  $\sim 10^{15} M_{\odot}$  at  $z = 0$ . This test is similar to the simulations performed in the Santa Barbara Cluster Comparison Project by Frenk et al. (1999). It is known that the central part of the entropy profiles of simulated clusters differs among different hydro schemes, and no agreed results have been obtained yet. Therefore, this test cannot be used to validate the code, but it is interesting to see how different the profiles are between different hydro settings. Interested readers are referred also to Springel (2010b), Hopkins (2015), and Sembolini et al. (2016).

<sup>10</sup>The test suite is in the documentation of the GIZMO code, whose website is [http://www.tapir.caltech.edu/~phopkins/Site/GIZMO\\_files/gizmo\\_documentation.html](http://www.tapir.caltech.edu/~phopkins/Site/GIZMO_files/gizmo_documentation.html).

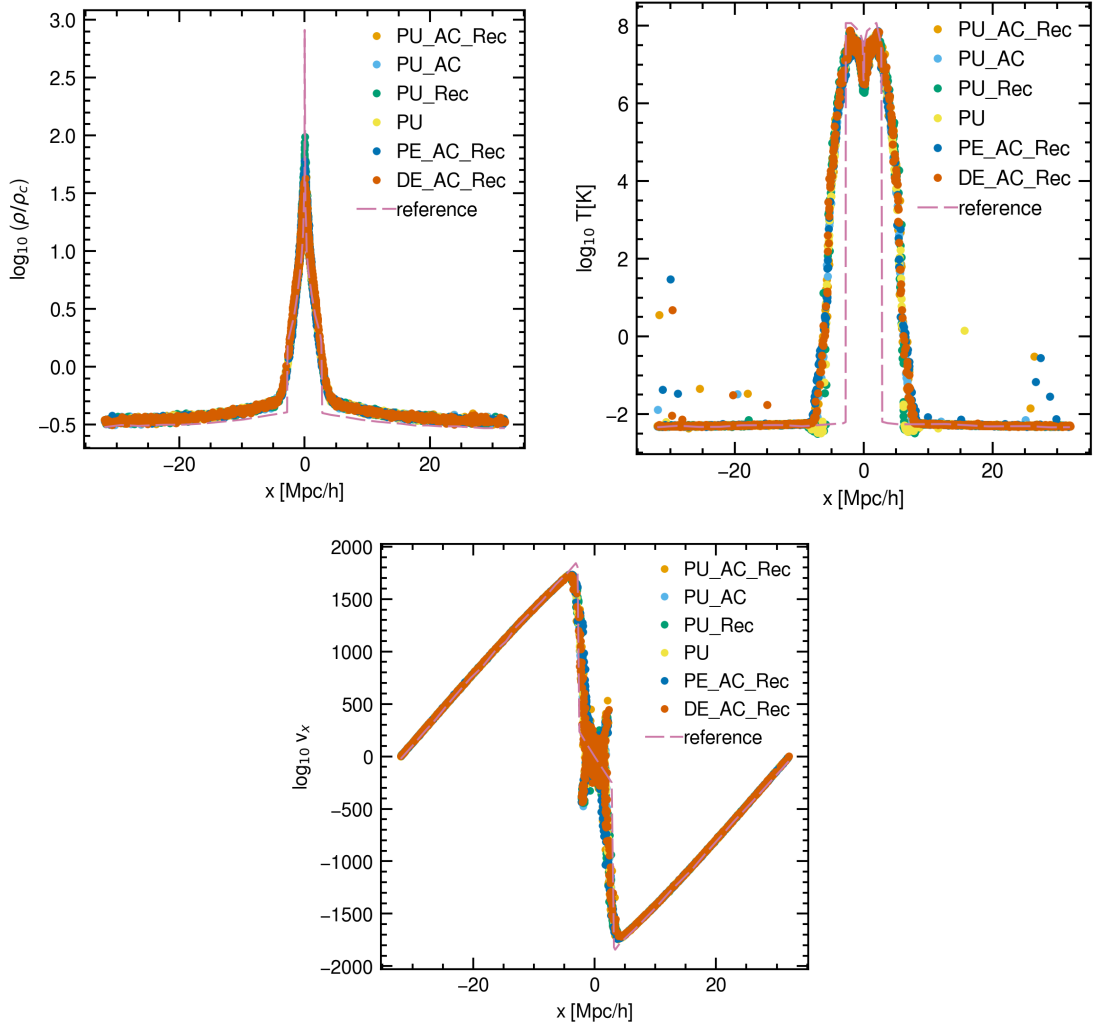


FIGURE 3.7: Density (top left), temperature (top right), and velocity (bottom) profiles of the Zeldovich pancake at  $z = 0$ . Each point indicates the  $x$ -position and each property of a sampled particle. The pink dashed line is the reference result of the 1D Piecewise Parabolic Method (PPM) simulation with high resolution (8194 grids).

The initial condition is generated using the cosmological initial condition generator MUSIC<sup>11</sup> (Hahn and Abel, 2011) with parameters used in Fukushima et al. (2023) but with reduced resolution. The adopted cosmological parameters largely follow those from Planck Collaboration et al. (2016),  $(\Omega_m, \Omega_\Lambda, \Omega_b, h, \sigma_8, n_s) = (0.3089, 0.6911, 0.0486, 0.6774, 0.811, 0.961)$ . The size of the simulation box is  $L = 100 h^{-1} \text{Mpc}$ , and the finest refinement level is 8, resulting in the particle mass of baryon and dark matter are  $8.04 \times 10^8 h^{-1} M_\odot$  and  $4.31 \times 10^9 h^{-1} M_\odot$ , respectively.

Figure 3.8 shows the time evolution of the simulated cluster. We do not include any astrophysical effects, including cooling and feedback, and the gas is heated by the virial shock for its thermal pressure to balance with gravity.

<sup>11</sup>The code's website is <https://bitbucket.org/ohahn/music/src/master/>.

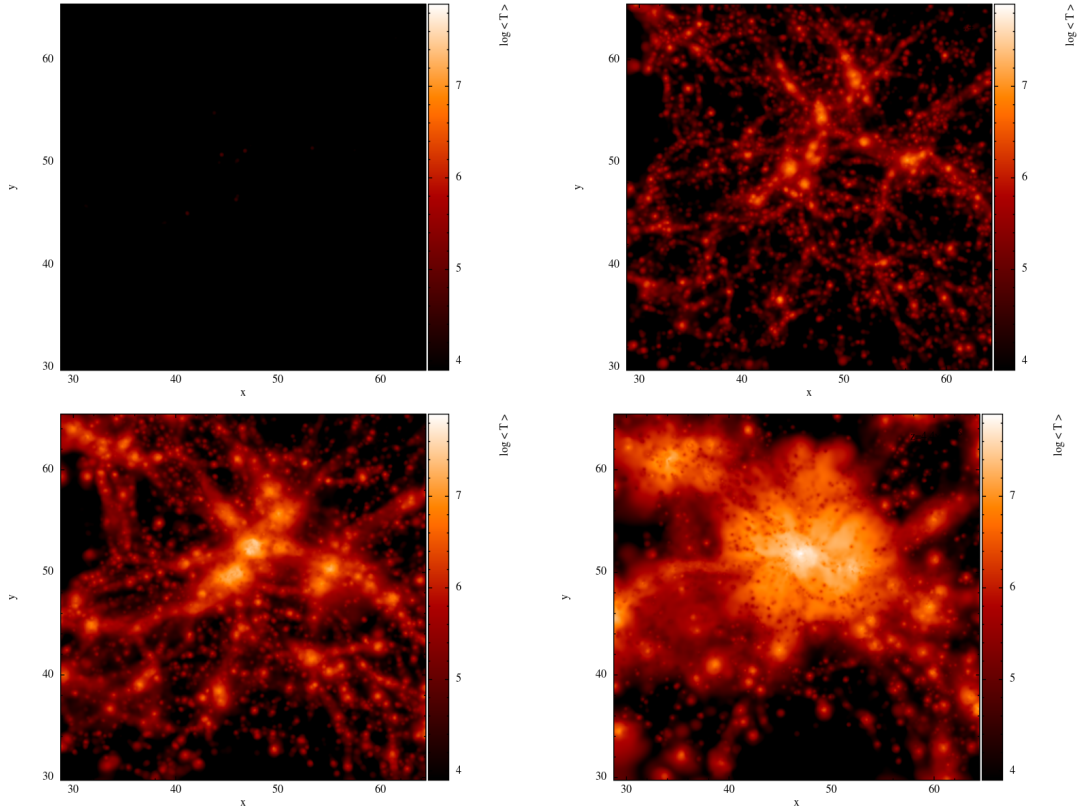


FIGURE 3.8: Projected density-weighted temperature of the simulated cluster at  $z = 9.75, 2.4, 1.05,$  and  $0$  (from top left to bottom right).

Figure 3.9 shows the radial profiles of density, temperature, entropy, and pressure at  $z = 0$ . The density profiles of dark matter are consistent with each other among the simulations, and the gas density at the center is slightly higher in the PU and PU\_Rec runs than in others. The PU and PU\_Rec runs have lower temperature and entropy at the cluster center than the other runs. The higher entropy in runs with artificial conduction suggests that artificial conduction promotes the diffusion of cold clumps. The pressure profiles are consistent among the simulations because they have the same gravitational potential due to dark matter, and gas has to be in equilibrium with gravity by its thermal pressure. The different entropy profiles indicate the effect of artificial conduction in cluster evolution, but there is no analytical solution nor fiducial simulation result, and we cannot conclude which model is better in this comparison.

### 3.4 Subgrid physics

In the following subsections, we describe our treatment of subgrid star formation, stellar feedback, and **black hole (BH)** physics. In this work, **SNe** and **AGB** stars are considered as sources of stellar feedback, while early stellar feedback, e.g., stellar radiation and

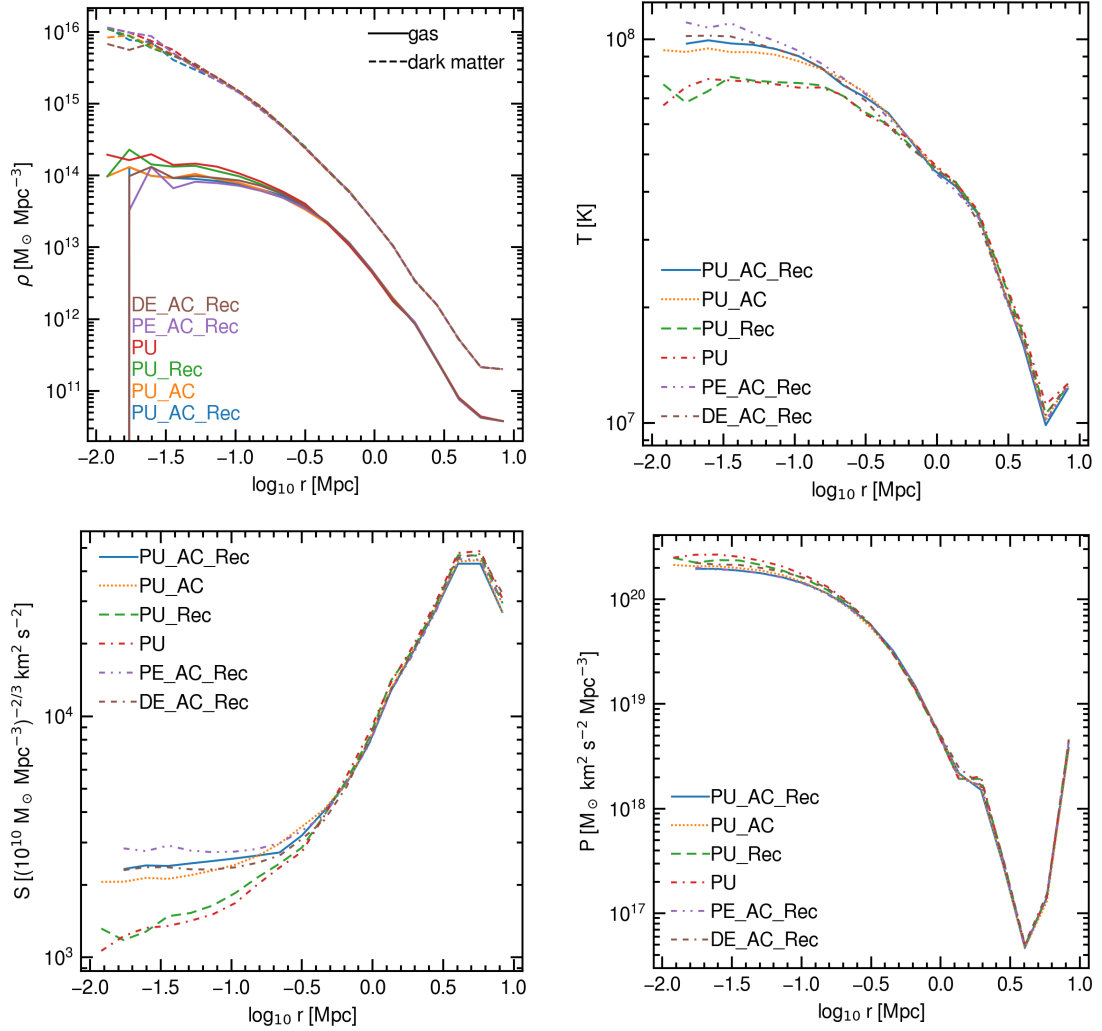


FIGURE 3.9: Radial profiles of density, temperature, entropy, and pressure (from top left to bottom right) of the cluster test at  $z = 0$ .

stellar wind, is neglected. The adopted values of parameters introduced in the following subsections are summarized in Table 3.2.

### 3.4.1 Star Formation

We assume star formation to occur when the hydrogen number density is higher than the threshold density,  $n_{\text{thres}} = 0.1 \text{ cm}^{-3}$ , and the temperature is lower than the threshold temperature,  $T_{\text{thres}} = 10^4 \text{ K}$ . Each gas particle is allowed to spawn  $n_{\text{spawn}}$  star particles at most, and the mass of the star particle is  $m_* = m_{\text{gas}}/n_{\text{spawn}}$ , where  $m_{\text{gas}}$  is the mass of the gas particle, and  $n_{\text{spawn}} = 2$ .

We use the SSP approximation; a star particle represents a cluster of stars with the same metallicity, and their mass function follows an adopted IMF. For the IMF, its

TABLE 3.2: List of common parameters for subgrid physics

Parameter	Adopted value	Description
$n_{\text{thres}}$	$0.1 \text{ cm}^{-3}$	Lower density threshold to allow star formation
$T_{\text{thres}}$	$10^4 \text{ K}$	Upper temperature threshold to allow star formation
$\epsilon_*$	0.01	Star formation efficiency
$n_{\text{spawn}}$	2	Maximum number of stars spawned from one gas particle
$N_{\text{ngb,fb}}$	$8 \pm 2$	Number of gas particles subject to feedback
$n_{\text{event,snii}}$	2	SNII feedback event number
$n_{\text{event,snia}}$	8	SNIa feedback event number
$n_{\text{event,agb}}$	8	AGB feedback event number
$M_{\text{seeding,FoF}}$	$10^{10} h^{-1} M_{\odot}$	FoF mass threshold to seed BH
$M_{\text{seeding,star}}$	$10^8 h^{-1} M_{\odot}$	FoF stellar mass threshold to seed BH
$\epsilon_r$	0.1	Radiative efficiency of BH
$\epsilon_{\text{FB}}$	0.15	AGN feedback efficiency
$\Delta T_{\text{AGN}}$	$10^{8.5} \text{ K}$	AGN feedback temperature

dependence on metallicity and redshift is considered based on the star cluster formation simulation by [Chon et al. \(2022\)](#). They have investigated IMF at a metallicity range of  $10^{-4} \leq Z/Z_{\odot} \leq 10^{-1}$  and redshift range of  $0 \leq z \leq 20$  and quantified the mass fraction of excess component from a Salpeter-like component,

$$f_{\text{massive}} = 1.07(1 - 2^x) + 0.04 \times 2.67^x \times z, \quad (3.30)$$

with  $x = \min\{1 + \log_{10}(Z/Z_{\odot}), 0\}$ , where  $z$  is the redshift. The metallicity range investigated by [Chon et al. \(2022\)](#) is limited to  $Z \leq 0.1 Z_{\odot}$ , and we use the value of  $f_{\text{massive}}$  at  $Z = 0.1 Z_{\odot}$  for the higher metallicity because IMF at  $Z = 0.1 Z_{\odot}$  and  $z = 0$  is already similar to present day Salpeter-like IMF. Figure 3.10 shows the variation of IMF depending on  $f_{\text{massive}}$ . We first assume the Chabrier IMF ([Chabrier, 2003](#)) with stellar mass range  $0.1 M_{\odot} < M < 100 M_{\odot}$ , and then add a log-flat component at  $5 M_{\odot} < M < 100 M_{\odot}$  with mass fraction  $f_{\text{massive}}$  to allow for a treatment of top-heavy IMF.

When a star particle is spawned from a gas particle,  $f_{\text{massive}}$  is computed from the metallicity of the gas particle and the redshift at that time, which is used later for computing energy and metal yield by SNe and AGB stars. In computing the metal and energy yields, we use the metallicity of the star particle with a floor of  $Z_{\text{yield,floor}} = 0.03 Z_{\odot}$ . This metallicity floor is introduced to consider the metal enrichment by unresolved early star formation, and the  $Z_{\text{yield,floor}}$  is similar to the observed metallicity of galaxies with  $M_* \sim 10^7 M_{\odot}$ .

The star formation rate for a gas particle follows the local Schmidt law ([Schmidt, 1959](#)),

$$\dot{\rho}_* = \epsilon_* \frac{\rho}{t_{\text{ff}}}, \quad (3.31)$$

where  $t_{\text{ff}} = \sqrt{3\pi/32G\rho}$  is the local free fall time and  $\epsilon_* = 0.01$  is the star formation efficiency. Star particles are spawned stochastically (Katz, 1992, Springel and Hernquist, 2003, Shimizu et al., 2019) following the star formation rate.

### 3.4.2 Core Collapse Supernova

When a massive star ( $\gtrsim 8 M_{\odot}$ ) ends its life, its major path is to explode as **core-collapse supernova (CCSN)**. Typically, there is one massive star per  $100 M_{\odot}$  stars, and the kinetic energy of a supernova is  $10^{51}$  erg; the specific SN energy is  $\zeta_{\text{SN}} = 10^{49}$  erg  $M_{\odot}^{-1}$ . However, the specific energy can vary due to multiple factors, e.g., stellar IMF, lower and upper limits of SN progenitor mass, and energy per SN. The specific SN energy adopted in previous works varies by more than a factor of two (Keller and Kruijssen, 2022).

Some supernovae, called hypernovae (HNe) or superluminous supernovae, have an order of higher explosion energy of  $10^{52}$  erg. The number fraction of HNe in a solar metallicity environment is about one per cent, but it is observationally suggested that the HN fraction increases at subsolar metallicity (Moriya et al., 2018, Gal-Yam, 2019). From a cosmological hydrodynamic simulation of galaxies, Kobayashi et al. (2006) suggested that the HN fraction of 50% is necessary to explain the zinc abundance.

In this work, we use the yield model by Nomoto et al. (2013), which covers the progenitor mass range of 13–40  $M_{\odot}$ . We assume that some CCSNe with progenitor masses of 20–40  $M_{\odot}$  explode as HNe, and its number fraction in that mass range is 50% at  $Z < 10^{-3}$  and 1% otherwise. We generate a yield table as a function of stellar age using the chemical evolution library CELIB (Saitoh, 2017). The bottom panel of Figure 3.10 shows the specific energy of CCSNe as a function of metallicity in our model. A low-metallicity star’s specific energy is higher due to top-heavy IMF and higher HN fraction.

We divide the Type-II SN feedback from a star particle into  $n_{\text{event,snii}}$  events so that the SN energy and metal yields are deposited gradually rather than instantaneously (Shimizu et al., 2019), and in this work, we adopt  $n_{\text{event,snii}} = 2$ . The SN feedback event occurs following the yield table, considering the stellar age. The energy and metal output of SN is distributed to surrounding  $N_{\text{ngb,fb}} = 8 \pm 2$  gas particles using the feedback model developed in Oku et al. (2022) with some updates, as we briefly summarize in the following. The model consists of two components: local mechanical feedback and galactic wind feedback.

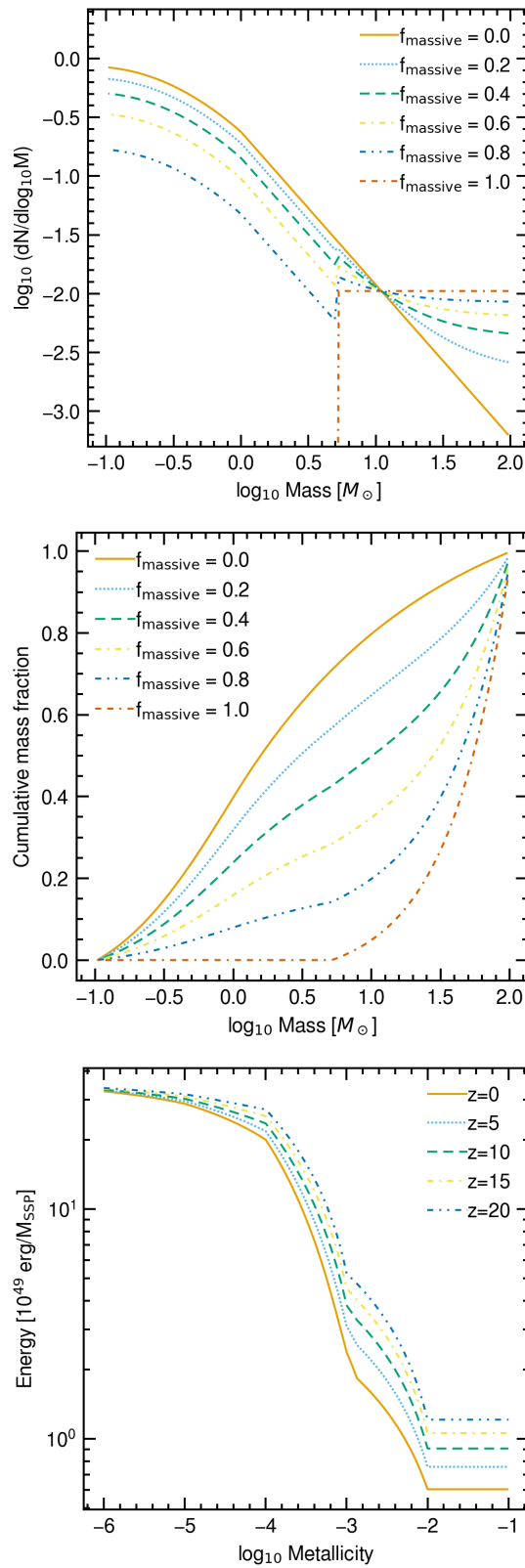


FIGURE 3.10: *Top panel:* Metallicity- and redshift-dependent IMF assumed in this work. *Middle:* Cumulative mass fraction of the stars following the IMF's shown in the top panel. *Bottom:* Metallicity- and redshift-dependent specific energy of Type-II supernova.

### 3.4.2.1 Mechanical Feedback Model

The mechanical feedback model accounts for the momentum injection by SN remnants acquired in the unresolved Sedov–Taylor and pressure-driven snowplow phases. Oku et al. (2022) have performed three-dimensional hydrodynamic simulations using ATHENA++ code (Stone et al., 2020) to investigate the momentum of superbubble formed by clustered SN explosions in a variety of density and metallicity environments with different intervals of SN explosions. The terminal momentum obtained in the simulations is normalized over an initial mass function of star clusters and finally translated into the terminal momentum per SN,

$$\hat{p} = 1.75 \times 10^5 \text{ M}_\odot \text{ km s}^{-1} n_0^{-0.05} \Lambda_{6,-22}^{-0.17}, \quad (3.32)$$

where  $n_0 = n_{\text{H}}/(1 \text{ cm}^{-3})$ , and  $\Lambda_{6,-22} = \max\{1.9 - 0.85 (Z/Z_\odot), 1.05\} \times (Z/Z_\odot) + 10^{-1.33}$  is the value of cooling function of Sutherland and Dopita (1993) at  $10^6 \text{ K}$  normalized by  $10^{-22} \text{ erg s}^{-1} \text{ cm}^3$ . For every feedback event, the local density and metallicity are computed, and the SN energy is translated to momentum using Eq. (3.32) assuming that the energy per SN is  $10^{51} \text{ erg}$ .

The momentum is distributed to surrounding particles with weights calculated using Voronoi tessellation. Metals from Type-Ia SNe, Type-II SNe, and AGB stars are distributed using the same weights. When coupling the feedback momentum to surrounding particles, we limit the momentum if necessary to ensure manifest energy conservation considering the relative velocity of star and gas particles for individual coupling events (see Appendix B1 of Hopkins et al., 2023b). We did not consider the manifest conservation of total energy and linear momentum of multiple feedback events as discussed in Appendix B3 of Hopkins et al. (2023b), and this would be a task for future development of GADGET4-OSAKA, while its effect would be small in our low-resolution simulation where most of SN event is at the momentum-conserving limit on the resolved scale.

### 3.4.2.2 Supernova-driven Galactic Wind Model

The galactic wind model accounts for the hot ( $T \gtrsim 10^6 \text{ K}$ ) galactic wind driven by SNe. We use the scaling relations by Kim et al. (2020a) to determine mass, energy, and metal loading factors from metallicity and star formation surface density. The star formation surface density is estimated as  $\Sigma_{\text{SFR}} = \rho_{\text{SFR}} H$ , where  $\rho_{\text{SFR}}$  is the star formation rate density and  $H = \rho/|\nabla\rho|$  is the gas scale height obtained using the Sobolev-like approximation. The model provides the scaling relations for cool ( $T \lesssim 10^4 \text{ K}$ ) and hot ( $T \gtrsim 10^6 \text{ K}$ ) galactic outflows based on the TIGRESS simulation (Kim et al., 2020b), and we employ the model for hot phase.



In our previous work (Oku et al., 2022), we used a constant entropy wind based on the galactic wind property in the high-resolution dwarf galaxy simulation by Hu (2019) assuming a fixed energy loading factor  $\eta_e = 0.7$ . By updating our model as described above, we no longer have to assume  $\eta_e$ , thus reducing one free parameter.

Our simulation has the mechanical feedback model, which drives the cool wind, and we did not use the wind model for the cool phase. The galactic wind model for the hot phase is necessary for low-resolution simulations that cannot resolve the Sedov–Taylor phase because the mechanical feedback model is for the snowplow phase where the SN bubble has cooled down, and treatment to avoid overcooling is necessary to produce hot galactic wind (Oku et al., 2022).

We follow the TWIND sampling procedure described in Appendix B of Kim et al. (2020a) to sample wind particles and determine their temperature, metallicity, and wind velocity except for the first step. For the first step, we obtain the mass of the hot wind as  $M_{\text{hot}} = \tilde{\eta}_M^{\text{hot}}(m_*/n_{\text{event,snii}})(\zeta_{\text{SN}}/\zeta_{\text{TIGRESS}})$ , where  $\tilde{\eta}_M^{\text{hot}}$  is the mass loading factor obtained as a function of  $\Sigma_{\text{SFR}}$ . The second term represents the stellar mass contributing to one feedback event. The third term is a factor considering the difference in the energy yield, where  $\zeta_{\text{SN}}$  and  $\zeta_{\text{TIGRESS}}$  are the specific SN energy adopted in our simulation and the TIGRESS framework (Kim and Ostriker, 2017, Kim et al., 2020a). The specific SN energy adopted in our simulation is redshift- and metallicity-dependent as shown in Fig. 3.10, and  $\zeta_{\text{TIGRESS}} = 1.05 \times 10^{49} \text{ erg } M_{\odot}^{-1}$ .

The sampled particles are flagged as wind particles and kicked at the wind velocity in random directions isotropically. We assume that wind particles represent the hot galactic wind flowing through unresolved low-density channels, and we disable their hydrodynamical interaction and cooling to avoid the wind particles being affected by ISM. We re-couple the wind particle to hydrodynamics and enable cooling after its density falls below 0.05 times the threshold density of star formation or 0.025 times the current Hubble time has elapsed, following the criteria used in the IllustrisTNG model (Pillepich et al., 2018b).

### 3.4.3 Type-Ia Supernova

For Type-Ia SNe, the element yield table by Seitenzahl et al. (2013) is used in combination with a power-law delay-time distribution function of  $\Psi(t) = 4 \times 10^{-13} \text{ SN yr}^{-1} M_{\odot}^{-1} (t/1 \text{ Gyr})^{-1}$  with minimum delay of 40 Myr (Maoz and Mannucci, 2012). We divide the Type-Ia SN feedback from a star particle into  $n_{\text{event,snia}} = 8$  events. The energy per Type-Ia SN is fixed to  $10^{51}$  erg, and we use Eq. (3.32) to convert the energy to feedback momentum. We did not consider thermal galactic wind feedback for Type-Ia SNe because their degree

of clustering is low, and they are not considered to be the major driver of the galactic wind.

### 3.4.4 AGB Stars

For AGB stars, two yield tables are combined to cover the mass range of  $1\text{--}8 M_{\odot}$ ; Karakas (2010) table is used in  $M_*/M_{\odot} \in [1, 6]$ , Doherty et al. (2014) table in  $M_*/M_{\odot} \in [7, 8]$ , and we linearly interpolate between them. We do not consider the mechanical feedback due to the stellar wind of AGB stars. We divide the AGB feedback from a star particle into  $n_{\text{event,agb}} = 8$  events.

### 3.4.5 Black Hole Physics

For the supermassive BHs, we largely follow the model used in the EAGLE project (Schaye et al., 2015, Crain et al., 2015). The model consists of seeding using the Friend-of-Friends (FoF) halo finder, torque-limited Bondi–Hoyle accretion, and thermal quasar feedback, as summarized below.

#### 3.4.5.1 Seeding & Repositioning

We regularly run the FoF halo finder with an interval of  $\Delta \ln a = 0.005$ , where  $a = 1/(1+z)$  is the scale factor, and convert the gas particle with a minimum gravitational potential in the halo to a BH particle if the total mass of the halo is larger than  $M_{\text{seeding,FoF}} = 10^{10} h^{-1} M_{\odot}$ , stellar mass in the halo is larger than  $M_{\text{seeding,star}} = 10^8 h^{-1} M_{\odot}$ , and does not contain BHs.

If a FoF halo contains BH particles and the BHs are within three times the gravitational softening length of BH particles from the star particle with minimum potential, the BH particles are repositioned and assigned the velocity of the FoF halo.

#### 3.4.5.2 Accretion

The mass accretion rate onto BH is computed by the Eddington-limited Bondi rate. The Bondi rate (Bondi, 1952) is

$$\dot{M}_{\text{Bondi}} = \frac{4\pi G^2 M_{\text{BH}}^2 \rho}{(c_s^2 + v_{\text{BH}}^2)^{3/2}}, \quad (3.33)$$

where  $G$  is the gravity constant,  $M_{\text{BH}}$  is the BH mass, and  $v_{\text{BH}}$  is the velocity of the BH relative to the surrounding medium. We set  $v_{\text{BH}}$  to zero because the velocities of BH particles are set by hand when repositioned. In computing the sound speed  $c_s$ , we assume the effective equation of state (EoS) used in the EAGLE project, i.e.,  $c_s = \sqrt{\gamma(k_{\text{B}}/\mu_{\text{a}}m_{\text{p}})T_{\text{eos}}}$ , where  $\gamma = 5/3$  is the adiabatic index,  $k_{\text{B}}$  is the Boltzmann constant,  $\mu_{\text{a}} = 1.2285$  is the mean molecular weight of primordial atomic gas,  $m_{\text{p}}$  is the proton mass, and  $T_{\text{eos}} = 8 \times 10^3 \text{ K} (n_{\text{H}}/0.1 \text{ cm}^{-3})^{1/3}$  is the temperature derived from the EoS. The EoS is used only in computing the BH accretion rate for consistency with the accretion model of the EAGLE simulation.

The Eddington accretion rate is

$$\dot{M}_{\text{Eddington}} = \frac{4\pi G M_{\text{BH}} m_{\text{p}}}{\epsilon_r c \sigma_{\text{T}}}, \quad (3.34)$$

where  $\epsilon_r = 0.1$  is the radiative efficiency of BH,  $c$  is the speed of light, and  $\sigma_{\text{T}}$  is the Thomson cross section. The accretion rate is the minimum of the Bondi rate and the Eddington rate

$$\dot{M}_{\text{acc}} = \min(\dot{M}_{\text{Eddington}}, C \dot{M}_{\text{Bondi}}), \quad (3.35)$$

where  $C = \min(C_{\text{visc}}^{-1}(c_s/v_{\phi})^3, 1)$  is a factor to limit the Bondi rate considering the angular momentum and the viscosity of the accretion disk on a subgrid scale (Rosas-Guevara et al., 2015). We set the model parameter  $C_{\text{visc}}$  to  $200\pi$  in our fiducial run, and  $v_{\phi}$  is the rotation speed of gas around the BH.

We use the subgrid BH mass to follow the growth of BH (Springel et al., 2005). Each BH particle has particle mass,  $m_{\text{part}}$ , and subgrid BH mass,  $M_{\text{BH}}$ ; the former is used in the computation of gravitational force and potential, and the latter is used for the calculation of the accretion rate onto the black hole. The mass growth rate of the BH is

$$\dot{M}_{\text{BH}} = (1 - \epsilon_r) \dot{M}_{\text{acc}}. \quad (3.36)$$

The BH particles swallow the surrounding gas particles stochastically following their subgrid BH mass. For each gas particle  $j$  around the BH, we compute a probability

$$p_{j,\text{acc}} = \frac{w_j \Delta m}{\rho}, \quad (3.37)$$

where  $w_j$  is the kernel weight of the gas particle relative to the BH,  $\Delta m = \max(M_{\text{BH}} - m_{\text{part}}, 0)$  is the mass increment from the BH particle mass to the subgrid mass, and  $\rho$  is the gas density at the position of the BH. We then draw a uniform random number  $x_j \in [0, 1]$ , and the BH absorbs the gas particle with conserving mass and momentum if  $x_j < p_{j,\text{acc}}$ .

### 3.4.5.3 Feedback

The AGN feedback is modeled by stochastic thermal energy injection. Each BH particle has an energy reservoir, and we increase it at a rate of  $\dot{E}_{\text{res}} = \epsilon_r \epsilon_{\text{FB}} \dot{M}_{\text{acc}} c^2$ , where  $\epsilon_{\text{FB}} = 0.15$  is the efficiency of converting AGN radiation to thermal energy via radiative pressure. When  $E_{\text{res}}$  is large enough to increase the temperature of a gas particle by  $\Delta T_{\text{AGN}}$ , the BH is allowed to distribute feedback energy stochastically. Similarly to the treatment of accretion, for each gas particle  $j$  around the BH, we compute a probability

$$p_{j,\text{FB}} = \frac{(\gamma - 1)\mu_i m_p w_j E_{\text{res}}}{k_B \Delta T_{\text{AGN}} \rho}, \quad (3.38)$$

where  $\mu_i = 0.588$  is the mean molecular weight of a primordial ionized gas, and draw a uniform random number  $y_j \in [0, 1]$ . The thermal energy of

$$E_{j,\text{FB}} = \frac{m_j k_B \Delta T_{\text{AGN}}}{(\gamma - 1)\mu m_p} \quad (3.39)$$

is added to the gas particle if  $y_j < p_{j,\text{FB}}$ , and then we reduce  $E_{\text{res}}$  by  $E_{j,\text{FB}}$ .

### 3.4.5.4 Timestepping

The timestep size of a black hole is limited to constrain the accreting mass and feedback energy per time step. The accretion timestep is determined to limit the mass growth rate of a black hole per time step to less than 10% and the number of SPH particles swallowed by a black hole to one:

$$\Delta t_{\text{acc}} = \min \left\{ 0.1 \frac{M_{\text{BH}}}{\dot{M}_{\text{BH}}}, \frac{\bar{m}_{\text{gas}}}{\dot{M}_{\text{BH}}} \right\}, \quad (3.40)$$

where  $\bar{m}_{\text{gas}}$  is the mean gas particle mass. The feedback timestep is determined as

$$\Delta t_{\text{FB}} = 0.3 \frac{N_{\text{ngb,BH}} \bar{m}_{\text{gas}} k_B \Delta T_{\text{AGN}}}{(\gamma - 1)\mu m_p \dot{E}_{\text{res}}}, \quad (3.41)$$

such that the fraction of neighboring SPH particles that receive feedback energy is less than 30% within the kernel. We use the shortest of  $\Delta t_{\text{acc}}$ ,  $\Delta t_{\text{FB}}$ , and the gravitational timestep size of the black hole particle.

## 3.5 Runs

We conduct simulations with varied feedback settings, black hole accretion parameters, and resolution as summarized in Table 3.3.

TABLE 3.3: List of simulations. The columns list (1) the run name; (2) the box size in comoving Mpc,  $L_{\text{box}}$ ; (3) the number of particles employed in the run,  $N_{\text{particle}}$ ; (4) the subgrid viscous parameter for BH accretion,  $C_{\text{visc}}$ ; (5) the subgrid mass of BH seed,  $m_{\text{seed}}$ ; (6-8) the checklist of feedback modules activated in the run, (6) the mechanical feedback from core-collapse SNe (see Section 3.4.2.1), (7) the SN-driven galactic wind model (see Section 3.4.2.2), and (8) AGN feedback (see Section 3.4.5.3); (9) the stellar IMF; (10) the number fraction of HNe.

Name (1)	$L_{\text{box}}$ (2)	$N_{\text{particle}}$ (3)	$C_{\text{visc}}$ (4)	$m_{\text{seed}}$ (5)	Feedback Type					HN fraction (10)
					SN Mechanical (6)	SN GalWind (7)	AGN (8)	Stellar IMF (9)	HN fraction (10)	
Fiducial	50	$2 \times 512^3$	$200\pi$	$1 \times 10^5$	✓	✓	✓	variable <sup>a</sup>	Z-dependent <sup>b</sup>	
NoSNGalWind	50	$2 \times 512^3$	$200\pi$	$1 \times 10^5$	✓		✓	variable	Z-dependent	
AGNonly	50	$2 \times 512^3$	$200\pi$	$1 \times 10^5$			✓	variable	Z-dependent	
SNonly	50	$2 \times 512^3$	$200\pi$	$1 \times 10^5$	✓	✓		variable	Z-dependent	
NoFB	50	$2 \times 512^3$	$200\pi$	$1 \times 10^5$				variable	Z-dependent	
LowCvisc	50	$2 \times 512^3$	$2\pi$	$1 \times 10^5$	✓	✓	✓	variable	Z-dependent	
LowCviscLowMseed	50	$2 \times 512^3$	$2\pi$	$1 \times 10^4$	✓	✓	✓	variable	Z-dependent	
L25N512	25	$2 \times 512^3$	$200\pi$	$1 \times 10^5$	✓	✓	✓	variable	Z-dependent	
L25N256	25	$2 \times 256^3$	$200\pi$	$1 \times 10^5$	✓	✓	✓	variable	Z-dependent	
L25N128	25	$2 \times 128^3$	$200\pi$	$1 \times 10^5$	✓	✓	✓	variable	Z-dependent	
L25N256NoZdepSN	25	$2 \times 256^3$	$200\pi$	$1 \times 10^5$	✓	✓	✓	Chabrier	0.01	

<sup>a</sup>The metallicity- and redshift-dependent IMF (see Section 3.4.1)

<sup>b</sup>The redshift-dependent HN fraction (see Section 3.4.2)

The Fiducial run considers the two-component SN feedback and AGN feedback. The NoSNGalWind run does not use the SN-driven hot galactic wind model. It is presented to show the effect of explicit modeling of the galactic wind in comparison to the Fiducial run. The AGNonly and SNonly runs only consider AGN and SN feedback, respectively, and are performed to investigate the impact of these feedbacks. The NoFB run does not consider any feedback and is presented as a baseline to show the impact of feedback in comparison to other runs.

The LowCvisc and LowCviscLowMseed runs adopt black hole accretion parameters different from the Fiducial run. In these two runs, we adopt  $C_{\text{visc}} = 2\pi$  (same value as the fiducial EAGLE simulation), which is 100 times smaller than the one adopted in the Fiducial run. The parameter  $C_{\text{visc}}$  modulates the limiting value of parameter  $C$  in Eq. 3.35 through the accretion suppression factor of  $C_{\text{visc}}^{-1}(c_s/v_\phi)^3$ , which is usually less than unity. The lower  $C_{\text{visc}}$  results in a higher suppression factor (Rosas-Guevara et al., 2015, Schaye et al., 2015, Crain et al., 2015), which allows BHs to accrete at near Bondi rate, hence faster and earlier growth at  $M_* \simeq 10^9 - 10^{10} M_\odot$  as we will see in Section 4.3.2. The LowCviscLowMseed adopts the BH seed mass of  $M_{\text{seed}} = 10^4 h^{-1} M_\odot$ , 10 times smaller than that used in the other two runs.

The L25N512, L25N256, and L25N128 runs have different mass resolutions and are performed to investigate the dependence on resolution. The size of the simulation box of the L25N256 run is  $25 h^{-1} \text{cMpc}$ , and the number of employed particles is  $2 \times 256^3$ , as the name indicates. The L25N256 run has the same resolution as the Fiducial run (i.e., L50N512). The L25N512 and L25N128 have eight times better and worse mass resolution than the L25N256 run. The same configurations and parameters are employed in the three runs except for the gravitational softening length. In the L25N256 run, we use the same gravitational softening length as the Fiducial run, and we set it to twice as small and as large in the L25N512 and L25N128 runs.

Finally, in the L25N256NoZdepSN run, the stellar IMF is fixed to the Chabrier IMF, and the supernova fraction is set to 0.01, independent of metallicity and redshift. This is different from our fiducial treatment used in L25N256, where the specific energy of Type-II SN is higher for lower metallicity stars as shown in Fig. 3.10 due to metallicity- & redshift-dependent IMF and supernova fraction.

## 3.6 Data Analysis

Simulation data is analyzed by on-the-fly FoF and the SUBFIND group and substructure finder (Springel et al., 2001, 2021). For visualization and further data analysis, we

generate a uniform three-dimensional cartesian mesh covering the entire simulation box with  $1024^3$  voxels, assign particle data, and take projections on the fly. The **cloud-in-cell (CIC)** assignment is used for dark matter and star particles, and the **SPH** kernel weight is used for gas particles. The **SPH** particle data is assigned to the mesh, conserving the total mass, metal mass, and internal energy. For only data analysis purposes, we set a floor in the **SPH** smoothing length at  $(\sqrt{3}/2)L_{\text{voxel}}$ , where  $L_{\text{voxel}}$  is the size of a voxel, so that there are some voxel centers within the smoothing length from each **SPH** particle. We then assign mass of  $m_i W_{ij}(h_i) / \sum_k W_{ik}(h_i)$  to  $j$ -th voxel from  $i$ -th particle, where  $m_i$  and  $h_i$  are the mass and smoothing length of the  $i$ -th particle, and  $W_{ij}(h_i) = W(r_{ij}; h_i)$  is the kernel weight with  $r_{ij}$  being the distance from  $i$ -th particle to the center of  $j$ -th voxel. The metal mass and internal energy are assigned to voxels in the same manner, and the metallicity and temperature of each voxel are calculated using the mass, metal mass, and internal energy of the voxel. This mesh generator module is useful for the post-process analysis of the **IGM** presented in Section 5.1.

Figure 3.11 shows the density projection image of the Fiducial run at  $z = 0$ . The baryonic cosmic web, composed of intermediate-temperature ( $10^{4.5} \text{ K} < T < 10^{5.5} \text{ K}$ ) filaments and high-temperature nodes, is apparent. The rest of the cosmic volume is filled with low-temperature voids. <sup>12</sup>

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<sup>12</sup>The movie is available at <https://www.yurioku.com/research/>

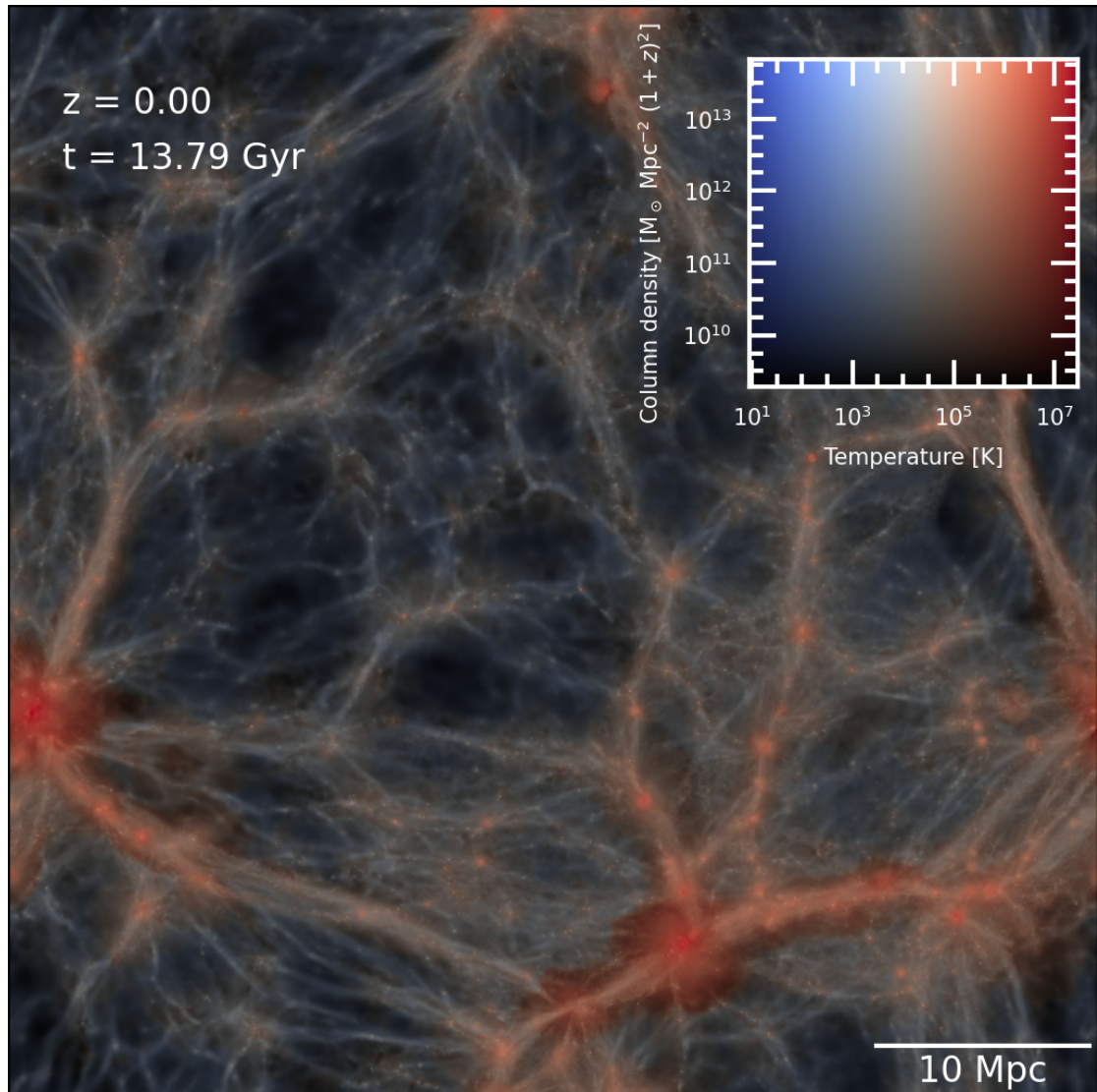


FIGURE 3.11: Projected image through a  $6.25 h^{-1}$  cMpc slice of the Fiducial run. The color and intensity indicate temperature and density, as shown by the color map at the top right corner of the image



# Chapter 4

## General results

In this chapter, we show the general results from the CROCODILE simulation dataset.

### 4.1 Cosmic star formation rate history

Figure 4.1 shows the history of cosmic star formation rate density of CROCODILE simulations. The black dashed line is the best-fitting function to the **UV** and **infrared (IR)** observations at  $0 < z < 8$  by [Madau and Dickinson \(2014\)](#),

$$\psi = 0.015 \frac{(1+z)^{2.7}}{(1+(1+z)/2.9)^{5.6}} \text{M}_{\odot} \text{yr}^{-1} \text{cMpc}^{-3}, \quad (4.1)$$

which peaks at  $z \sim 1.8$ . The Fiducial run generally captures the trend of the observational best-fit function. Three runs with mechanical **SN** feedback suppress star formation at high redshift and have a peak of cosmic **SFR** density at  $z \sim 2$ , and others produce more stars at high redshift and have a peak at  $z \sim 3$ . Comparing Fiducial and SNonly runs, the **SFR** of the Fiducial run is lower at  $z < 2$ , indicating the suppression of star formation by **AGN** feedback. The small bump at  $z = 7$  is due to the reionization, after which the **UV** background radiation ionizes neutral hydrogen and suppresses star formation.

We note that this is not a direct comparison; our simulation results show the actual **SFR** while the observational best-fit function is obtained from **SFR** estimated from **UV** or **IR** luminosity function under an assumption of fixed **IMF**. Our simulation adopts metallicity- and redshift-dependent **IMF**, and further analysis is necessary for direct comparison. At high redshift, dwarf galaxies with low metallicity are the major place of star formation, where the **IMF** is top-heavy and more **UV** photon is produced for a given **SFR**. We expect

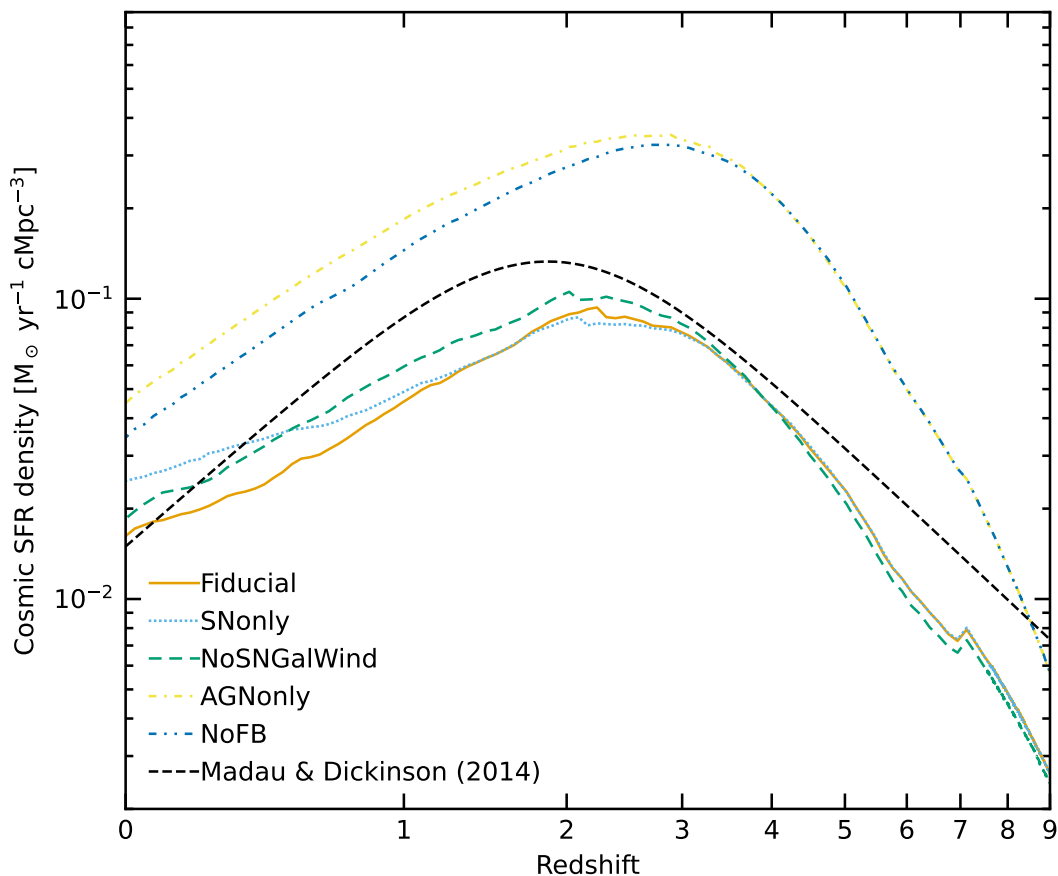


FIGURE 4.1: The history of cosmic star formation rate density of CROCODILE simulation. The black dashed line is the fitting function to **UV** and **IR** observations by [Madau and Dickinson \(2014\)](#).

the discrepancy between the Fiducial simulation and observations to be smaller when they are compared in terms of **UV** luminosity density.

## 4.2 Phase diagram

Figure 4.2 shows the phase diagram of the Fiducial run at  $z = 0$ . The cold and dense gas is the star-forming gas in the interstellar medium in galaxies, and the hot and tenuous gas is the circumgalactic medium heated by virial shock and feedback. The cold and tenuous gas is the intergalactic medium at photoionization equilibrium of **UV** background radiation and Compton cooling off of the cosmic microwave background and has a slope of  $1/1.7$  ([Hui and Gnedin, 1997](#), [McQuinn, 2016](#)).

Unlike some previous cosmological simulations e.g., EAGLE and IllustrisTNG, we did not use an effective **EoS** for unresolved multiphase **ISM**. We instead use the non-thermal

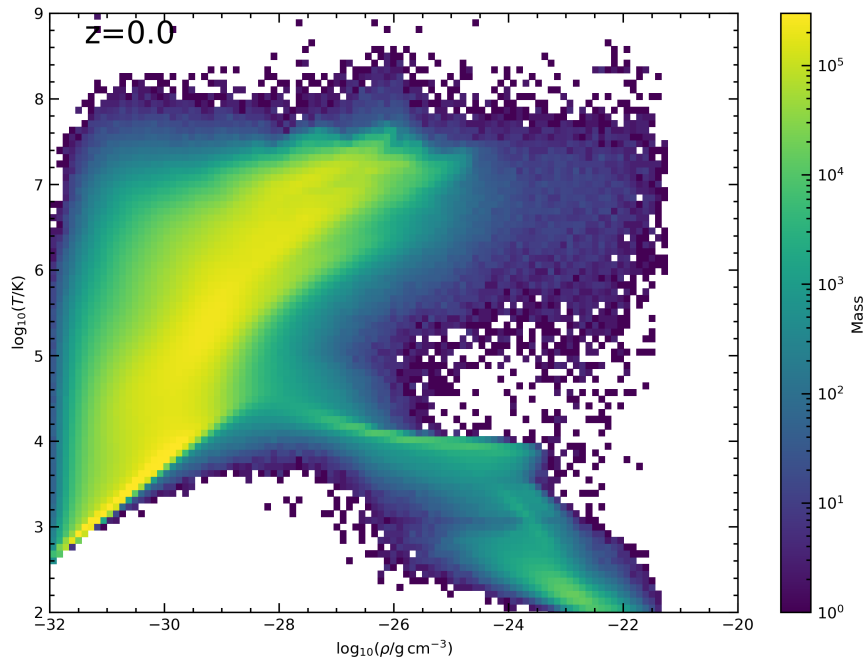


FIGURE 4.2: Phase diagram of the Fiducial run at  $z = 0$ . The color shows the mass in each bin.

pressure floor to track the gas cooling down to 100 K. This treatment enables us to obtain a realistic phase diagram.

### 4.3 Galaxy Statistics

This section compares the statistical properties of galaxies formed in our simulations. In the following subsections, we compare simulations focusing on the feedback model variation, BH model parameters, resolution, and SN feedback energy variation. We examine the stellar mass, SFR, gas-phase metallicity, and the most massive black hole mass in galaxies, identified as subhalos by the SUBFIND algorithm. The stellar mass presented in the following is the mass of stars within twice half-stellar-mass radius; for each collection of stellar particles in a subhalo, we compute the radius of a sphere enclosing half of its mass and then obtain the stellar mass within the twice half-stellar-mass radius. The SFR of a galaxy is the sum of the gas particles' SFR, computed using Eq. 3.31, in the subhalo. The gas-phase metallicity of a galaxy is an SFR-weighted average of the metallicity of gas particles in the subhalo, intended for comparison with observations where metallicity is measured using nebular lines from ionized regions around young stars in star-forming regions. In the following figures, we show various quantities as a function

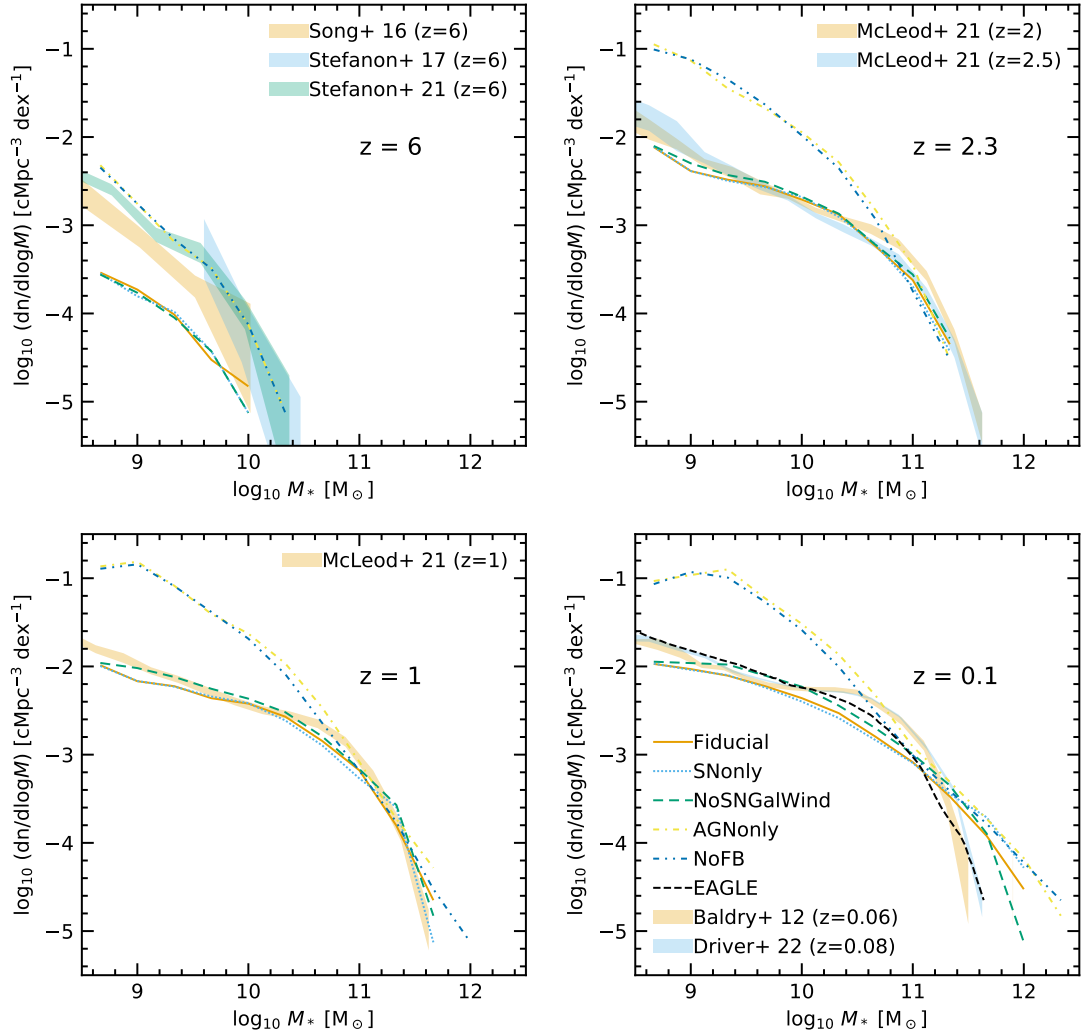


FIGURE 4.3: Galaxy stellar mass function at  $z = 0.1, 1, 2.3, 6$ . The black dashed line in the bottom right panel is for the Ref run of EAGLE simulation (Schaye et al., 2015). The shaded regions are the observational constraints on SMF from Song et al. (2016), Stefanon et al. (2017, 2021) at  $z = 6$ , McLeod et al. (2021) at  $z = 1, 2$ , and  $2.5$ , and Baldry et al. (2012) and Driver et al. (2022) around  $z = 0.1$ .

of galaxy stellar mass above  $M_* = 10^{8.5} M_\odot$  because the mass of each stellar particle is  $9.1 \times 10^6 M_\odot$ .

### 4.3.1 Feedback Model Variation

Figure 4.3 shows the galaxy stellar mass function at  $z = 6, 2.3, 1$ , and  $0.1$ . The shaded regions are the observational constraints on the stellar mass function from Song et al. (2016), Stefanon et al. (2017, 2021) at  $z = 6$ , McLeod et al. (2021) at  $z = 1, 2$ , and  $2.5$ , and Baldry et al. (2012) and Driver et al. (2022) around  $z = 0.1$ .

The Fiducial, SNonly, and NoGalWind runs show suppressed star formation compared to runs without SN mechanical feedback (AGNonly and NoFB) at  $M_* < 10^{11} M_\odot$ , leading to a better consistency with the observation at  $z = 2.3$  and 1. This indicates that the SN mechanical feedback is the dominant feedback source for the low-mass galaxies.

At  $z \sim 6$ , our SN feedback model appears to be a bit too strong, leading to an underprediction of galaxies with  $M_* < 10^{9.5} M_\odot$  despite the good agreement in the star-formation main sequence (top left panel of Figure 4.4). Interestingly, runs without SN mechanical feedback demonstrate a closer agreement with observational data. Moreover, recent observations by the *James Webb Space Telescope (JWST)* have unveiled more numerous massive galaxies at  $z > 7$  than expected from cosmological simulations (Harikane et al., 2023, Bouwens et al., 2023, Finkelstein et al., 2023, Chemerynska et al., 2023, Yung et al., 2024). At  $z \gtrsim 6$ , the discrepancy between our simulation results and observational data becomes more pronounced. Dekel et al. (2023) have introduced the concept of a ‘feedback-free starburst’ scenario. This theory suggests that gas in high- $z$  halo can be efficiently converted into stars with minimal feedback effects, primarily due to the conditions of high density and low metallicity prevalent at these early cosmic times. The closer agreement of the NoFB run with observations lends support to this feedback-free starburst hypothesis. However, it remains uncertain whether this scenario can consistently account for the observed stellar mass function at lower redshifts. This uncertainty points to a potentially critical area of investigation in understanding the evolution of galaxies across different epochs.

At  $z = 0.1$ , the Fiducial run nicely reproduces the low-mass end of the observed stellar mass function. Both our simulations and the EAGLE simulation decrease towards a higher mass end with a slightly steeper slope than the observed exponential cutoff at  $M_* \sim 10^{11.5} M_\odot$ , but capture the cutoff mass range relatively well.

Figure 4.4 shows the star-formation main sequence at  $z = 6, 2.3, 1,$  and  $0.1$ . The points and error bars show the median SFR values and 16th and 84th percentile for each stellar mass bin in our simulations. The shaded regions are the observational constraints from Salmon et al. (2015) at  $z = 6$ , Karim et al. (2011) at  $z = 2.25, 1.1, 0.9,$  and  $0.3$ , Tomczak et al. (2016) at  $z = 2.25, 1.125,$  and  $0.875$ , and Whitaker et al. (2012) at  $z = 0 - 0.5$ . We display only the star-forming galaxies, selected by a criterion  $\text{specific star formation rate (sSFR)} > 10^{-2} \text{ Gyr}^{-1}$ , because the observed data are also for star-forming galaxies.

At  $z = 6$ , the simulations show similar star-formation main sequences with each other. The runs without stellar feedback show lower SFR than the observed star-formation main sequences for a given stellar mass at lower redshifts. This indicates that stellar feedback is necessary to sustain star formation activity by driving interstellar turbulence and galactic wind to delay the depletion of gas in the dark matter halo and produce

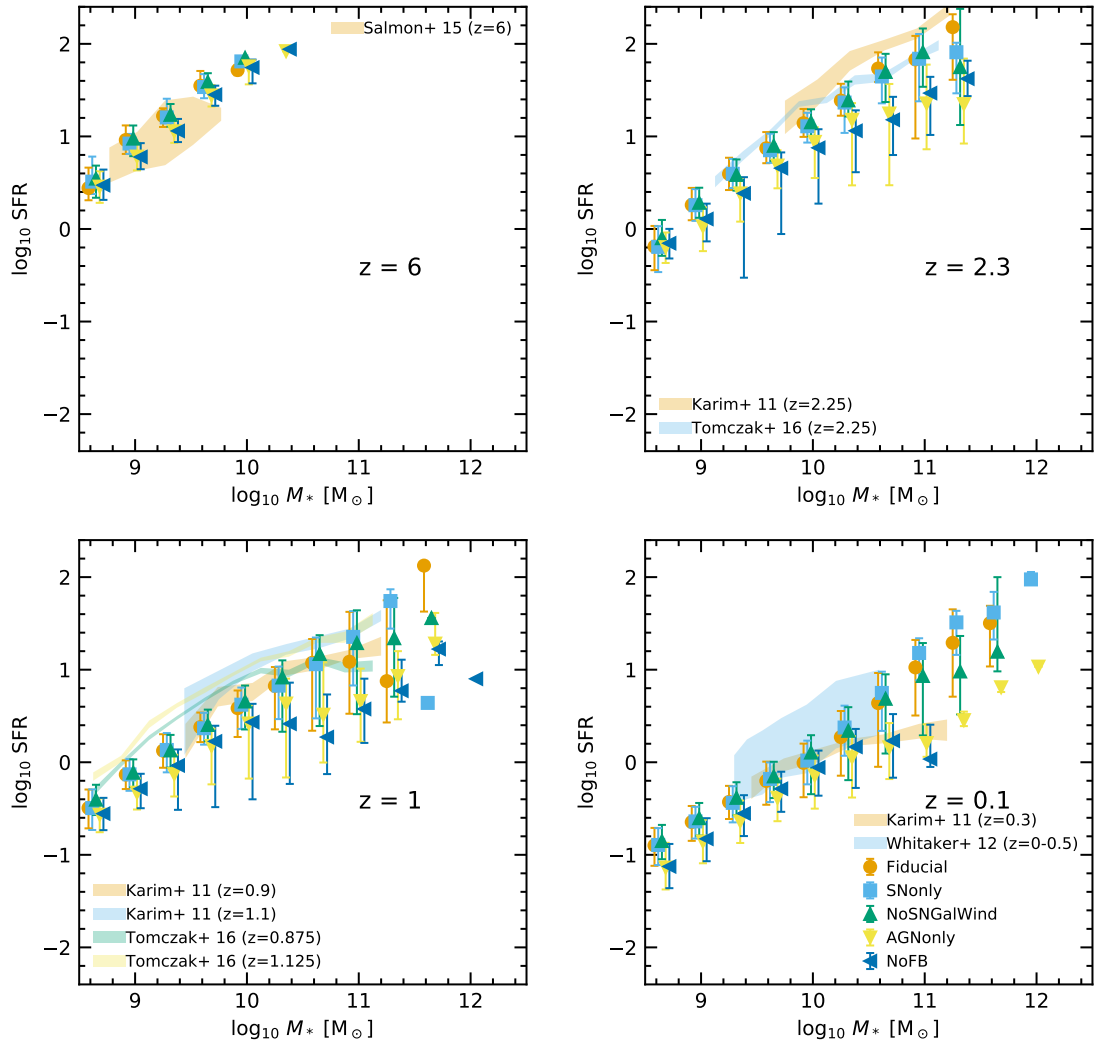


FIGURE 4.4: Redshift evolution of the star formation main sequence of the simulated galaxies with  $s\text{SFR} > 10^{-2} \text{Gyr}^{-1}$ . The points and error bars show the median SFR values and 16th and 84th percentile for each stellar mass bin in our simulations. The shaded regions are the observational constraints from Salmon et al. (2015) at  $z = 6$ , Karim et al. (2011) at  $z = 2.25, 1.1, 0.9$ , and  $0.3$ , Tomczak et al. (2016) at  $z = 2.25, 1.125$ , and  $0.875$ , and Whitaker et al. (2012) at  $z = 0 - 0.5$ .

star-forming galaxies at  $z = 0$ . Runs with stellar feedback show a nice agreement with observations.

Figure 4.5 shows the mass-metallicity relations at  $z = 6, 2.3, 1$ , and  $0.1$ . The metallicity of simulated galaxies is computed with the total metal mass in the gaseous phase. The points and error bars show the median metallicity values and 16th and 84th percentile for each stellar mass bin in our simulations. The shaded regions are observational constraints from Sanders et al. (2021), Strom et al. (2022) at  $z = 2.3$  and Andrews and Martini (2013), Tremonti et al. (2004) at  $z = 0.1$ . The galaxies in the runs without stellar feedback have higher metallicity at  $M_* \lesssim 10^9 M_\odot$ , which indicates that stellar feedback expels metals from galaxies.

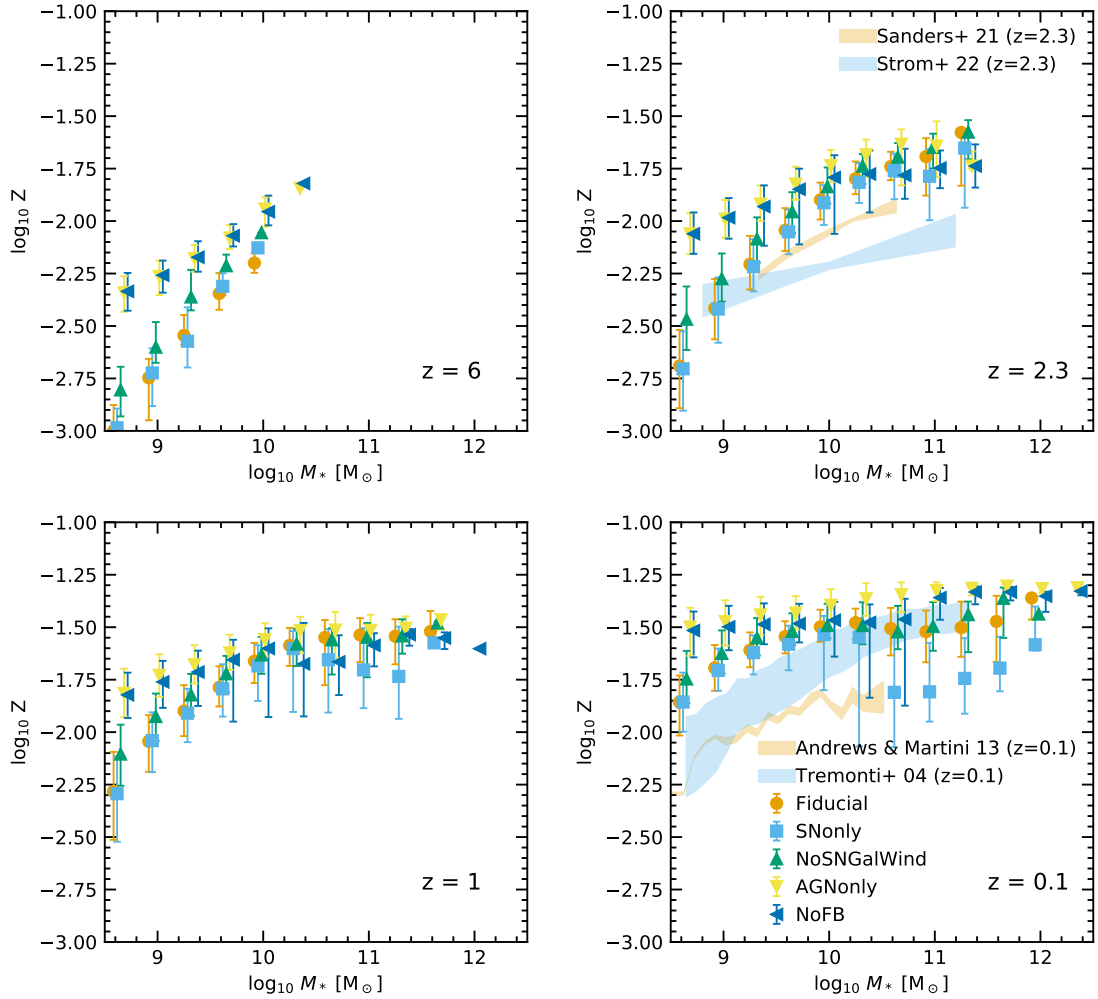


FIGURE 4.5: Redshift evolution of the mass–metallicity relation. The points and error bars show the median metallicity values and 16th and 84th percentile for each stellar mass bin in our simulations. The shaded regions are observational constraints from Sanders et al. (2021), Strom et al. (2022) at  $z = 2.3$  and Andrews and Martini (2013), Tremonti et al. (2004) at  $z = 0.1$ .

One can see that the NoSNGalWind run has slightly higher metallicity than the Fiducial run. This is because of the metal reduction by the galactic wind in the Fiducial run. The typical metal loading factor of our galactic wind model is 0.3, corresponding to 0.15 dex, which can explain the difference between the NoSNGalWind and Fiducial run. The difference among the models is small at  $M_* \gtrsim 10^{10} M_\odot$  because the feedback effect is weaker at the massive end, where the gravitational binding energy is stronger.

The metallicity of simulated galaxies of  $M_* \sim 10^{10} M_\odot$  is 0.2 dex higher than the mass–metallicity relation by Sanders et al. (2021) at  $z = 2.2$ , and 0.4 dex higher than the mass–metallicity relation by Andrews and Martini (2013) at  $z = 0.1$ . This can be due to either inefficient metal ejection by the galactic wind or insufficient gas mass in the

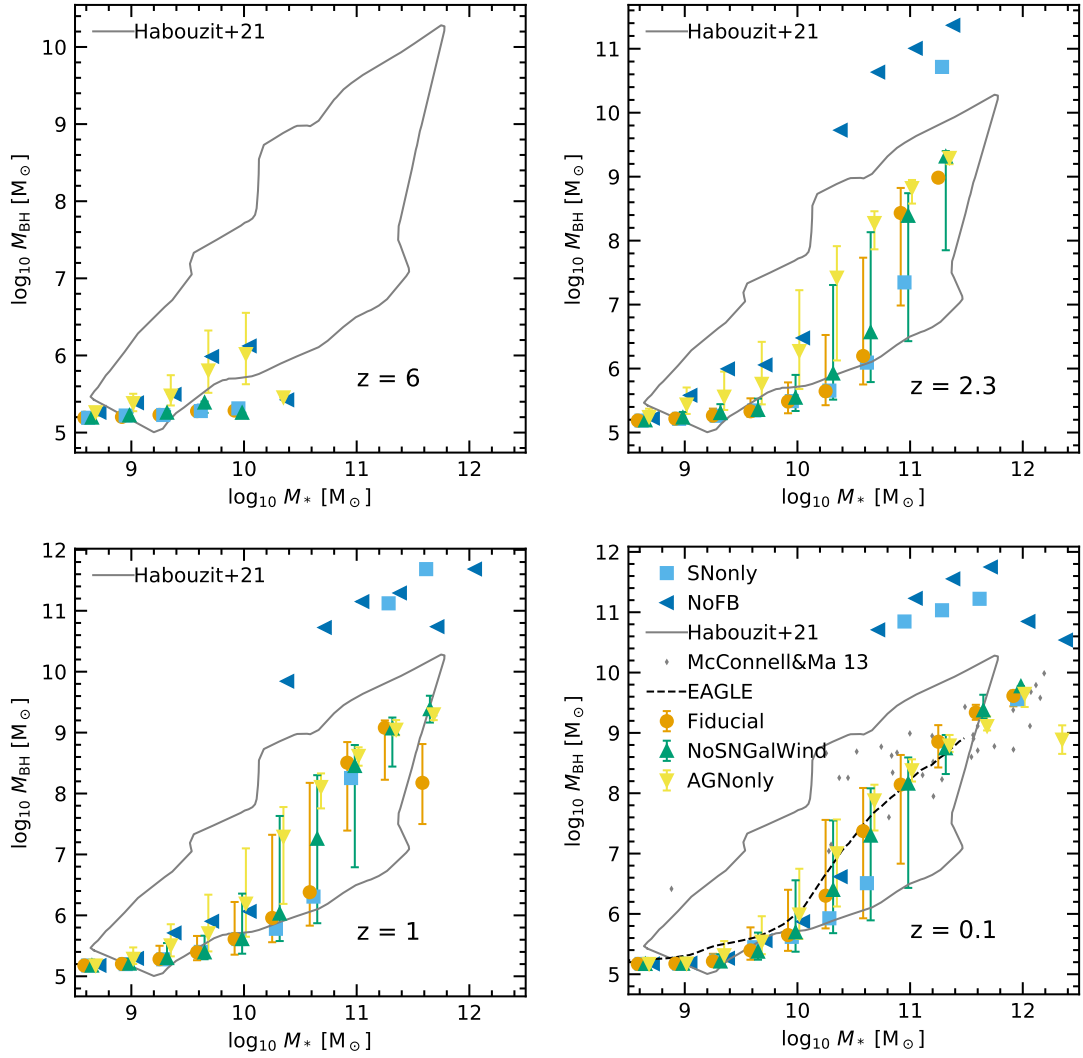


FIGURE 4.6: Redshift evolution of the BH mass–stellar mass relation. The points and error bars show the median value and 16th and 84th percentile of the most massive BH mass in the galaxies in each stellar mass bin. For the SNOnly and NoFB runs, we omit the error bars for clarity. The black dashed line shows the median of the EAGLE Ref run. The region indicated by the gray solid line covers the majority of local observational constraints compiled by Habouzit et al. (2021). The gray diamonds are observational data by McConnell and Ma (2013).

simulated galaxies at low redshift. We will investigate the galactic outflow properties in our simulations by comparing them with recent IFU data in our future work.

Figure 4.6 shows the BH mass as a function of galaxy total stellar mass. The points and error bars show the median value and 16th and 84th percentile of the most massive BH mass in the galaxies in each stellar mass bin. The region indicated by the black solid line is the observational constraint at  $z = 0$  compiled by Habouzit et al. (2021). The gray diamonds are observational data by McConnell and Ma (2013).

The runs with AGN feedback have lower BH masses at  $z \lesssim 3$  because the gas around



BHs is blown away by the AGN feedback. In the runs with AGN feedback, the  $M_{\text{BH}}-M_*$  relation is consistent with observations, and the medians are almost at the lower edge of the observationally constrained region at  $10^9 M_\odot < M_* < 10^{10.5} M_\odot$ . This behavior is sensitive to the choice of subgrid parameters of black holes, as demonstrated in Section 4.3.2.

The AGNonly run also shows higher BH mass than the Fiducial run, indicating that the stellar feedback inhibits the gas accretion onto BHs and suppresses BH growth. The difference between the AGNonly and Fiducial run is noticeable at  $M_* \sim 10^9 M_\odot - 10^{11} M_\odot$  at  $z > 1$ , where stellar feedback is considered to be playing the major role in regulating the galaxy formation, while the results from the two runs converge at the massive end.

Figure 4.7 shows the halo baryon fraction  $f_{\text{baryon}}$  normalized by the cosmic mean baryon fraction,  $\Omega_{\text{baryon}}/\Omega_{\text{matter}}$ , versus halo mass at  $z = 0$ . For the Fiducial run, the  $f_{\text{baryon}}$  increases monotonically as the halo mass increases. The baryon mass is reduced for low-mass halos due to SN feedback. Comparing the Fiducial and NoSNGalWind runs, there are only minor differences, which indicate that the hot galactic wind plays a minor role and the kinetic feedback is dominant in ejecting baryons out from halos. Comparing the Fiducial and SNonly runs, the SNonly run has higher  $f_{\text{baryon}}$  at  $M_h > 10^{12} M_\odot$ , indicating the AGN impact of ejecting gas from halos. The  $f_{\text{baryon}}$  of the Fiducial run is consistent with the observational estimate by Das et al. (2023) while EAGLE and TNG underpredict  $f_{\text{baryon}}$ . These simulations adopt SN and AGN feedback models that are too strong in driving the galactic outflows to suppress star formation by removing gas in halos. The momentum-based kinetic SN feedback model in our simulation is moderate in driving the galactic outflow for galaxies with  $M_h \sim 10^{12.5} M_\odot$ , and the baryons are kept in CGM.

### 4.3.2 BH Parameter Variation

Figure 4.8 again shows the  $M_{\text{BH}}-M_*$  relation, stellar mass function, and star-formation main sequence, but for the runs with different BH parameters, Fiducial, LowCvisc, and LowCviscLowMseed, at  $z = 2.3$  and 0.1.

Panels A and B show the  $M_{\text{BH}}-M_*$  relation. The  $C_{\text{visc}}$  controls the onset of the BH growth, and the BH mass starts to increase at  $M_* \sim 10^9 M_\odot$  for runs with low  $C_{\text{visc}}$  ( $= 2\pi$ ) and at  $10^{10} M_\odot$  for the runs with our default  $C_{\text{visc}}$  ( $= 200\pi$ ) at  $z = 0.1$ . The simulation data points of the Fiducial run are around the bottom of the region indicated by Habouzit et al. (2021), while those by the LowCvisc run are around the top of the region. At  $M_* > 10^{11} M_\odot$ , it is interesting to see that the  $M_{\text{BH}}-M_*$  relation for all three simulations agree due to the self-regulated growth of BH.

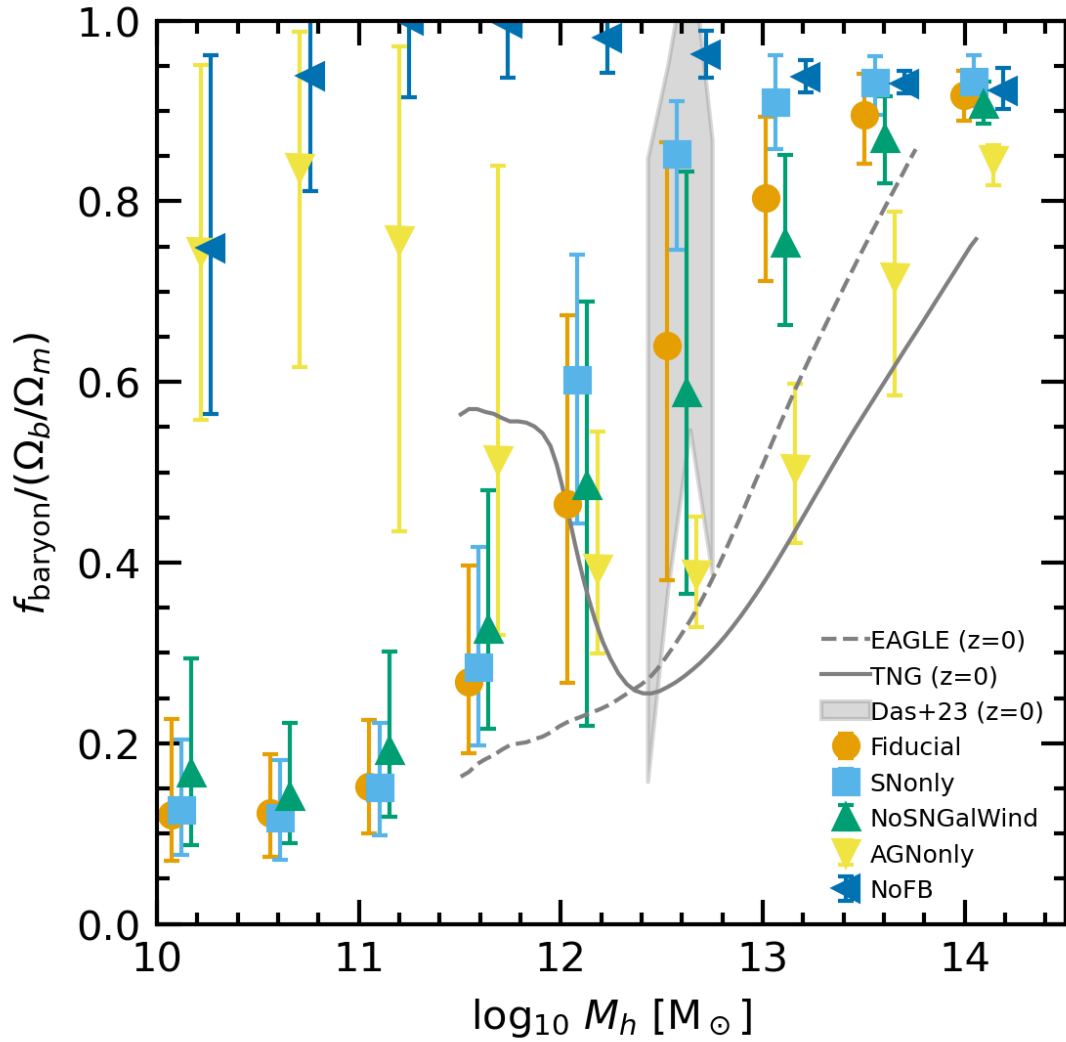


FIGURE 4.7: Halo baryon fraction,  $f_{\text{baryon}}$ , normalized by the cosmic mean baryon fraction,  $\Omega_{\text{baryon}}/\Omega_{\text{matter}}$ , vs. halo mass at  $z = 0$ . The points and error bars show the median value and 16th and 84th percentile of the mass of baryons (star and gas) in the halos in each halo mass bin. The gray dashed and solid lines are the median lines of the EAGLE-Ref and TNG-100 simulations taken from Davies et al. (2020). The gray-shaded region is estimated baryon fraction by the observation of thermal Sunyaev–Zel’dovich effect (Das et al., 2023).

Panels C and D show the stellar mass function. By comparing with panels A and B, one can see that the stellar mass function rapidly declines at the same mass scale where the BH mass rapidly increases. The stellar mass function of the LowCvisc run is lower than other runs at  $M_* > 10^{9.5} M_{\odot}$  due to the early growth of BHs and subsequent AGN feedback. In the LowCviscLowMseed run, the BH growth is delayed due to the smaller BH seed mass, as seen in the upper panels, and it shows a similar stellar mass function to the Fiducial run.

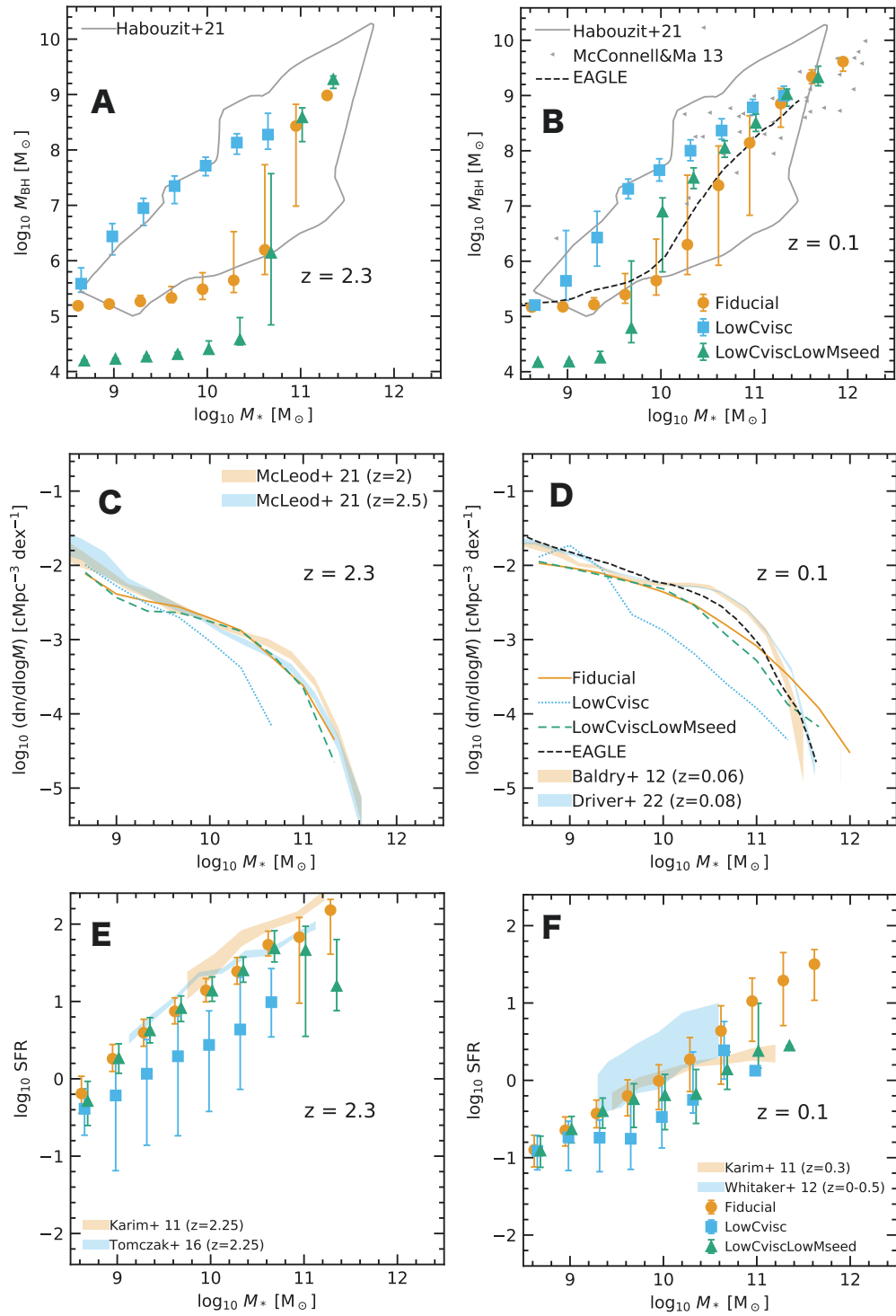


FIGURE 4.8: Comparing the  $M_{\text{BH}}-M_*$  relation, stellar mass function, and star-formation main sequence for the runs with different BH parameters, Fiducial, LowCvisc, and LowCviscLowMseed, at  $z = 2.3$  and 0.1.

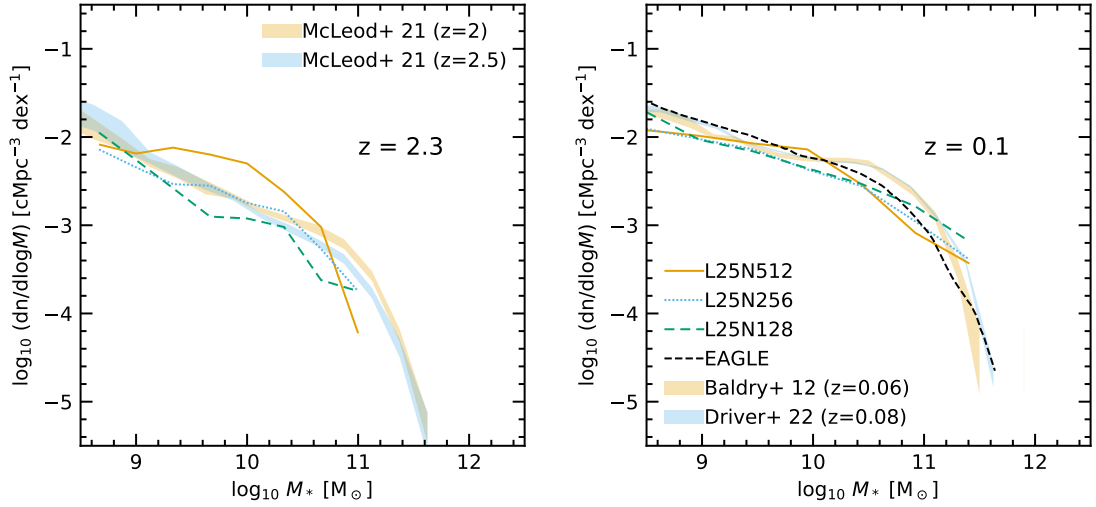


FIGURE 4.9: Galaxy stellar mass functions of the runs with different resolutions, L25N512, L25N256, and L25N128 at  $z = 2.3$  and  $0.1$ .

We can also see the impact of AGN feedback on the star formation activity in the star-formation main sequence shown in panels E and F. The slope of the star-formation main sequence becomes shallower at the same stellar mass where the BH begins to grow rapidly.

### 4.3.3 Resolution Variation

Figure 4.9 shows the stellar mass functions of the runs with different resolutions, L25N512, L25N256, and L25N128. We used the same subgrid and numerical parameters except for the gravitational softening length in these runs. They roughly converge and agree with the observed stellar mass function. The stellar mass function slightly increases with increasing resolution at  $z = 2.3$ . This is attributed to the density dependence of the star formation efficiency; higher resolution simulations can resolve higher density star-forming clouds, which have shorter star formation timescales.

### 4.3.4 SN Feedback Energy Yield Variation

Figure 4.10 shows the stellar mass function of the L25N256 and L25N256NoZdepSN runs at  $z = 2.2$  and  $0.1$ . In the L25N256 run, we used the metallicity- and redshift-dependent SN energy yield model, which has increasing specific SN energy towards lower SN progenitor metallicity as shown in Fig. 3.10. In the L25N256NoZdepSN run, the specific SN energy is fixed to  $\zeta_{\text{SN}} \simeq 6 \times 10^{48} \text{ erg } M_{\odot}^{-1}$ . One can see that the L25N256NoZdepSN run completely overpredicts the number of low-mass galaxies. This indicates that the SN

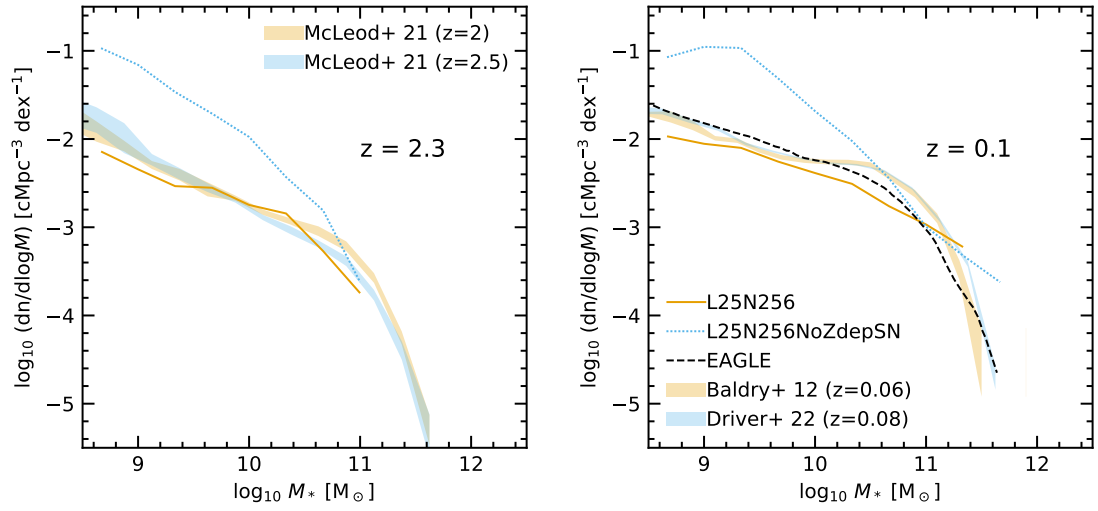


FIGURE 4.10: Galaxy stellar mass function of the L25N256 and L25N256NoZdepSN runs at  $z = 2.3$  and  $0.1$ .

feedback with the above constant  $\zeta_{\text{SN}}$  is not strong enough to suppress star formation and reproduce the observed stellar mass function.

## Chapter 5

# Metal enrichment in the IGM

In this chapter, we analyze the distribution of metals in the IGM and show the impact of SN and AGN feedback by comparing simulations with varying feedback models.

### 5.1 Visual inspection

Figure 5.1 shows the density-weighted projections of metallicity at  $z = 2.3$  and 0.<sup>1</sup> Metals are distributed following the large-scale structure with visible differences due to feedback settings.

The effect of explicit modeling of SN-driven galactic wind can be seen in the comparison between the Fiducial and NoSNGalWind runs. The SN-driven metal-rich galactic wind spread metals on  $\lesssim 100$  kpc scale in the Fiducial run more uniformly than in the NoSNGalWind run.

Comparing the Fiducial and SNonly runs clarifies the role of AGN outflow in the chemical enrichment of the IGM. The high-metallicity bubbles of a size of a few Mpc are formed by AGN feedback in the Fiducial run at  $z = 0$ , but they are not visible in the SNonly run. We modeled AGN feedback as an isotropic thermal energy injection, however the hot bubble cannot expand into the direction of the galactic disk. Therefore, the metal-rich AGN outflow naturally expands in the bipolar direction above and below the galactic disk.

In the NoFB case, metals produced in galaxies remain there, and the distribution of metals follows that of galaxies at  $z = 2.3$ . It is interesting to see that metals are somewhat spread at  $z = 0$ , which is likely due to the hydrodynamical effect in galaxy

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<sup>1</sup>The movie is available at <https://www.yurioku.com/research>



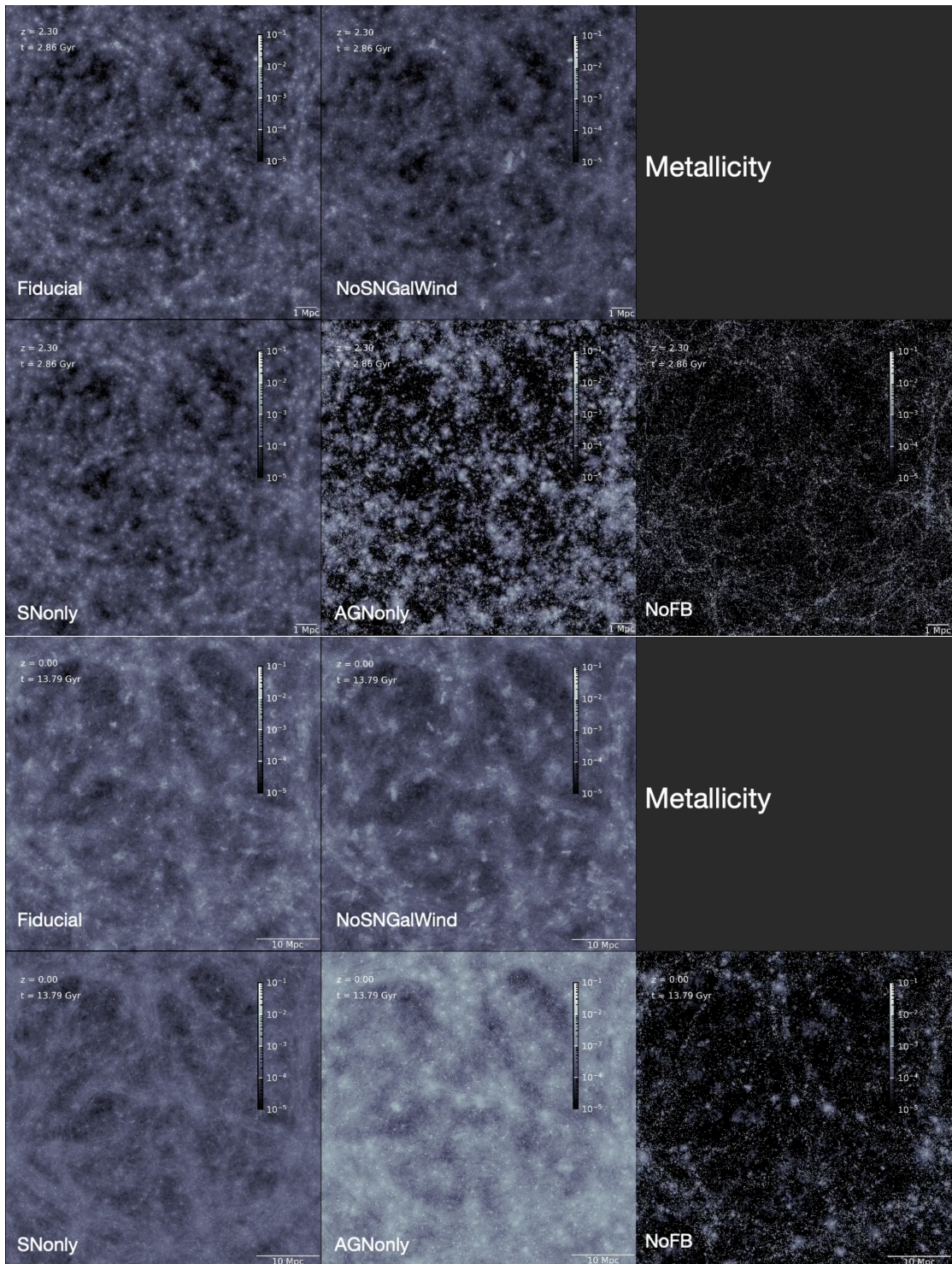


FIGURE 5.1: The density-weighted projection of metallicity at  $z = 2.3$  (top two rows) and 0 (bottom two rows).

mergers, galaxy collision, and ram pressure stripping. In other runs, feedback spread metals out to CGM and IGM.

The AGNonly run shows a distinctively higher metallicity than other runs at  $z = 0$  because star formation efficiency is higher due to the lack of SN feedback, more metals are produced by stars, and AGN feedback spreads metals to IGM. The AGN feedback begins to have an effect at  $z \sim 2$ , and the metal enrichment in the void region is delayed from other runs with SN feedback at  $z = 2.3$ .

## 5.2 Overdensity–metallicity relation

Figure 5.2 and 5.3 show the IGM metallicity as a function of the dark matter and gas overdensity. The black dashed line shows the best-fit line for the observational estimate of the metallicity–overdensity relation from the carbon abundance in the Ly $\alpha$  forest (Schaye et al., 2003),  $[C/H] = -3.47 + 0.08(z - 3) + 0.65(\log \delta - 0.5)$ , where  $\delta$  is the baryon overdensity and  $z$  is the redshift. We generate a uniform cartesian mesh with  $512^3$  voxels and compute dark matter density, gas density, and gas metallicity as described in Section 3.6. The Fiducial, NoSNGalWind, and SNonly run show similar results, indicating that the SN mechanical feedback is the dominant mechanism to enrich the IGM among other feedback processes. The slope of these runs shows a good agreement with the observation, which is encouraging. Compared to the Fiducial run, the AGNonly run shows higher metallicity at higher overdensity at  $z = 2.3$ , because more metals are produced and confined in galaxies due to the absence of stellar feedback. Below  $z \sim 2$ , the AGN feedback kicks in and spreads metals to IGM and increases metallicity at low overdensity regions, which cannot be seen in the NoFB run.

## 5.3 Metal density power spectrum

Figure 5.4 shows the power spectra of the metal density field at  $z = 2.3$  and 0, which allows us to examine the different effects of feedback models statistically. We use the cosmological analysis toolkit NBODYKIT<sup>2</sup> (Hand et al., 2018) to compute the power spectra on  $1536^3$  mesh, and the upper limit of the abscissa (wavenumber) is cut off at  $k = k_{\text{Nyq}}/4$ , where  $k_{\text{Nyq}} = \pi N_{\text{mesh}}/L_{\text{box}}$  is the Nyquist frequency.

At  $z = 2.3$ , the Fiducial run has lower power at  $k > 3 h \text{cMpc}^{-1}$  compared to the NoSNGalWind run, indicating that the galactic wind transport metals and smooth out the metal distribution in CGM. The effect of AGN can be seen around  $k \sim 3 h \text{cMpc}^{-1}$

<sup>2</sup>The code’s website is <https://nbodykit.readthedocs.io/en/latest/>



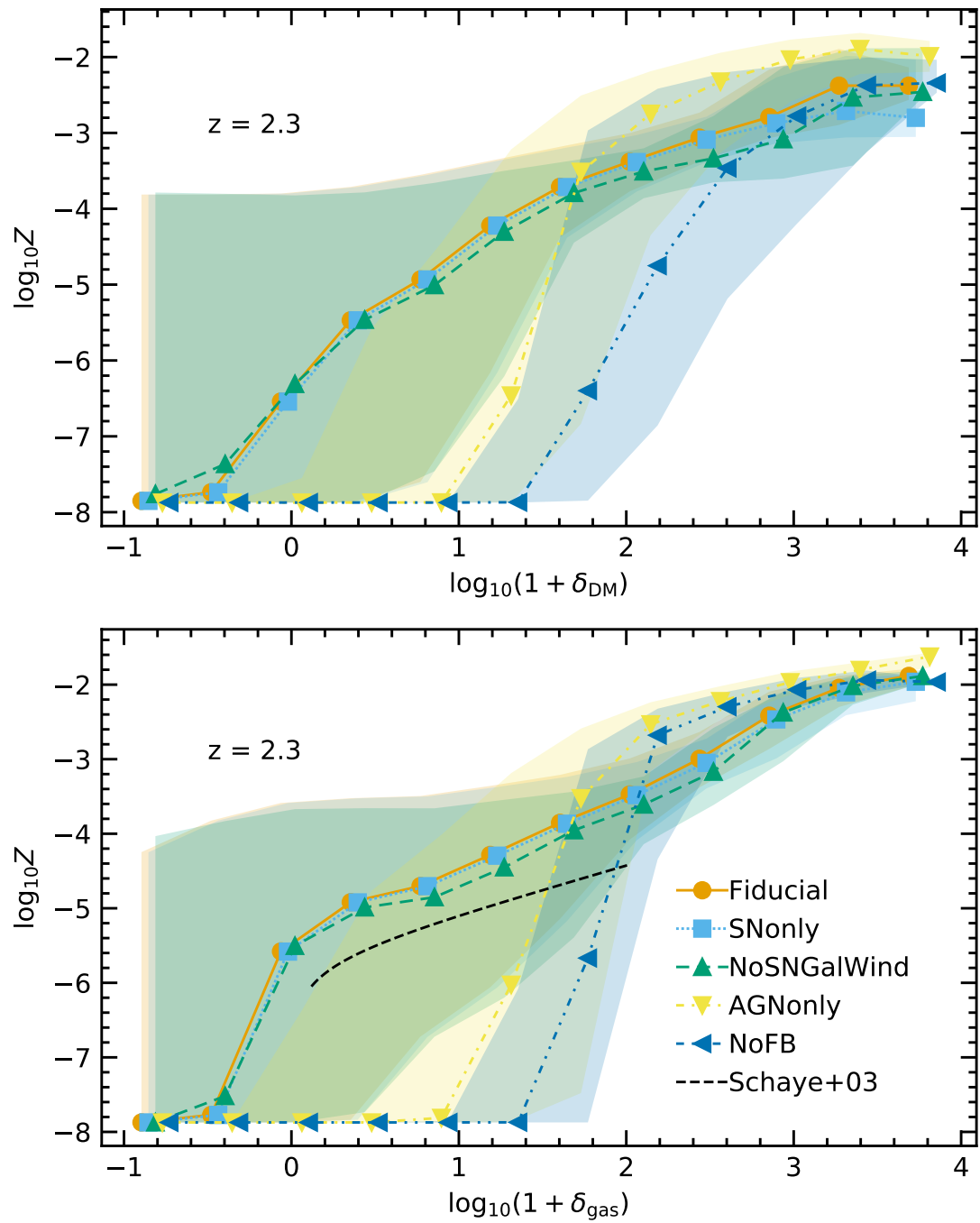
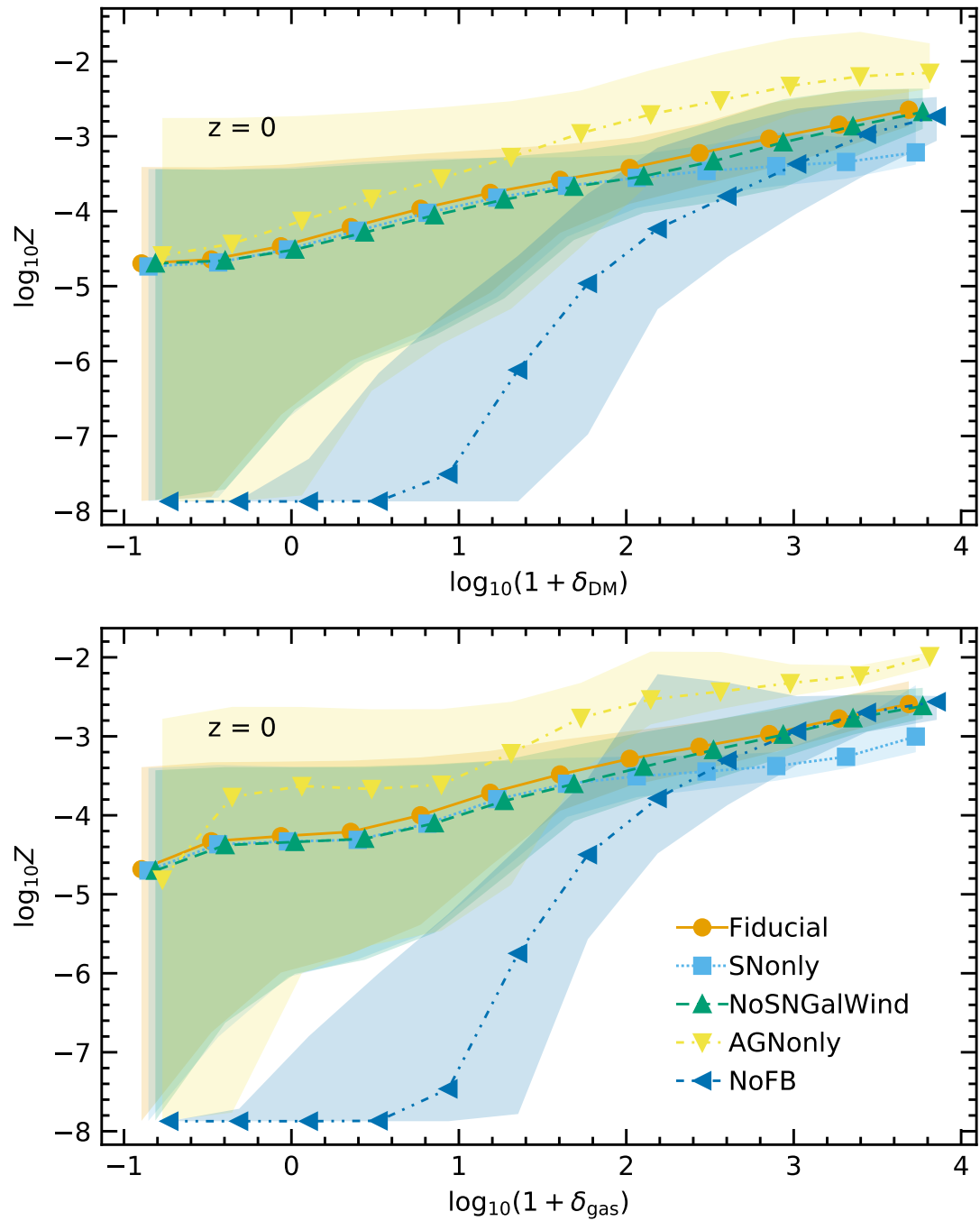


FIGURE 5.2: Metallicity as a function of dark matter (top) and gas (bottom) overdensity at  $z = 2.3$ . The points and shades indicate the median value and 16th and 84th percentile of the metallicity. The black dashed line shows the observational estimate of the metallicity–overdensity relation using Ly $\alpha$  forest (Schaye et al., 2003).

FIGURE 5.3: Same as Fig. 5.2 but at  $z = 0$ .

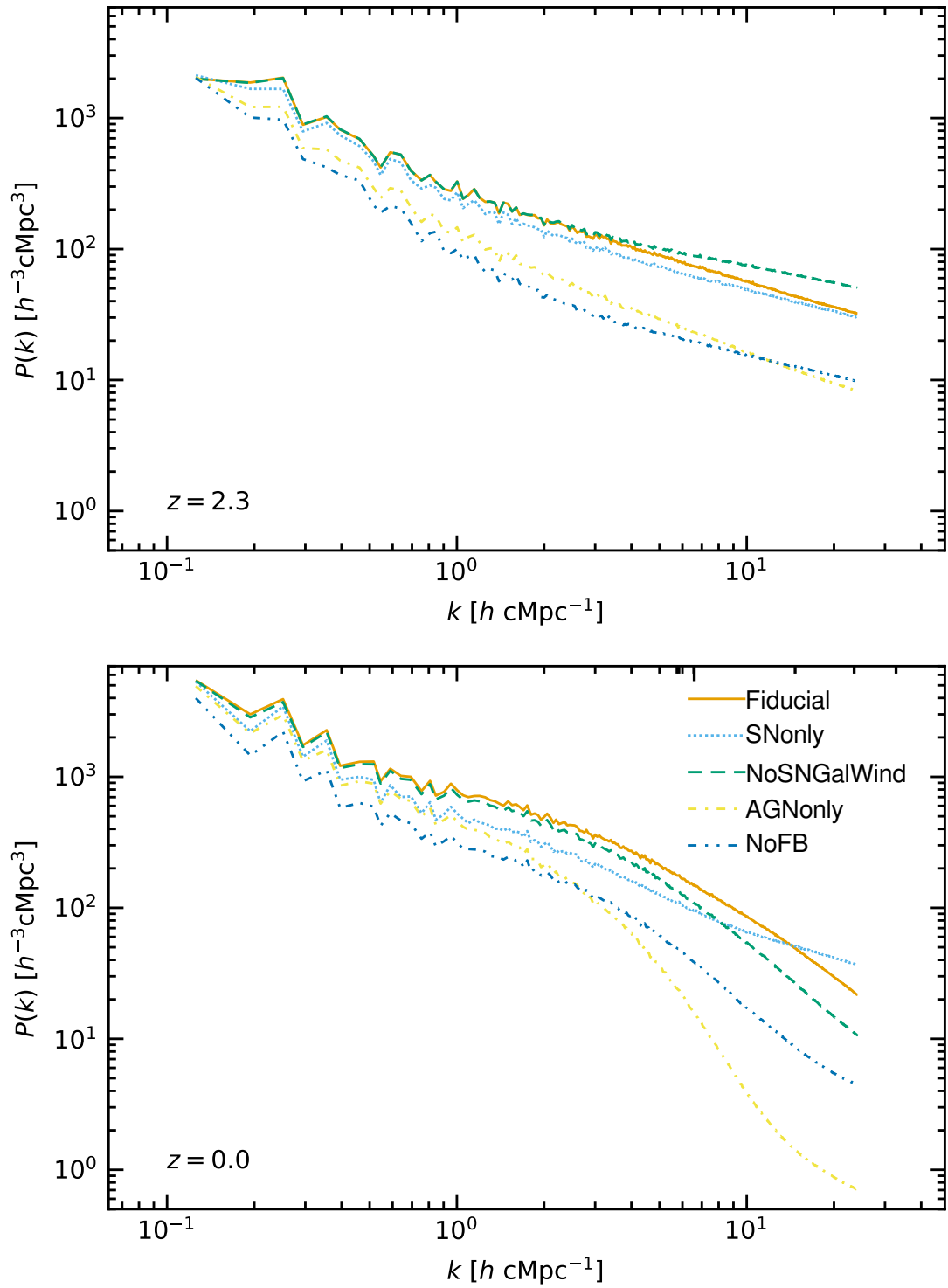


FIGURE 5.4: Power spectra of the metal density field at  $z = 2.3$  (top) and 0 (bottom). The upper limit of the abscissa (wavenumber) is cut off at  $k = k_{\text{Nyq}}/4$ , where  $k_{\text{Nyq}}$  is the Nyquist frequency.

as a slight enhancement of the power in the Fiducial run relative to the SOnly run due to the AGN-driven outflows entraining metals out to a few Mpc scale.

At  $z = 2.3$ , metals are more diffused in the Fiducial run compared to the NoSNGalWind run, hence lower power on small scales. On the other hand, at  $z = 0$ , the effect of the AGN outflow is stronger, and metals are more diffused in the NoSNGalWind run than in the Fiducial run, leading to a lower power on small scale in the NoSNGalWind run.

## Chapter 6

# Summary and future prospects

In this thesis, we develop a physically-motivated [supernova \(SN\)](#) feedback model based on high-resolution simulations. We then introduce a new suite of cosmological hydrodynamical simulations CROCODILE, powered by the GADGET4-OSAKA code utilizing the supernova feedback model. Our simulations also feature an updated chemical evolution model, which integrates a metallicity- and redshift-dependent [initial mass function \(IMF\)](#) based on the star cluster formation simulation by [Chon et al. \(2022\)](#), along with a metallicity-dependent [hypernova \(HN\)](#) fraction. This refinement significantly enhances the specific [SN](#) energy of low-metallicity stars by more than an order of magnitude (Fig. 3.10). Furthermore, we implement an [active galactic nucleus \(AGN\)](#) feedback model, following the methodologies outlined in [Rosas-Guevara et al. \(2015\)](#), [Schaye et al. \(2015\)](#), [Crain et al. \(2015\)](#). This model approaches the [AGN](#) feedback as a stochastic thermal energy injection process.

The main points of this thesis can be summarized as follows:

- Our [SN](#) feedback model incorporates both kinetic and thermal feedback in the form of momentum injection and stochastic thermal energy injection. In isolated galaxy simulations, we have demonstrated that the kinetic feedback suppresses star formation by sustaining the galactic disk against gravitational collapse, and the thermal feedback drives galactic scale outflow transporting metals to [circumgalactic medium \(CGM\)](#) and [intergalactic medium \(IGM\)](#).
- Our simulations reproduce the observed stellar mass function across a broad spectrum of galaxy stellar masses, ranging from  $10^8 M_\odot$  to  $10^{11} M_\odot$  as illustrated in Figure 4.3. Notably, at  $z \lesssim 3$ , our [SN](#) feedback model, incorporating a top-heavy [IMF](#), effectively suppresses the formation of low-mass galaxies at  $M_* < 10^{10.5} M_\odot$ . At  $z \sim 0.1$ , [AGN](#) feedback plays a crucial role in reducing the number of massive

galaxies with  $M_* \gtrsim 10^{11.8} M_\odot$  (bottom right panel of Figure 4.3). We anticipate that the influence of AGN feedback will be even more pronounced at the higher-mass end of the stellar mass function in a larger cosmological box of 100 Mpc, which we will perform in the near future.

- Our simulations that incorporate a metallicity- and redshift-dependent IMF (including HN contributions) can reproduce the stellar mass function at  $z \lesssim 2$  relatively well, as shown in Figure 4.10. In stark contrast, the run without this IMF treatment (NoZdepSN run) significantly overpredicts the stellar mass function.
- Our simulations generally agree with the observed star formation main sequence across all redshifts, except for the runs without SN feedback (AGNonly and NoFB runs) as depicted in Figure 4.4. The latter two runs significantly overestimate the stellar mass function and mass–metallicity relation, while simultaneously underestimating the star formation main sequence and IGM metallicity. This discrepancy underscores the critical role of SN feedback in cosmological galaxy evolution.
- Our super massive black hole result at  $z = 0.1$  show a general agreement with the EAGLE Ref run within the mass range of  $M_* = 10^8 - 10^{12} M_\odot$  and  $M_{\text{BH}} = 10^5 - 10^{10} M_\odot$  (Fig. 4.6). With a low  $C_{\text{visc}}$  parameter, the mass accretion onto BH in the LowCvisc run is enhanced relative to the Fiducial run, leading to an overestimation of  $M_{\text{BH}}$  and a corresponding underestimation of both the stellar mass function and star formation main sequence (Fig. 4.8). Furthermore, the runs without AGN feedback (SNonly and NoFB runs) consistently overpredict the  $M_{\text{BH}}$ .
- We find that the SN feedback is the dominant mechanism to transport metals into the IGM (Figure 5.2 and 5.3). In addition, the AGN feedback generates bipolar, metal-rich outflow (Fiducial and NoSNGalWind panels of Fig. 5.1), effectively enriching the CGM and extending into the IGM up to a few Mpc scales, as observed in the power spectrum of metal distribution with scales  $k < 10 h \text{ Mpc}^{-1}$  (right panel of Fig. 5.4).

In this thesis, we primarily focused on the broad distributions of metals as functions of overdensities and spatial scales. Given that our simulation tracks multiple chemical species, we are well-positioned to extend our analysis to more detailed ionization calculations for individual elements. This will enable us to conduct comparative studies with a variety of metal absorption lines observed in quasar spectra. Additionally, our simulation incorporates sophisticated models for the formation and destruction of dust (Aoyama et al., 2017, Romano et al., 2022a), which allows us to investigate dust distribution within galaxies, CGM, and IGM in the future. By conducting cross-correlation

studies between galaxies, H I, dust, and metals, we anticipate gaining a more comprehensive understanding of galaxy evolution and the dynamics of the baryonic universe.

Future observations of IGM tomography, line intensity mapping, and X-ray mapping, as well as sensitive observation of Ly $\alpha$  and H $\alpha$  halo, will reveal the baryon distribution in the local and distant universe and revolutionize the understanding of structure formation. The rich observational data will first clarify the matter distribution around galaxy clusters, where we expect bright emissions of intercluster medium.

The formation, growth, and feedback of supermassive black holes will remain a central challenge in structure formation for the next decades. The development of physically-motivated black hole models is a central task in cosmological simulation, which we could not complete in this work. The range of the spatial and temporal scale they involve is much wider than that of supernova feedback, and a lot of effort is still necessary. Simulations are expanding the scale they treat, as highlighted by the recent work by Hopkins et al. (2023a), which solves the accretion disk of the central black hole within the realistic cosmological simulation. The continuous effort in this line, along with larger-box cosmological simulation comparable to observational volume, would be the two major approaches in numerical cosmology.

The usage of artificial intelligence (AI) and machine learning (ML) is promising in treating big data from observations and simulations. With the help of social requirements in the development of AI, the study of AI will keep accelerating, and the knowledge will be imported into astronomical research. I expect the AI to learn the behavior of matter and substitute numerical simulation for the current position, but direct simulations will remain a tool for making an ab initio prediction of the structure formation of the universe.

# Appendix A

## Evolution of a superbubble in idealized ISM

In this appendix, we describe the details of the simulation, as well as the basic analytic theory of superbubble evolution. The content in this appendix is a part of my master's thesis work.

### A.1 Analytic theory

When multiple [SN](#) explosions occur clustered in space and time in stellar clusters, superbubbles are formed with the shell-formation time being a critical timescale for their growth. In [Section A.1.1](#), we analytically calculate the shell-formation time and investigate its dependence on metallicity.

#### A.1.1 Shell-formation time

We first consider the shell-formation time of an [SN](#) remnant formed by a single [SN](#) and extend it to the case of a superbubble formed by multiple [SNe](#).

##### A.1.1.1 Single SN

After [SN](#) explosion occurs, heated gas adiabatically expands and forms an [SN](#) remnant. The adiabatic phase is called the Sedov–Taylor phase, during which the [SN](#) remnant time evolution is described by Sedov–Taylor solutions. When the cooling effect is no



longer negligible, the SN remnant can no longer be considered adiabatic, terminating the Sedov–Taylor phase.

SN remnant cooling is most effective at the shock front, where its density is its highest. The cooling time immediately after the shock wave is estimated to be

$$t_c = \frac{e}{de/dt} = \frac{n_t k_B T_{\text{ST}}}{(\gamma + 1) n_H n_e \Lambda(T_{\text{ST}})} = \frac{2.3}{1.2} \frac{k_B T_{\text{ST}}}{(\gamma + 1) n_H \Lambda(T_{\text{ST}})}, \quad (\text{A.1})$$

where  $n_H$ ,  $n_e$ , and  $n_t$  are the number densities of hydrogen, electrons, and total ions and electrons, respectively, while  $\Lambda$  represents the cooling function. Here, we assume the ratio of the number densities of hydrogen to helium atoms to be 10:1.  $T_{\text{ST}}$  is the temperature at the post-shock layer of the shock wave, obtained from the Sedov–Taylor solution and the Rankine–Hugoniot relation (Kim and Ostriker, 2015):

$$T_{\text{ST}} = 5.3 \times 10^7 \text{ K } E_{51}^{2/5} n_0^{-2/5} t_3^{-6/5}, \quad (\text{A.2})$$

where  $E_{51} = E/(10^{51} \text{ erg})$ ,  $n_0 = n_H/(1 \text{ cm}^{-3})$ ,  $t_3 = t/(1 \text{ kyr})$  denote the energy injected by the SN explosion, the number density of hydrogen atoms in the ISM, and the time from the SN explosion.

Cooling via metal-line emission is most effective at  $T \sim 10^5 \text{ K}$ , and the cooling function at  $10^5 \text{ K} < T < 10^7 \text{ K}$  is well-approximated as

$$\Lambda(T) = 10^{-22} \text{ erg cm}^3 \text{ s}^{-1} \Lambda_{6,-22} \left( \frac{T}{10^6 \text{ K}} \right)^{-0.7}, \quad (\text{A.3})$$

where  $\Lambda_{6,-22} = \Lambda(10^6 \text{ K})/(10^{-22} \text{ erg cm}^3 \text{ s}^{-1})$  depicts the value of the cooling function at  $T = 10^6 \text{ K}$  (see Fig. A.1). From equations (A.1), (A.2), and (A.3), the cooling time of the gas at the shock front at time  $t_s$  is

$$t_c(t_s) = 2.6 \times 10^7 \text{ yr} \left( \frac{t_s}{1 \text{ kyr}} \right)^{-2.04} E_{51}^{0.68} n_0^{-1.68} \Lambda_{6,-22}^{-1}. \quad (\text{A.4})$$

Kim and Ostriker (2015) found that when the cooling time is set to  $t_c = 0.6 e/(de/dt)$ , the shell-formation time obtained from Eq. (A.6) is in good agreement with the numerical results (Kim et al., 2017).

The gas that is stirred up at time  $t_s$  cools down to form a low-temperature ( $T < 10^5 \text{ K}$ ) dense shell at

$$t_{\text{sf}}(t_s) = t_s + t_c(t_s). \quad (\text{A.5})$$

The shell-formation time is determined as the minimum value of  $t_{\text{sf}}(t_s)$  following the method of [Cox and Anderson \(1982\)](#), [Cox \(1986\)](#):

$$t_{\text{sf}} = 4.5 \times 10^4 \text{ yr } E_{51}^{0.22} n_0^{-0.55} \Lambda_{6,-22}^{-0.33}. \quad (\text{A.6})$$

Combining Eq. (A.6) with the Sedov–Taylor self-similar solution, we obtain the radius, mass, and momentum at shell formation as:

$$R_{\text{sf}} = \xi_0 \left( \frac{E}{\rho} \right)^{2/5} t_{\text{sf}}^{2/5} = 23 \text{ pc } E_{51}^{0.29} n_0^{-0.42} \Lambda_{6,-22}^{-0.13}, \quad (\text{A.7})$$

$$M_{\text{sf}} = \frac{4}{3} \pi R_{\text{sf}}^3 \rho = 1.8 \times 10^3 M_{\odot} E_{51}^{0.87} n_0^{-0.26} \Lambda_{6,-22}^{-0.39}, \quad (\text{A.8})$$

$$p_{\text{sf}} = 2.69 \frac{3}{4\pi} M_{\text{sf}} \dot{R}_{\text{sf}} = 2.2 \times 10^5 M_{\odot} \text{ km s}^{-1} E_{51}^{0.93} n_0^{-0.13} \Lambda_{6,-22}^{-0.19}, \quad (\text{A.9})$$

where the coefficient 2.69 is the value obtained when integrating the profiles of the Sedov–Taylor self-similar solution (see Eq. (16) of [Kim and Ostriker, 2015](#)). The  $\Lambda_{6,-22}$  value depends on metallicity. Since the cooling rate due to metal-line emission is proportional to the metal abundance, it proportionally varies with metallicity for a fixed metal abundance ratio. In this study, we use the cooling function of [Sutherland and Dopita \(1993\)](#). They assumed a solar abundance ratio ([Anders and Grevesse, 1989](#)) for  $\log(Z/Z_{\odot}) > 0.0$ , and a primordial abundance ratio ([Wheeler et al., 1989](#), [Bessell et al., 1991](#)) for  $\log(Z/Z_{\odot}) \leq -1.0$ , where  $Z_{\odot} = 0.0194$  is the solar metallicity. Here, we fit the cooling function at  $T = 10^6$  K as follows:

$$\Lambda_{6,-22}(Z) = \max \left( 1.9 - 0.85 \frac{Z}{Z_{\odot}}, 1.05 \right) \frac{Z}{Z_{\odot}} + 10^{-1.33} \quad (\text{A.10})$$

Combining Eqs. (A.6) and (A.10), we obtained the metallicity-dependent shell-formation time.

### A.1.1.2 Multiple SNe

One can estimate the average time interval between the SN explosions in a stellar cluster by multiplying the stellar initial mass function with stellar age, which is approximately evenly spaced ([Ferrand and Marcowith, 2010](#)). The temporal evolution of the superbubble can be thought of in the same way as that of an SN remnant formed by a single SN explosion, by assuming SN explosions to occur at regular time intervals with a continuous injection of energy.

The superbubble evolves adiabatically until the cooling effect manifests and a shell forms. Its time evolution is represented by a self-similar solution, where the dimensionless quantity  $\xi$  is a combination of the radius  $r$ , the energy released in a single SN explosion  $E_{\text{SN}}$ ,

the SN explosion interval  $\Delta t_{\text{SN}}$ , the density of the ISM  $\rho$ , and the time  $t$ :

$$\xi = \left( \frac{\rho}{E_{\text{SN}}/\Delta t_{\text{SN}}} \right)^{1/5} \frac{r}{t^{3/5}}. \quad (\text{A.11})$$

Compared to the case of a single SN explosion, the energy  $E$  in the dimensionless quantity of the Sedov–Taylor solution is replaced by the energy injection rate  $E/\Delta t_{\text{SN}}$ , resulting in a difference in the time dependence from  $t^{2/5}$  to  $t^{3/5}$ . The value of  $\xi$  at the shock is  $\xi_0 = 0.88$ , and the ratio of kinetic and thermal energies is  $E_k : E_{\text{th}} = 22 : 78$  (Weaver et al., 1977).

The shell-formation time can be estimated by replacing the energy  $E$  in Eq. (A.6) with the total energy injected until time  $t$ ,  $E_{\text{SN}}(t/\Delta t_{\text{SN}})$ , and solving for  $t$ :

$$t_{\text{sf,m}} = 1.7 \times 10^4 \text{ yr } E_{51}^{0.28} \Delta t_{\text{SN},6}^{-0.28} n_0^{-0.71} \Lambda_{6,-22}^{-0.42}. \quad (\text{A.12})$$

The radius, velocity, mass, and momentum at this point in time are

$$R_{\text{sf,m}} = 5.3 \text{ pc } E_{51}^{0.37} \Delta t_{\text{SN},6}^{-0.37} n_0^{-0.63} \Lambda_{6,-22}^{-0.25}, \quad (\text{A.13})$$

$$V_{\text{sf,m}} = 1.8 \times 10^2 \text{ km s}^{-1} E_{51}^{0.088} \Delta t_{\text{SN},6}^{-0.088} n_0^{0.084} \Lambda_{6,-22}^{0.17}, \quad (\text{A.14})$$

$$M_{\text{sf,m}} = 22 M_{\odot} E_{51}^{1.11} \Delta t_{\text{SN},6}^{-1.11} n_0^{-0.89} \Lambda_{6,-22}^{-0.75}, \quad (\text{A.15})$$

$$p_{\text{sf,m}} = 3.3 \times 10^3 M_{\odot} \text{ km s}^{-1} E_{51}^{1.2} \Delta t_{\text{SN},6}^{-1.2} n_0^{-0.80} \Lambda_{6,-22}^{-0.59}. \quad (\text{A.16})$$

We use Eqns. (A.12), (A.13), and (A.16) to normalize each physical quantity while examining the time evolution in Fig. A.8 & A.9.

## A.2 ATHENA++ simulation of superbubbles

### A.2.1 Numerical Method

We carried out 3D hydrodynamical simulations with the ATHENA++ code<sup>1</sup> (Stone et al., 2020) with the second-order accurate van Leer time integrator, the HLLC solver, and

<sup>1</sup><https://www.athena-astro.app>

second-order spatial reconstruction. We solved for the equations of continuity, momentum conservation, and energy while incorporating cooling, heating, and thermal conduction:

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{v}) = 0 \quad (\text{A.17})$$

$$\frac{\partial(\rho \mathbf{v})}{\partial t} + \nabla \cdot (\rho \mathbf{v} \mathbf{v} + P) = 0 \quad (\text{A.18})$$

$$\frac{\partial E}{\partial t} + \nabla \cdot \{(E + P) \cdot \mathbf{v}\} = \nabla \cdot (\kappa \nabla T) + n_{\text{H}} \Gamma(T) - n_{\text{H}}^2 \Lambda(T), \quad (\text{A.19})$$

where  $E$  is the energy density. We did not consider self-gravity and magnetic fields in our simulation. Assuming a mean molecular weight of  $\mu = 1.4$ , the gas temperature is taken at  $T = P/(1.1n_{\text{H}}k_{\text{B}})$ , where the hydrogen number density is  $n_{\text{H}} = \rho/(1.4m_{\text{H}})$ . We followed [Kim and Ostriker \(2015\)](#) for the implementation of radiative cooling and heating. For the cooling function  $\Lambda(T)$  at low ( $T < 10^4$  K) and high ( $T > 10^4$  K) temperatures of gas, we adopted the fitting formulae from [Koyama and Inutsuka \(2002\)](#)<sup>2</sup> and piecewise power-law fits to the cooling function of [Sutherland and Dopita \(1993\)](#) with collisional ionization equilibrium<sup>3</sup>, respectively, as shown in Fig. A.1. Heating was applied, with the following heating function, only at  $T < 10^4$  K to model the photoelectric heating of warm/cold ISM:

$$\Gamma(T) = \begin{cases} 10^{-26} \left(\frac{n_{\text{H}}}{1 \text{ cm}^{-3}}\right) \text{ erg s}^{-1} & (T < 10^4 \text{ K}) \\ 0 \text{ erg s}^{-1} & (T > 10^4 \text{ K}). \end{cases} \quad (\text{A.20})$$

We used different cooling functions at  $T > 10^4$  K for different metallicities, but we did not take into account the metallicity dependence at  $T < 10^4$  K. We did not consider the metallicity dependence of the heating function. At  $Z \ll 1$ , the low-temperature cooling and heating rates would be quite different due to reduced photoelectric heating and cooling by fine-structure C and O lines when the metal abundance is low. However, these differences do not affect the results of our simulations, because the shell formation time is determined by the cooling time of shock-heated gas at high temperatures. We imposed a temperature floor of  $10^3$  K.

We followed [El-Badry et al. \(2019\)](#) to implement thermal conduction. For thermal conductivity  $\kappa$  at low ( $T \leq 6.6 \times 10^4$  K) and high ( $T > 6.6 \times 10^4$  K) temperatures of gas, we applied, respectively, the thermal conductivities due to the neutral atomic collision ([Parker, 1963](#)):

$$\kappa = 2.5 \times 10^5 T_4^{1/2} \text{ erg s}^{-1} \text{ cm}^{-1} \text{ K}^{-1}, \quad (\text{A.21})$$

<sup>2</sup>The cooling function given by Eq. (4) of [Koyama and Inutsuka \(2002\)](#) contains two typographical errors. See Eq. (4) of [Vázquez-Semadeni et al. \(2007\)](#) for the corrected functional form.

<sup>3</sup><https://www.mso.anu.edu.au/~ralph/data/cool/>

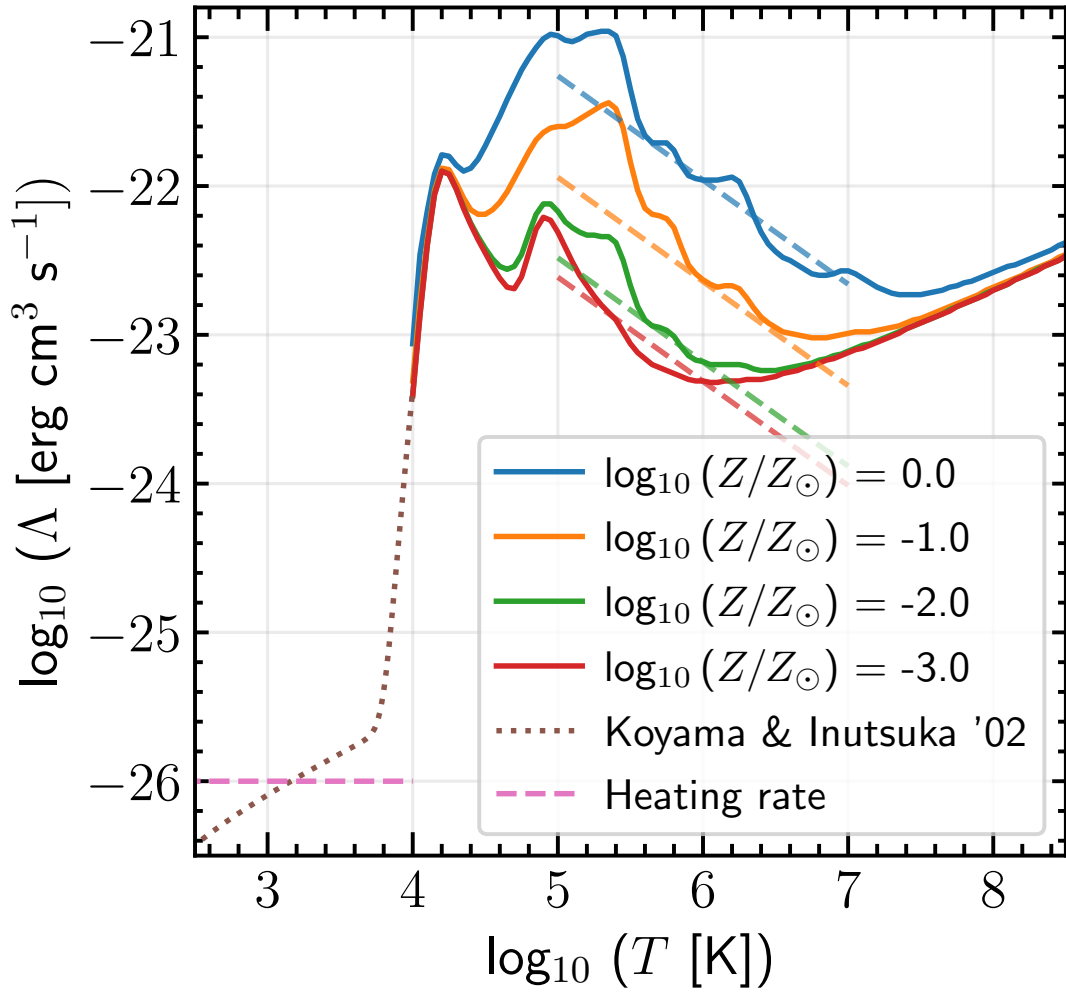


FIGURE A.1: Cooling curves used in this work at different metallicities from [Sutherland and Dopita \(1993\)](#) combined with those of [Koyama and Inutsuka \(2002\)](#). The dashed colored lines show approximations given in Eq. (A.3) for the same metallicities given in the legend. The horizontal line indicates the constant photoelectric heating function  $\Gamma = 1 \times 10^{-26} (n_H/1 \text{ cm}^{-3}) \text{ erg s}^{-1}$  at  $T < 10^4 \text{ K}$ .

where  $T_4 = T/10^4 \text{ K}$ , and hydrogen plasma ([Spitzer, 1962](#)):

$$\kappa = \frac{1.7 \times 10^{11} T_7^{5/2}}{1 + 0.029 \ln(T_7 n_{e,-2}^{-1/2})} \text{ erg s}^{-1} \text{ cm}^{-1} \text{ K}^{-1}, \quad (\text{A.22})$$

where  $T_7 = T/10^7 \text{ K}$ ,  $n_{e,-2} = n_e/10^{-2} \text{ cm}^{-3}$  and  $n_e$  denotes the electron number density. The conductive heat flux  $q = \kappa \nabla T$  is limited by the energy flux that can actually be transported by the electrons  $q_{\text{max}} = \frac{3}{2} \rho c_{s,\text{iso}}^3$  ([Parker, 1963](#), [Cowie and McKee, 1977](#)). The effective thermal conductivity  $\kappa_{\text{eff}}$ , which includes the saturation resulting from limiting the heat flux, becomes

$$\kappa_{\text{eff}}^{-1} = \kappa^{-1} + \frac{|\nabla T|}{q_{\text{max}}}. \quad (\text{A.23})$$

TABLE A.1: Initial conditions of the superbubble simulations.

Number density $n_{\text{H}}$ [ $\text{cm}^{-3}$ ]	0.1, 1, 10
Metallicity $Z$ [ $Z_{\odot}$ ]	$10^{-3}$ , $10^{-2}$ , $10^{-1}$ , 1
Time interval of SN explosions $\Delta t_{\text{SN}}$ [Myr]	0.01, 0.1, 1

To save calculation time, we imposed a ceiling on the thermal conductivity at the following value:

$$\kappa_{\text{ceiling}} = 1.8 \times 10^{12} \left( \frac{n_{\text{H}}}{1 \text{ cm}^{-3}} \right) \text{ erg s}^{-1} \text{ cm}^{-1} \text{ K}^{-1}. \quad (\text{A.24})$$

This value is sufficiently high and has negligible effects on our results. We note that our resolution is not high enough to resolve the conductive interface.

We ran 36 simulations by varying the initial values of the parameters as listed in Table A.1. The spatial resolution was fixed in time and uniform over the simulation box with periodic boundary conditions (we did not use static mesh refinement, SMR, or adaptive mesh refinement, AMR). The spatial resolutions were  $\Delta x = 6, 3,$  and  $0.75$  pc for number densities of  $n_{\text{H}} = 0.1, 1,$  and  $10 \text{ cm}^{-3}$ , respectively, to satisfy the convergence condition by [Kim and Ostriker \(2015\)](#),  $\Delta x < R_{\text{sf}}/10$ . To set up a turbulent initial condition, we start from a uniform density field with pressure of  $2.0 \times 10^3 (n_{\text{H}}/1 \text{ cm}^{-3}) k_{\text{B}} \text{ K cm}^{-3}$ . We then generate the decaying turbulence with only initial forcing and evolve to 1 Myr. The initial forcing field was normalized to a [Kolmogorov \(1941\)](#) power spectrum  $E(k) \propto k^{-5/3}$ , while the range of driving was set to  $2 \leq kL/2\pi \leq 20$ . The velocity dispersion in the box was set to  $\sigma = 5 \text{ km s}^{-1}$  adopted based on Larson’s law ([Larson, 1981, Ohlin et al., 2019](#)). We note that this velocity dispersion of  $5 \text{ km s}^{-1}$  is lower than observed values at the scale of the simulation box, and that the initial evolution of 1 Myr is not long enough for multiphase ISM to develop via thermal instability. As a result, the inhomogeneity in the background is very weak, and the bubble expansion can be much more spherical than in realistic cases, which in turn affects the development of the Kelvin–Helmholtz instabilities that are normally driven by the shear at interfaces.

Thermal energy of  $10^{51}$  erg per SN was injected into cells whose centers were at a distance  $< r_{\text{init}}$  from the site of the SN explosion, where  $r_{\text{init}}$  is the radius within which the mass is  $1 M_{\odot}$ . When thermal energy was injected, a mass of  $1 M_{\odot}$  was also simultaneously injected. We repeated this ten times, at intervals of  $\Delta t_{\text{SN}}$ , setting  $t = 0$  at the time of the initial energy injection.

To study the time evolution of the physical quantities of the superbubble, we define the bubble radius  $R_{\text{bub}}$  as the largest radius which satisfies following two criteria: (i)  $v_r > 3 \text{ km s}^{-1}$ , and (ii)  $t_{\text{dens}} < 4t_{\text{sc}}$ , where  $v_r$  is the radial velocity averaged over a spherical shell of radius  $r$ ,  $t_{\text{dens}} = \rho/\dot{\rho}$  indicates the timescale of the density change, and  $t_{\text{sc}} = \Delta x/c_s$  depicts the sound-crossing time. In practice, we compute  $v_r$ ,  $t_{\text{dens}}$ , and  $t_{\text{sc}}$

for each cell, draw averaged radial profiles of these quantities, and then apply the above criteria. We have described the time evolution of total mass, energy, and momentum within  $R_{\text{bub}}$  in Section A.2.2.1.

To discuss the time evolution of the hot bubble, we also define the hot-gas radius as  $R_{\text{hot}} = (V_{\text{hot}}/(4/3)\pi)^{1/3}$ , where  $V_{\text{hot}}$  is the region at which  $T > 10^4$  K. The time evolution of  $R_{\text{hot}}$  is discussed in Section A.2.3.

## A.2.2 Results from Athena++ simulations

### A.2.2.1 Results for $n_{\text{H}} = 1 \text{ cm}^{-3}$ , $Z = 1 Z_{\odot}$ , $\Delta t_{\text{SN}} = 0.1 \text{ Myr}$

Figure A.2 shows a slice plot of density and temperature at 0.03 Myr after the fifth energy injection for the case of  $n_{\text{H}} = 1 \text{ cm}^{-3}$ ,  $Z = Z_{\odot}$ ,  $\Delta t_{\text{SN}} = 0.1 \text{ Myr}$ . The collected gas forms a low-temperature, high-density shell, inside which exists a high-temperature, low-density gas. The shell grows almost spherically, but with a slight distortion due to the density fluctuations caused by turbulence. We see that  $R_{\text{hot}}$  adequately captures the size of the hot bubble inside the shell, with  $R_{\text{bub}}$  enclosing the shell itself.

Figure A.3 shows the phase diagram at this time. The low-temperature ( $T < 2 \times 10^3$  K) gas at the bottom right corner is the ISM gas. The gas swept up at the front of the shell is heated by the shock, but as the temperature rises to  $T > 10^4$  K, it loses energy due to hydrogen recombination. Since the shock compresses the gas to a high density, its cooling time is shorter than the dynamical time, and a shell of  $T \sim 10^4$  K,  $n_{\text{H}} \sim 10 \text{ cm}^{-3}$  is formed. At the post-shock layer of the shell, the gas can be heated by compression (if a shock propagates through the layer), or by mixing (if hot gas is advected into a cell containing cool gas), or by thermal conduction (if conduction is resolved). In our simulation, the upper left plume of hot gas in Figure A.3 is heated by compression and thermal conduction.

Figure A.4 shows the time evolution of the superbubble. The shell forms when it grows to a radius of about 20 pc, after which its growth slows down from the adiabatic phase. The subsequent energy injection stirs up the gas inside the shell and reduces its density. However, the density increases again due to the evaporation from the shell to the interior, and the mass is transferred from the cold shell to the hot interior.

### A.2.2.2 Results for $\Delta t_{\text{SN}} = 0.01 \text{ Myr}$

The time evolution of mass, energy, and momentum for an SN explosion with a time interval of 0.01 Myr is shown in Figure A.5.

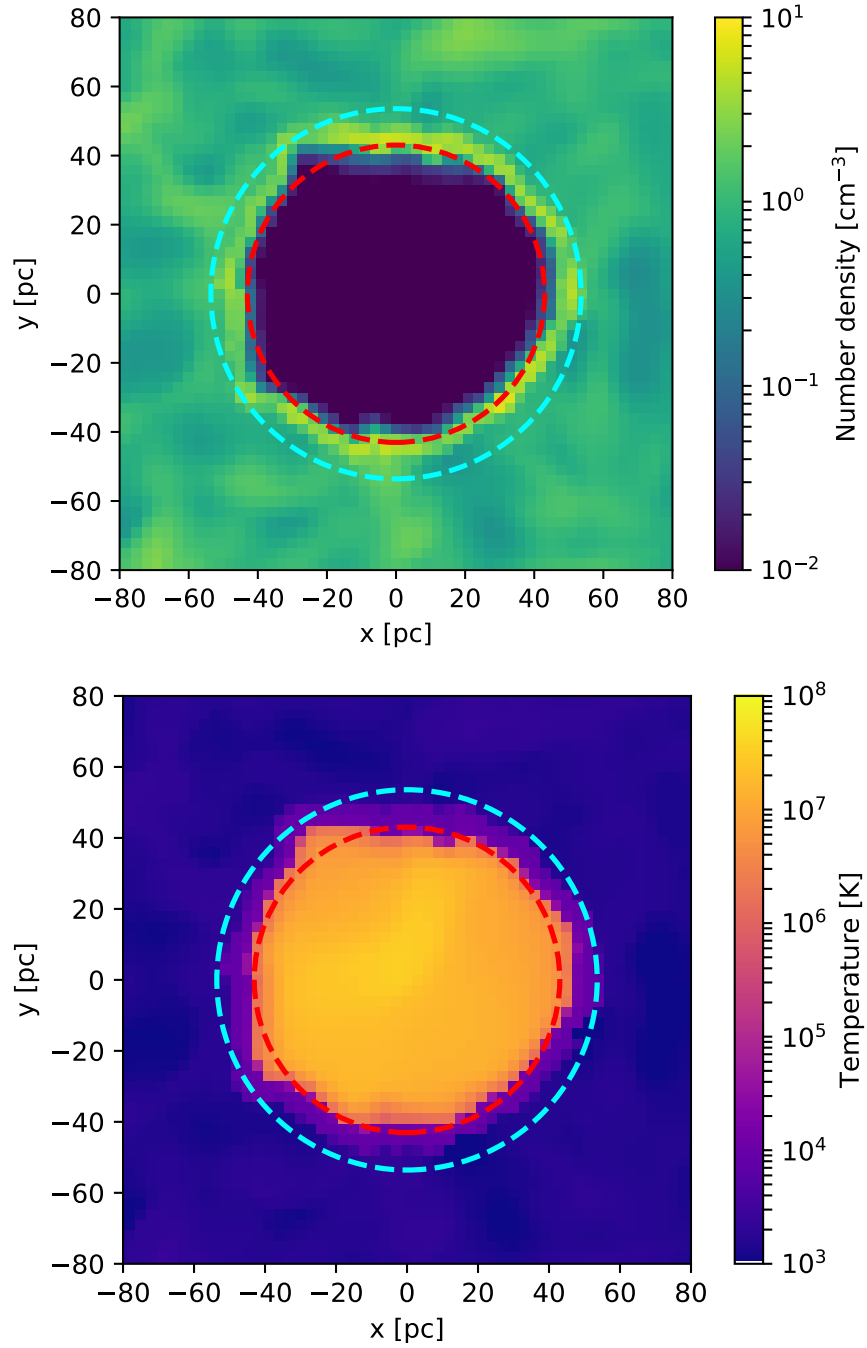


FIGURE A.2: Slice plot of gas number density and temperature distribution at  $t = 0.53$  Myr for the case of  $n_{\text{H}} = 1 \text{ cm}^{-3}$ ,  $Z = Z_{\odot}$ ,  $\Delta t_{\text{SN}} = 0.1$  Myr. The inner red circle shows  $R_{\text{hot}}$ , while the outer cyan circle shows  $R_{\text{bub}}$ .



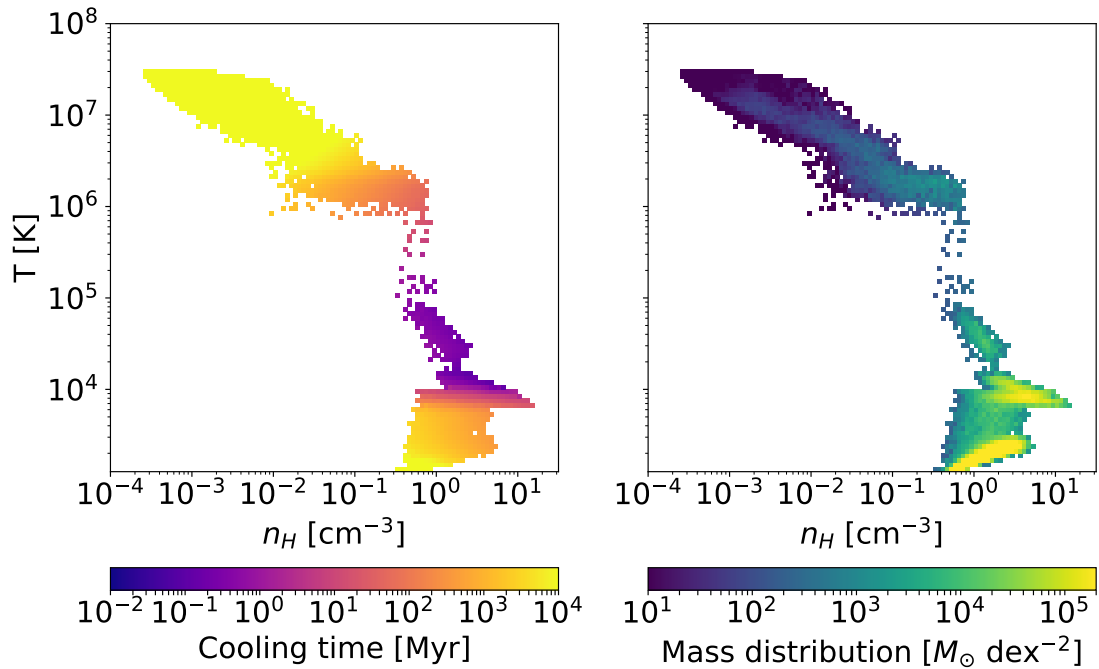


FIGURE A.3: Phase diagram of gas in computational box, weighted for its cooling time (left panel) and mass (right panel), at the same time as in Fig. A.2. In the left panel, one can see that the cooling time is short in the shell of  $T \sim 10^4$  K and  $n_H \sim 10 \text{ cm}^{-3}$ .

For  $n_H = 0.1 \text{ cm}^{-3}$ , the system evolves adiabatically because the shell-formation time is longer than 0.1 Myr for any metallicity. Since the metallicity affects the shell-formation time but not the system’s dynamics, no metallicity dependence is observed in this case. Since the system evolves adiabatically, its total energy after 10 SN explosions is  $10^{52}$  erg. In the case of  $n_H = 1 \text{ cm}^{-3}$ , the cooling time is shorter due to the higher density, and this cooling effect is seen for  $\log(Z/Z_\odot) = 0, -1$ . The cooling effect is seen earlier for  $\log(Z/Z_\odot) = 0$  because the larger the metallicity is, the shorter the cooling time is. Shell formation does not immediately get completed and, in the case of  $\log(Z/Z_\odot) = 0$ , the cooling effect begins to appear at  $t \sim 0.04$  Myr, while shell formation completes at  $t \sim 0.1$  Myr. During shell formation, the mass of the shell increases while that of the hot gas remains constant because it proceeds from the dense and short cooling time gas gathered in front of the superbubble.

In the case of  $n_H = 10 \text{ cm}^{-3}$ , the shell-formation time is shorter than 0.1 Myr at all metallicities, and a low-temperature, high-density shell is formed. After shell formation, most of the system’s mass is in the shell, and at  $t = 0.1$  Myr, the mass of the hot gas is about 2% of the total. Comparing the cases of  $\log(Z/Z_\odot) = -2.0, -3.0$ , there is little difference in the time evolution of the physical quantities. In the low-metallicity environment, bremsstrahlung is a more dominant cooling mechanism than metal line emission at  $T > 10^6$  K, and hence the difference in metallicity becomes less apparent.

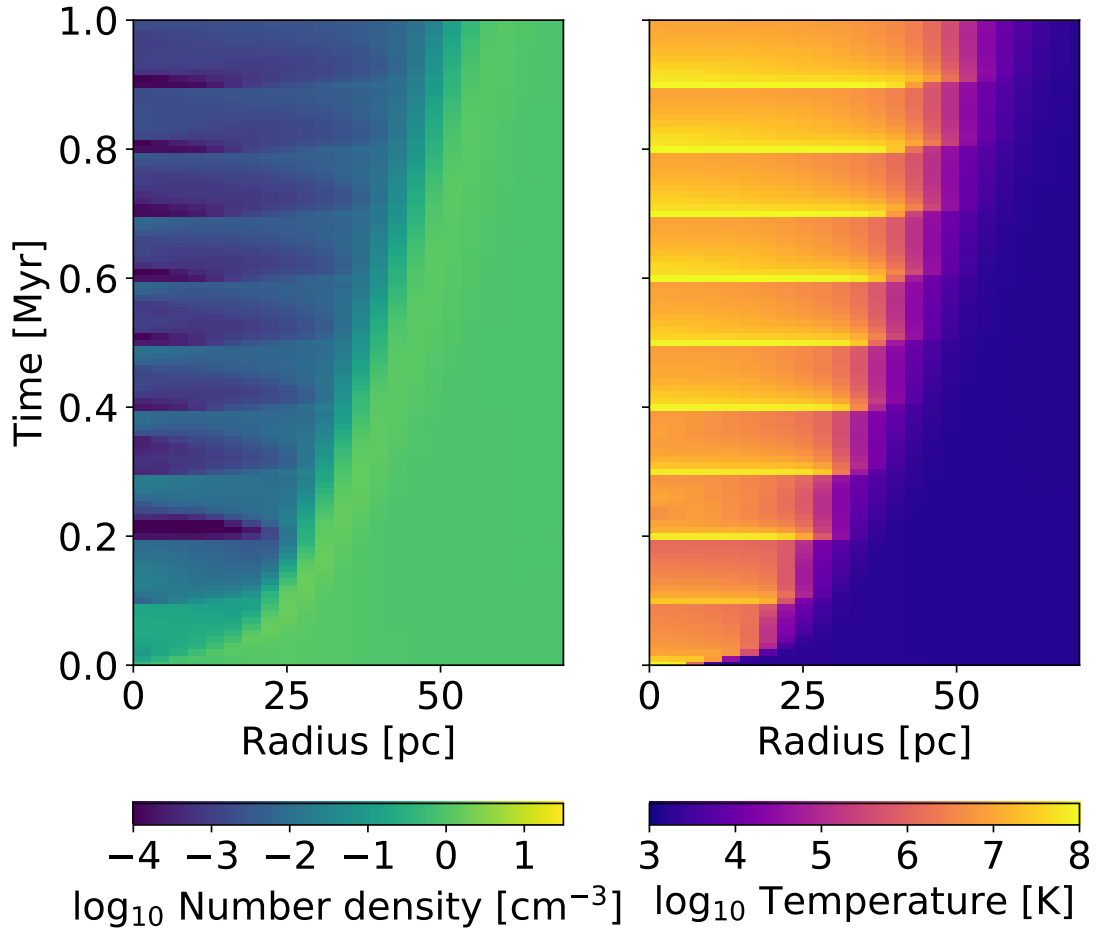


FIGURE A.4: Evolution of superbubble as a function of radius, weighted for gas number density (left panel) and gas temperature (right panel), for the case of  $n_{\text{H}} = 1 \text{ cm}^{-3}$ ,  $Z = Z_{\odot}$ ,  $\Delta t_{\text{SN}} = 0.1 \text{ Myr}$ . One can see the power-law expansion of the hot bubble. The horizontal features indicate the intermittent SN injection.

### A.2.2.3 Results for $\Delta t_{\text{SN}} = 0.1 \text{ Myr}$

The time evolution of mass, energy, and momentum of a superbubble in the cases of  $\Delta t_{\text{SN}} = 0.1 \text{ Myr}$  is shown in Fig. A.6. In this case, the shell-formation time is shorter due to the lower energy injection rate than  $\Delta t_{\text{SN}} = 0.01 \text{ Myr}$ .

In cases of  $n_{\text{H}} = 0.1 \text{ cm}^{-3}$  and  $\log(Z/Z_{\odot}) = 0.0, -1.0$ , the shell formation is completed within the simulation time, after which the kinetic energy becomes roughly constant as shown by the red solid line in the left middle panel of the Fig. A.6.

In cases of  $n_{\text{H}} = 1 \text{ cm}^{-3}$ , the shell formation completes before the second SN explosion. Each SN explosion injects  $10^{51} \text{ erg}$  of thermal energy; some of it is converted to kinetic energy by  $PdV$  work on the shell, and the rest is dissipated by cooling so that most of the thermal energy is lost within 0.1 Myr following energy injection. From the phase diagram at  $t = 0.53 \text{ Myr}$  for  $\log(Z/Z_{\odot}) = 0.0$  (Fig. A.3), the cooling time of the gas

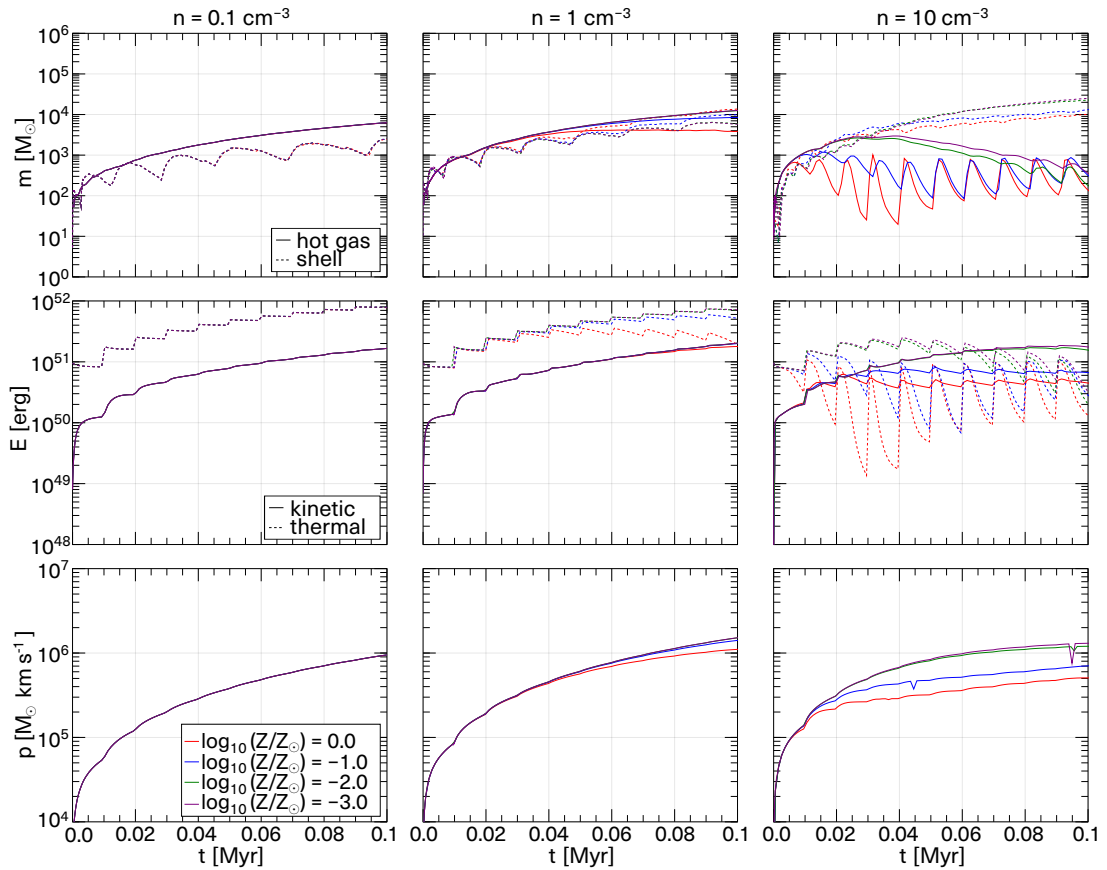


FIGURE A.5: Time evolution of mass (top row), energy (middle row) and momentum (bottom row) of the superbubble for SN injection time intervals of  $\Delta t_{\text{SN}} = 0.01$  Myr. For each component, we also show four different metallicities as indicated in the legend. Left column:  $n_{\text{H}} = 0.1 \text{ cm}^{-3}$ . Middle column:  $n_{\text{H}} = 1 \text{ cm}^{-3}$ . Right column:  $n_{\text{H}} = 10 \text{ cm}^{-3}$ . In the top panels for mass, the solid lines are for the hot gas inside the superbubble while dotted lines are for the shell. In the middle panels for energy, the solid lines are for kinetic energy while the dotted lines are for the thermal energy of superbubble gas including the shell. In the left column, the lines for the four metallicities overlap because of low density and long shell-formation time, which prolongs the adiabatic phase with little metal-cooling. In the right column, the effect of intermittent SN injection is visible.

inside the shell is longer than 1 Myr. However, heat is transported to the shell by gas mixing at its rear surface and then radiated away (El-Badry et al., 2019, Fielding et al., 2020, Lancaster et al., 2021a,b), resulting in the loss of thermal energy within a duration shorter than 1 Myr. We note that our resolution is not high enough to resolve the conductive interfaces, and some of the thermal energy could be lost due to numerical diffusion. As shown in the top middle panel of Fig. A.6, the shell grows in mass while conserving momentum after each SN injection. At the same time, the kinetic energy decreases as shown in the central panel of Fig. A.6.

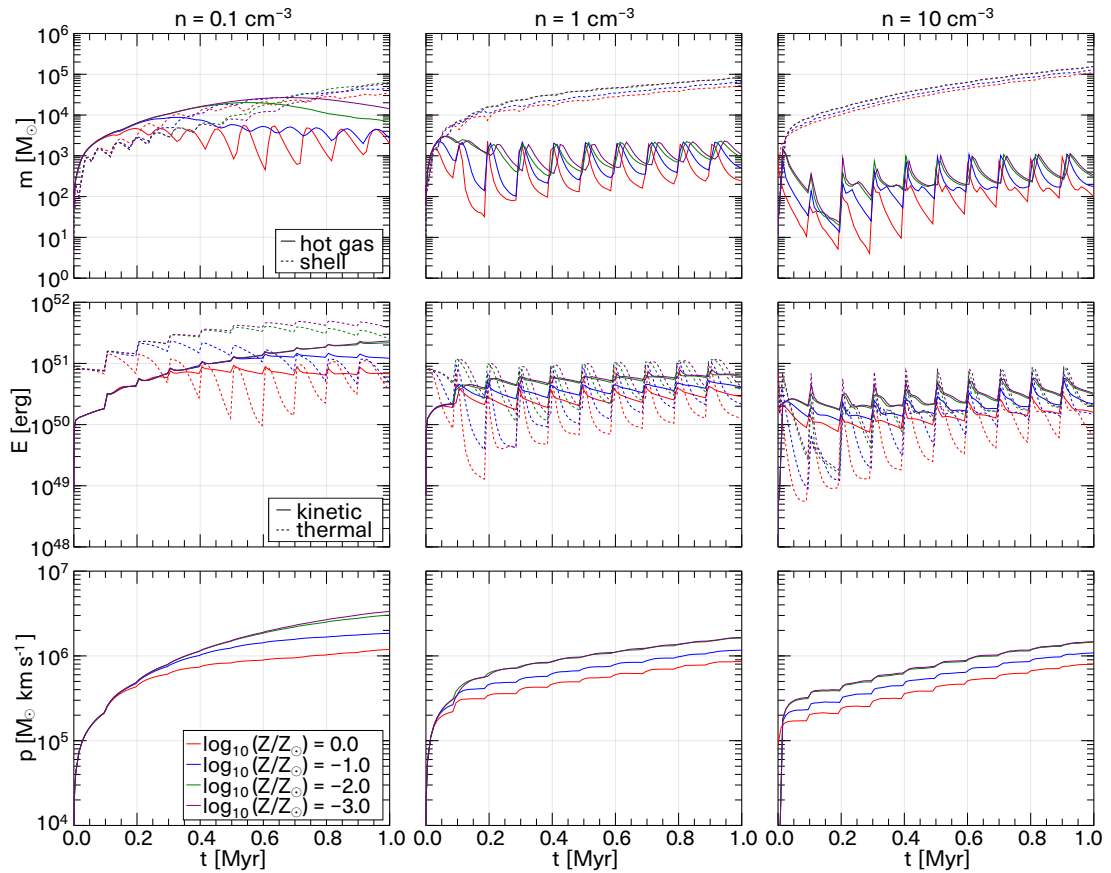


FIGURE A.6: Same as Figure A.5, but for SN injection time interval  $\Delta t_{\text{SN}} = 0.1$  Myr. Note that the time range in the abscissa is different from that in Figure A.5.

#### A.2.2.4 Results for $\Delta t_{\text{SN}} = 1$ Myr

The time evolution of superbubble mass, energy, and momentum in the case of  $\Delta t_{\text{SN}} = 1$  Myr is shown in Fig. A.7. In this case, the shell is formed before the second SN explosion occurs in all cases; therefore the time evolution is similar to that for  $\Delta t_{\text{SN}} = 0.1$  Myr,  $n_{\text{H}} = 1, 10 \text{ cm}^{-3}$ . At  $t > 4$  Myr, thermal energy exceeds kinetic energy. At this time, most of the mass is in the shell with its interior being cooled. Therefore, the gas in the shell contains most of the thermal energy of the superbubble. As shell mass increases while conserving momentum, its kinetic energy decreases. Let the velocity, temperature, and density of the shell be  $v_{\text{shell}}$ ,  $T_{\text{shell}}$ , and  $\rho_{\text{shell}}$ , respectively. When the kinetic energy decreases to  $(1/2)\rho_{\text{shell}}v_{\text{shell}}^2 < (3/2)(\rho_{\text{shell}}/\mu m_{\text{H}})k_{\text{B}}T_{\text{shell}}$ , the thermal energy becomes larger. If the temperature of the shell is around the ISM temperature  $T_{\text{ISM}} \sim 2 \times 10^3$  K, then the thermal energy exceeds kinetic energy when  $v_{\text{shell}} < 7 \text{ km s}^{-1}$ . When  $n_{\text{H}} = 10 \text{ cm}^{-3}$ , the mass and momentum appear to be decreasing when  $t$  is large. This is because the shell velocity has fallen below  $3 \text{ km s}^{-1}$ , whereby we can no longer follow its time evolution. In such a case, the shell is expected to gradually mix with the ISM.

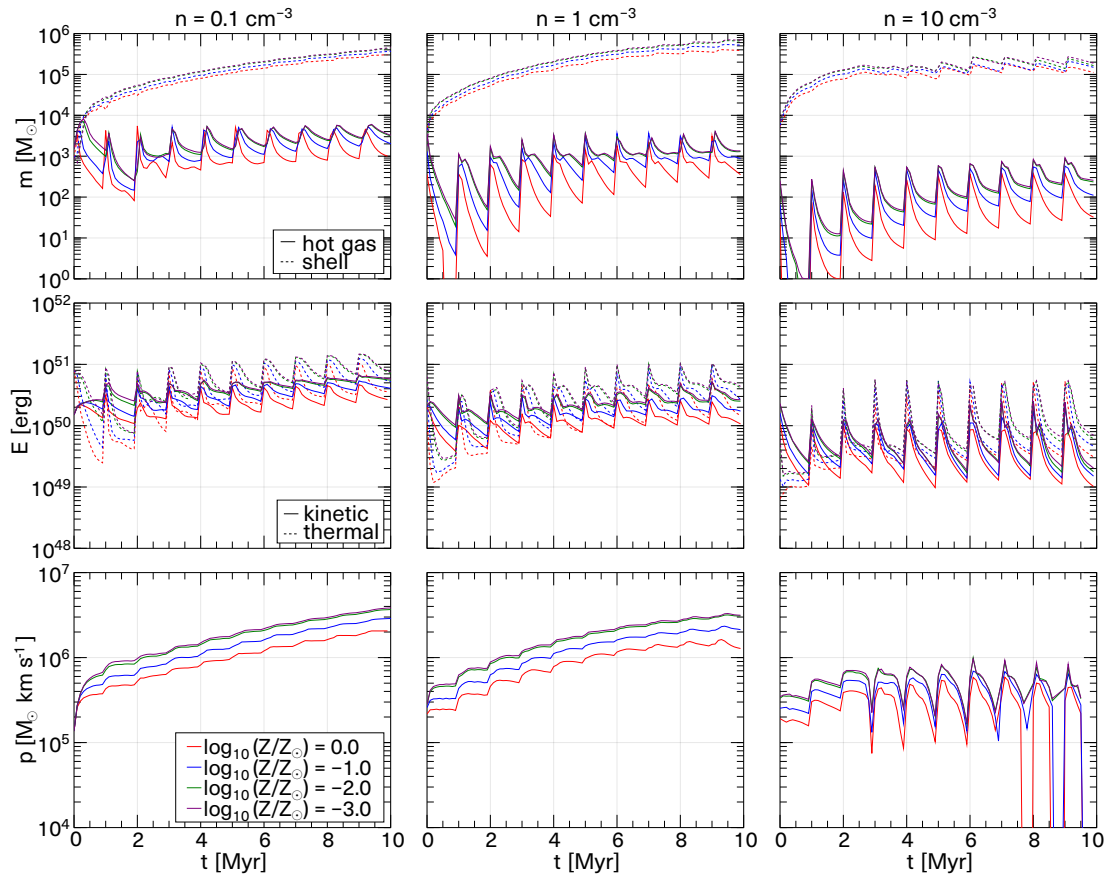


FIGURE A.7: Same as Figure A.5, but for SN injection time interval  $\Delta t_{\text{SN}} = 1$  Myr. Note that the time range in the abscissa is different from that in Figure A.5.

### A.2.3 Application to SN feedback model in galaxy simulations

In this section, we derive the scaling relations for the time evolution of superbubble momentum and radius for the application to the SN feedback model in galaxy simulations.

To discuss the environmental dependence of the superbubble in a unified manner, we normalize each physical quantity by its value at the shell-formation time. The same was done for single SN explosion simulations by Kim and Ostriker (2015), and also by Kim et al. (2017) for only the time variable for multiple SN explosion simulations.

Figure A.8 shows the time evolution of the radius, normalized by its value at the shell-formation time. The time evolution of the radius shows some deviations, but in all cases, we can see that the radius evolves according to

$$\frac{R_{\text{hot}}}{R_{\text{sf,m}}} = \left( \frac{t}{t_{\text{sf,m}}} \right)^{0.5}, \quad (\text{A.25})$$

as was also found by Kim et al. (2017). When  $t < t_{\text{sf,m}}$ , the superbubble is in an adiabatic period and expected to evolve with  $R \propto t^{3/5}$  (Eq. A.11). The good fit of the straight

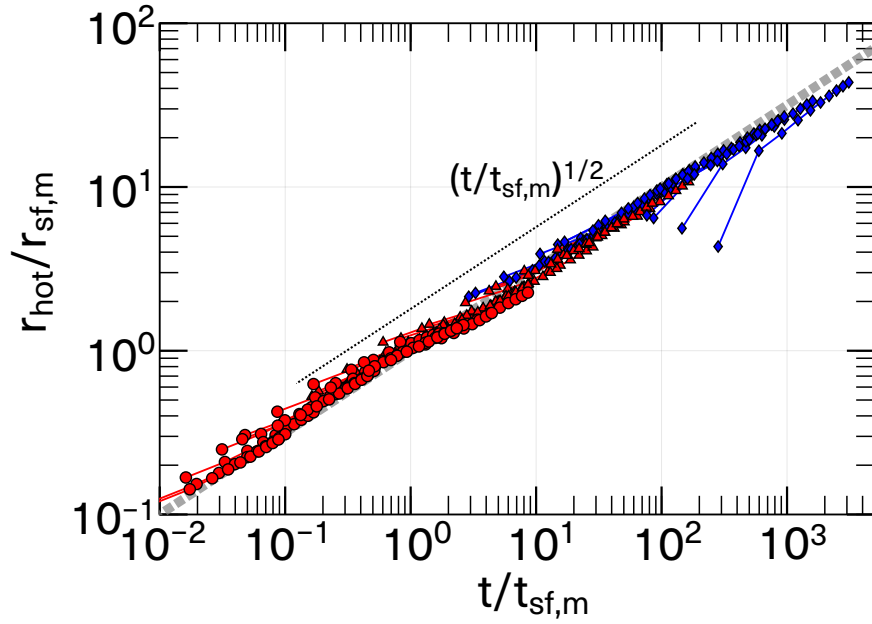


FIGURE A.8: Evolution of  $R_{\text{hot}}$  normalized by  $R_{\text{sf},m}$ , versus time normalized by  $t_{\text{sf},m}$ . Red and blue points depict the runs with  $\Delta t_{\text{SN}} < 0.1t_{\text{PDS}}$  and  $\Delta t_{\text{SN}} > 0.1t_{\text{PDS}}$ , respectively. Different symbols connected by line correspond to runs at different SN intervals:  $\Delta t_{\text{SN}} = 0.01 \text{ Myr}$  (circle),  $\Delta t_{\text{SN}} = 0.1 \text{ Myr}$  (triangle),  $\Delta t_{\text{SN}} = 1 \text{ Myr}$  (diamond). The thick black dotted line shows the power-law of Eq. (A.25).

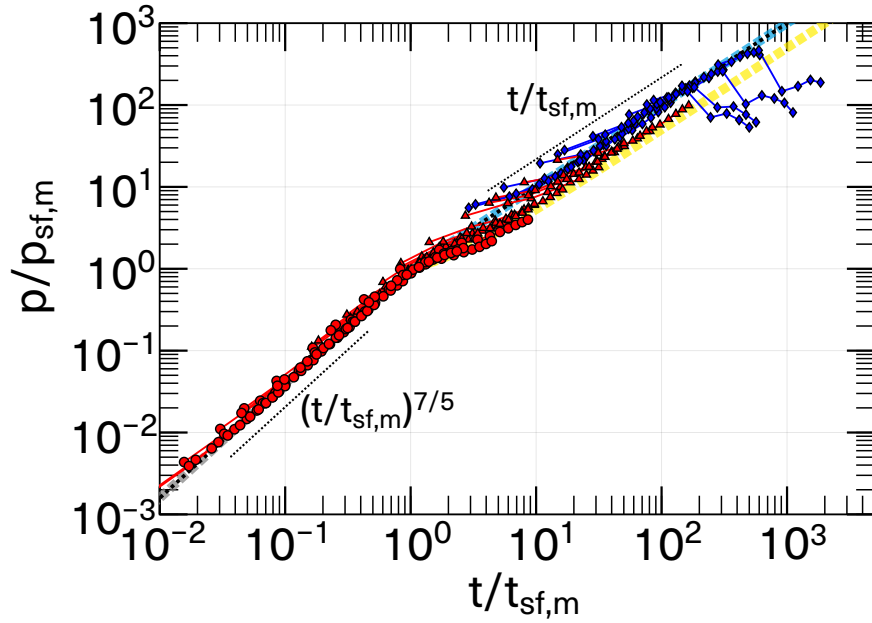


FIGURE A.9: Evolution of momentum  $p$  normalized by  $p_{\text{sf},m}$ , versus time normalized by  $t_{\text{sf},m}$ . Red and blue points depict the runs with  $\Delta t_{\text{SN}} < 0.1t_{\text{PDS}}$  and  $\Delta t_{\text{SN}} > 0.1t_{\text{PDS}}$ , respectively. Different symbols connected by line correspond to runs at different SN intervals:  $\Delta t_{\text{SN}} = 0.01 \text{ Myr}$  (circle),  $\Delta t_{\text{SN}} = 0.1 \text{ Myr}$  (triangle),  $\Delta t_{\text{SN}} = 1 \text{ Myr}$  (diamond). The black dotted lines indicates the  $(p/p_{\text{sf},m}) \propto (t/t_{\text{sf},m})^{7/5}$  and  $(p/p_{\text{sf},m}) \propto (t/t_{\text{sf},m})$  power-law, respectively. The thick gray, yellow and cyan dotted lines indicate the fitting function of Eq. (A.29).

line with a slope of 0.5 can be attributed to the fact that the energy injection is discrete rather than continuous, resulting in an intermediate time evolution with the Sedov–Taylor solution  $R \propto t^{2/5}$ . The asymptote of the fitting line is due to the transition from the Sedov–Taylor solution to the adiabatic solution of the superbubble. Time evolution after shell formation can also be approximated by a straight line with a slope of 0.5. The asymptotic behavior of the blue lines from the bottom is because the hot-gas radius  $R_{\text{hot}}$  could not correctly follow the radius of the inside of the shell when it was cooled down to  $T < 2 \times 10^4$  K. The scaling relation  $R \propto t^{1/2}$  agrees with the prediction from the momentum-driven model and not with that from the pressure-driven model (Ostriker and McKee, 1988). Substituting the values of  $R_{\text{sf,m}}$ ,  $t_{\text{sf,m}}$  (Eqs. (A.13), (A.12)), the time evolution of radius and velocity are obtained as

$$R = 40 \text{ pc } t_6^{1/2} E_{51}^{0.23} \Delta t_{\text{SN},6}^{-0.23} n_0^{-0.28} \Lambda_{6,-22}^{-0.040}, \quad (\text{A.26})$$

$$V = 20 \text{ km s}^{-1} t_6^{-1/2} E_{51}^{0.23} \Delta t_{\text{SN},6}^{-0.23} n_0^{-0.28} \Lambda_{6,-22}^{-0.040}. \quad (\text{A.27})$$

Next, we show the time evolution of momentum in Figure A.9. It shows two different trends after the shell-formation time. If the interval between SN explosions is longer than the duration of the pressure-driven snowplow (PDS) phase of a single SN explosion,

$$t_{\text{PDS}} = 5.0 \times 10^6 \text{ yr } T_{\text{ISM},3}^{-0.7} E_{51}^{0.32} n_0^{-0.36} \Lambda_{6,-22}^{-0.053}, \quad (\text{A.28})$$

where  $T_{\text{ISM},3} = T_{\text{ISM}}/(10^3 \text{ K})$  is the temperature of the ISM, energy injection is considered to be discrete and the superbubble is expected to display an evolution over time that is different from the continuous case. Since thermal transfer to the shell was not considered in the derivation of  $t_{\text{PDS}}$ , the actual duration of the PDS phase will be shorter than  $t_{\text{PDS}}$ .

Here we find that the following fitting functions can describe the two separate regimes continuously, as shown in Fig. A.9:

$$\frac{p}{p_{\text{sf,m}}} = \begin{cases} \tau^{7/5} & (t < t_{\text{sf,m}}) \\ \frac{1}{2} (\tau + \tau^{-1/5}) & (t > t_{\text{sf,m}} \ \& \ \frac{\Delta t_{\text{SN}}}{t_{\text{PDS}}} < 0.1) \\ \tau & (t > t_{\text{sf,m}} \ \& \ \frac{\Delta t_{\text{SN}}}{t_{\text{PDS}}} > 0.1), \end{cases} \quad (\text{A.29})$$

where  $\tau = t/t_{\text{sf,m}}$ . Since the momentum can be estimated as  $p = (4/3)\pi R^3 \rho \dot{R}$ , when the time evolution of the radius is expressed as  $R \propto t^\alpha$ ,  $p \propto t^{4\alpha-1}$ . Before shell formation, the superbubble grows adiabatically, and the time evolution of its radius is  $R \propto t^{3/5}$ ; thus, the time evolution of momentum is  $p \propto t^{7/5}$ .

When  $t \gg t_{\text{sf,m}}$ , there occurs a deviation from the fitting line. This was also seen when  $\Delta t_{\text{SN}} = 1 \text{ Myr}$ ,  $n_{\text{H}} = 10 \text{ cm}^{-3}$  (Fig. A.7), because the shell velocity dropped below

$3 \text{ km s}^{-1}$  and its time evolution could not be followed.

In passing, we note that [El-Badry et al. \(2019\)](#) derived a criterion to distinguish discrete energy injection versus continuous limit in their Eq.(53). They derived this criterion only by considering the blast waves from individual [SNe](#) before reaching the shell, and their simulation results asymptote to their modified energy-driven solution with cooling at  $t > t_{\text{subsonic}}$ . We only simulated ten [SN](#) explosions, while [El-Badry et al. \(2019\)](#) examined the evolution all the way to the continuous energy injection limit (although with 1-D simulation); therefore, our time-scale shown in Fig.9 is somewhat of a shorter time range than that of [El-Badry et al. \(2019\)](#)'s work (see their Fig. 6). The subsonic timescale  $t_{\text{subsonic}}$  in Eq.(53) of [El-Badry et al. \(2019\)](#) is much longer than our  $t_{\text{PDS}}$ , and therefore it is not straightforward to compare our results using their criteria based on  $t_{\text{subsonic}}$ .



## Appendix B

# Implementation of supernova feedback

In this appendix, we describe the implementation of supernova feedback in SPH simulation. The content in this appendix is a part of my master's thesis work.

A schematic description of the ‘Spherical superbubble model’ developed in this thesis is illustrated in Fig. B.1. When the SN event occurs, we first calculate the density and metallicity at the SN site. An iterative solver is used to find a smoothing length for the stellar particle that satisfies

$$h_{\text{sml},i} = \left( \frac{3N_{\text{ngb}}}{4\pi \sum_j W(r_{ij}, h_{\text{sml},i})} \right)^{1/3}, \quad (\text{B.1})$$

where  $r_{ij}$  is the distance from the  $i$ -th stellar particle to the  $j$ -th gas particle,  $N_{\text{ngb}}$  is the number of neighboring SPH particles, and  $W$  is the kernel function adopted in the SPH simulation. We then compute the shock radius  $R_{\text{shock}}$  using local density and metallicity, using equation (2.18). We search for the gas particles within the shock radius and project them from the position of the star onto a sphere centered at the star with radius  $R_{\text{shock}}$ . Then, we construct a Voronoi polyhedron using STRIPACK<sup>1</sup> (Renka, 1997), which is an algorithm that constructs a Voronoi diagram of a set of points on the surface of a sphere. After constructing the Voronoi polyhedron on the spherical surface, we calculate  $\Omega$ , which is the solid angle of the corresponding face on the Voronoi polyhedron from the star. We distribute physical quantities from the SN to neighboring gas particles weighted

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<sup>1</sup>[https://people.sc.fsu.edu/~jburkardt/f\\_src/stripack/stripack.html](https://people.sc.fsu.edu/~jburkardt/f_src/stripack/stripack.html)

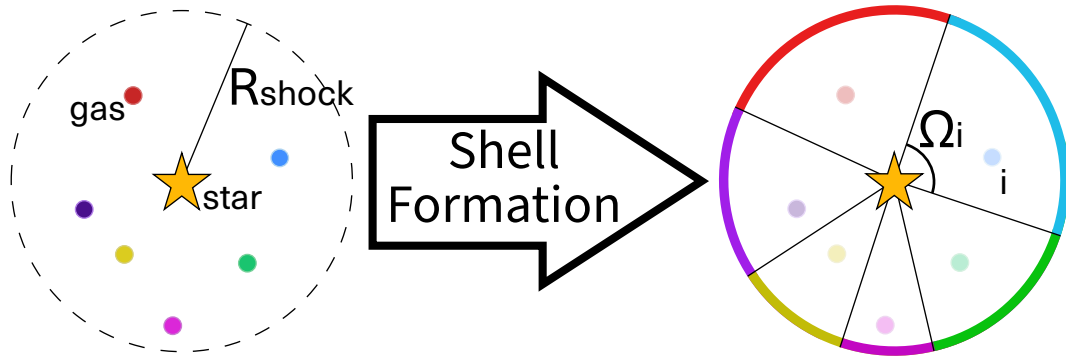


FIGURE B.1: Schematic description of the spherical superbubble feedback model developed in this paper. The left hand side shows the particle distribution of gas and star particles when the supernova explosions begin, whereas the right hand side shows the superbubble shell formation, and how we split the shell using Voronoi tessellation based on the gas particle distribution inside the bubble.

by  $\Omega$ . The mass and metal deposited on the  $i$ -th gas particle are

$$\Delta m_i = m_{\text{SN}} \left( \frac{\Omega_i}{4\pi} \right), \quad (\text{B.2})$$

$$\Delta m_{Z,i} = m_{Z,\text{SN}} \left( \frac{\Omega_i}{4\pi} \right), \quad (\text{B.3})$$

where  $m_{\text{SN}}$  and  $m_{Z,\text{SN}}$  are the mass and metal inputs from feedback and  $\Omega_i$  is the solid angle of the corresponding face on the Voronoi polyhedron from the star. If the number of gas particles inside the shock radius is less than four, the Voronoi polyhedron cannot be constructed. In that case, we search for at least two nearest gas particles and equally assign mass and metals to them. Note that our method is similar to, but different in detail from, that of [Hopkins et al. \(2018\)](#).

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